

# Final Drainage Report

## Leeper Industrial Park

(JN: 21087)

3700 E. 64<sup>th</sup> Avenue  
Commerce City, CO

April 27, 2022

Revised: July 22, 2022

Revised: August 18, 2022

Prepared for:

### **Hampton Partners / SCS LLC**

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Prepared by:

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## **Certification**

### **ENGINEER CERTIFICATION OF DRAINAGE REPORT**

I hereby certify that this report (plan) for the Preliminary Drainage design of Leeper Industrial Park was prepared by me or under my direct supervision in accordance with the provisions of Commerce City Storm Drainage Design and Technical Criteria for the owners thereof. I understand that Commerce City does not and will not assume liability for drainage facilities designed by others.

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Date

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Registered Professional Engineer  
State of Colorado PE No. 45332  
For and on behalf of Proof Civil Co.

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## I. Introduction

This final drainage report for Leeper Industrial Park will address the on-site stormwater conveyance and treatment for the development in accordance with criteria set forth by applicable governing agencies as well as previously approved relevant drainage studies.

## II. General Location and Description

### A. Project Location

The subject property is a 20.08 industrial facility located at 3700 E. 64<sup>th</sup> Avenue in Commerce City, Colorado. The property consists of Lot 3, and a previously unplatted parcel in the Leeper Industrial Park Subdivision. The property is bound to the west by Monroe Street, to the north by an unplatted parcel, to the east by other lots within the Leeper Industrial Park Subdivision and Colorado Boulevard, and to the south by East 64<sup>th</sup> Avenue.

### B. Project Description

The property is an existing industrial facility with two offices, auxiliary buildings, storage yard area, and associated driveways. Aside from the existing buildings, the groundcover of the property consists largely of existing recycled asphalt. A significant portion of the site (approximately 60% of the site area) along the western boundary lies on a buried inactive landfill. The site contains permanent and temporary easements for energy pipeline purposes. No wetlands are known to exist onsite.

### C. Floodplain Information

According to FEMA Flood Insurance Rate Map Panel #08001C0604H, the subject site is located within flood hazard area Zone X. Zone X is defined as area outside the 0.2-percent-chance (or 500-year) flood. Refer to Appendix A for the applicable FEMA flood map.

### D. Soils Description

According to the United States Department of Agriculture Natural Resources Conservation Service (NRCS) National Cooperative Soil Survey, onsite soils are identified as Terrace Escarpments and Vona Sandy Loam and are classified as Hydrologic Soil Group A. Group A is sand, loamy sand or sandy loam types of soils. It has low runoff potential and high infiltration rates even when thoroughly wetted. They consist chiefly of deep, well to excessively drained sands or gravels and have a high rate of water transmission. See Appendix A for the site soil map.

## III. Historic Drainage

### A. Existing Drainage Pattern

The site generally drains from south to north and west to east at a general slope of 0.5%. Flows are then generally conveyed to Monroe Street, and eventually to the O'Brien Canal in the existing condition. The site is covered by compacted earth with little vegetation.

### B. Existing Basins

The existing site is divided into drainage basins described as follows:

#### a. Basin EX-A (9.25 Acres)

Basin EX-A consists of the western portion of the development. The basin is covered with buildings, small concrete pads, and largely made up of recycled earth storage area and undeveloped slope down to Monroe Street. Runoff generated from Basin EX-A sheet flows north and west to Monroe Street. The existing basin is 68% impervious.

**b. Basin EX-B (9.60 Acres)**

Basin EX-B consists of an eastern portion of the bulk area of the site. The basin is covered with buildings, small concrete pads, driveways, and largely made up of recycled asphalt storage yard. Runoff generated from Basin EX-B sheet flows north and east to a low point within the site. Flows either percolate into the soil at this location or overflow into Basin EX-A. The existing basin is 83% impervious.

**c. Basin EX-C (1.64 Acres)**

Basin EX-C consists generally of access to the site from Colorado Boulevard. The basin is covered with asphalt roadway and recycled asphalt storage yard. Runoff generated from Basin EX-C flows onto neighboring properties and the Colorado Boulevard right-of-way. The existing basin is 62% impervious.

**IV. Drainage Criteria**

**A. Regulation**

Methods described in the UDFCD Urban Storm Drainage Criteria Manual and in the Commerce City Storm Drainage Design and Technical Criteria were used for the drainage design of the Site.

**B. Hydrology**

The Rational Method analysis, utilizing the Intensity-Duration-Frequency curves for the area established by the National Oceanic and Atmospheric Administration was used to determine the on-site runoff generated for the 5-year (minor), and 100-year (major) storm events. Runoff coefficients were based on the type of proposed development outlined in the UDFCD manual. Runoff coefficients used in the analysis were weighted according to the existing and proposed land uses in each basin or sub-basin and the time of concentration values have been calculated for each of the basins or sub-basins per Urban Drainage criteria. Detention storage and release rate have been calculated using the UDFCD full-spectrum design criteria. Hydrologic calculations can be found in Appendix B.

**V. Drainage Design**

**A. General Concept**

Proposed on-site drainage design will follow historical drainage patterns. The site will not be altered in any way with the exception of the addition of fresh recycled asphalt for some storage areas and the introduction of an infiltration pond.

**B. Proposed Drainage Basins**

The improved site is divided into drainage basins described as follows:

**a. Basin A (7.96 Acres)**

Basin A consists of the western portion of the development. The basin is covered with buildings, small concrete pads, aggregate all-weather access material for fire lane, and largely made up of recycled asphalt storage yard. Runoff generated from Basin A will sheet flow north and west to Monroe Street. A Mile High Flood District grass swale has been designed along the sites western boundary to provide additional water quality to the runoff from the basin. The basin is 68% impervious.

#### **b. Basin B (10.09 Acres)**

Basin B consists of an eastern portion of the bulk area of the site. The basin is covered with buildings, small concrete pads, driveways, aggregate all-weather access material for fire lane, and largely made up of recycled asphalt storage yard. Runoff generated from B will sheet flow toward a proposed infiltration pond. Flows from Basin B will infiltrate into the soil and recharge groundwater. Minimal depth grading has been proposed in order to maximize the size of Basin B and direct runoff toward the infiltration basin to the extent possible. The entire site cannot be graded toward the basin due to restrictions of cut over the existing landfill. The basin is 69% impervious.

#### **c. Basin C (1.26 Acres)**

Basin C consists generally of access to the site from Colorado Boulevard. The basin is covered with asphalt roadway, aggregate all-weather access material for fire lane, recycled asphalt storage yard. Runoff generated from Basin C will flow onto neighboring properties and the Colorado Boulevard right-of-way to match historical drainage patterns. The basin is 40% impervious.

### **C. Storage**

As the O'Brien Canal barricades the natural drainage pattern of the relatively flat existing site, conventional methods of detention and release are not feasible for the site. In order to prevent discharge of stormwater into the Canal, site drainage will be directed to a proposed infiltration pond. To prevent any overflow from the infiltration pond to the O'Brien Canal, the ponds have been sized to contain the entire 100-year runoff event (see Appendix C for site basin characteristics) with a pond capacity of 2.97 acre-ft. The 100-year water surface elevation is more than one foot below the crest of the basin, so freeboard in excess of one foot has been provided.

The surface infiltration rate of 1.0 in/hr. determined via borehole infiltration testing in the pond area has been used to determine the overall infiltration rate of the pond. The infiltration rate observed was 2.0 in/hr, but a 0.5 scale down factor applied. Given the proposed pond bottom area, the pond will infiltrate 97% the 100-year event runoff within 63.4 hours, complying the state regulation of 72 hours or less. Similarly, the pond will infiltrate 99% of the 100-year event runoff volume within 63.6 hours, in compliance with the state regulation of 120 hours or less. See Appendix C for pond volume calculations.

Water quality for Basins B and C is provided by the infiltration ponds. Water quality for Basin A is provided by the MHFD water quality swale along the site's western boundary.

### **D. Groundwater Management**

No groundwater impacts are anticipated at this time. The Infiltration Report has been provided in the report appendix.

## **VI. Conclusion**

### **A. Compliance with Standards**

This report presents the description and calculations for the drainage analysis and design of Leeper Industrial Park. The drainage system was designed in accordance with the Commerce City Storm Drainage Design and Technical Criteria and the UDFCD Urban Storm Drain Criteria Manual. As impacts to the subject site are minimal and historic drainage patterns will be maintained, the site will not have adverse effect on downstream properties.

### **B. Variances from Criteria**

No variances from applicable criteria are being requested as a part of this drainage design.

## VII. References

(2016, June). *Urban Storm Drainage Criteria Manual Volumes 1, 2, and 3*. Mile High Flood District.

(2022) *Storm Drainage Design and Technical Criteria Manual*. City of Commerce City Department of Public Works

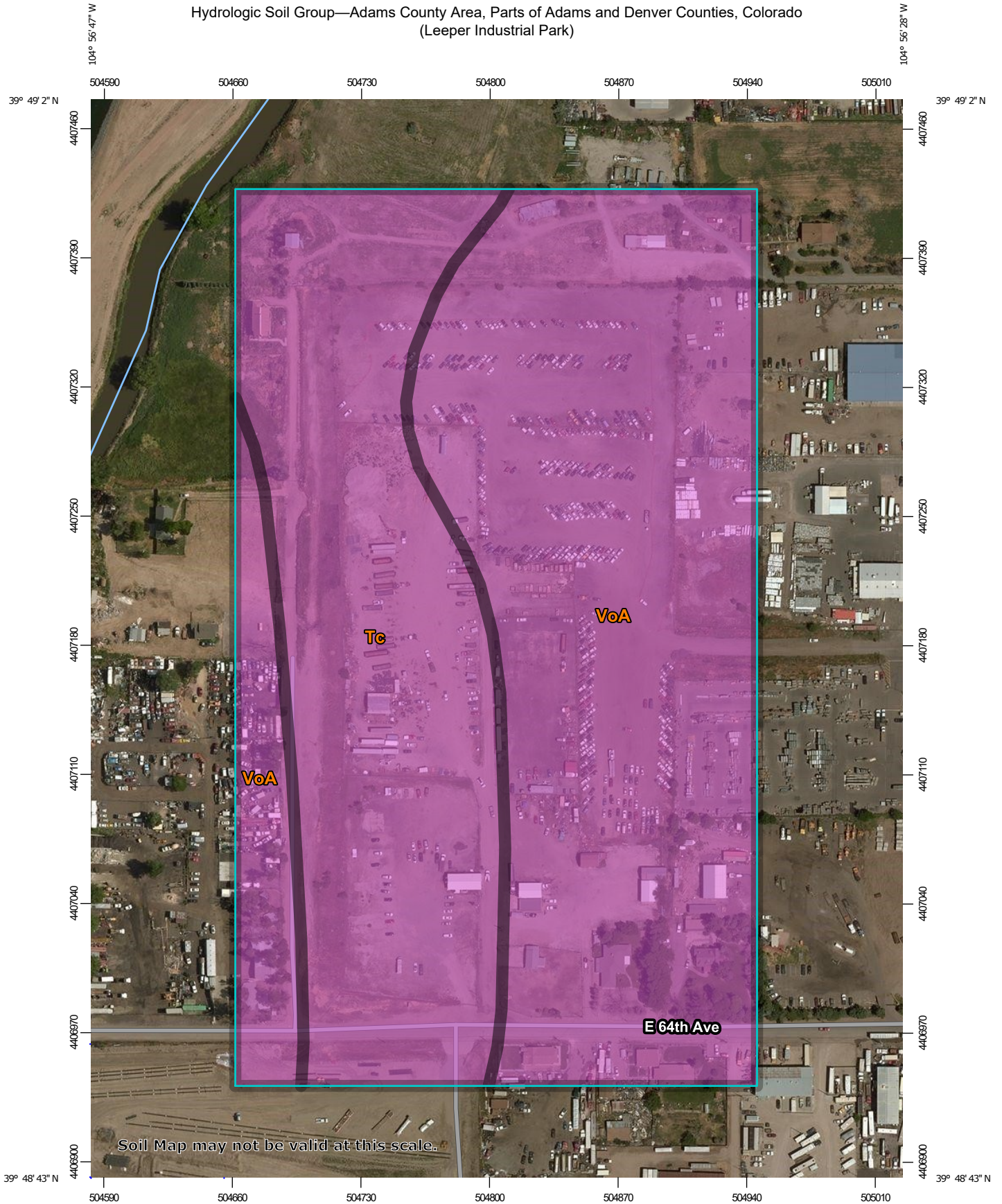


- APPENDIX A – MAPS AND SITE DESCRIPTIONS

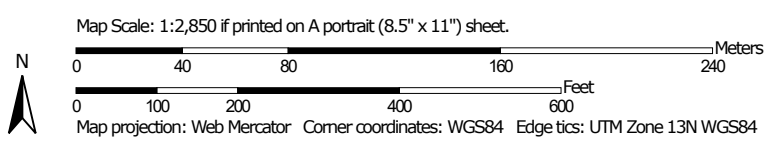




Hydrologic Soil Group—Adams County Area, Parts of Adams and Denver Counties, Colorado  
(Leeper Industrial Park)




Soil Map may not be valid at this scale.



## MAP LEGEND

### Area of Interest (AOI)









 Area of Interest (AOI)

### Soils

#### Soil Rating Polygons





 A  
 A/D  
 B  
 B/D  
 C  
 C/D  
 D  
 Not rated or not available

#### Soil Rating Lines


 A  
 A/D  
 B  
 B/D  
 C  
 C/D  
 D  
 Not rated or not available

#### Soil Rating Points






 A  
 A/D  
 B  
 B/D

 C  
 C/D  
 D  
 Not rated or not available

### Water Features

 Streams and Canals

### Transportation

 Rails  
 Interstate Highways  
 US Routes  
 Major Roads  
 Local Roads

### Background

 Aerial Photography

## MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:20,000.

**Warning:** Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
 Web Soil Survey URL:  
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Adams County Area, Parts of Adams and Denver Counties, Colorado  
 Survey Area Data: Version 15, Sep 13, 2018

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jun 10, 2014—Aug 21, 2014

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
Tc	Terrace escarpments	A	13.2	38.5%
VoA	Vona sandy loam, 0 to 1 percent slopes	A	21.1	61.5%
<b>Totals for Area of Interest</b>			<b>34.3</b>	<b>100.0%</b>

### Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

### Rating Options

*Aggregation Method:* Dominant Condition

*Component Percent Cutoff: None Specified*

*Tie-break Rule: Higher*



**POINT PRECIPITATION FREQUENCY ESTIMATES**

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

[PF\\_tabular](#) | [PF\\_graphical](#) | [Maps & aerals](#)

**PF tabular**

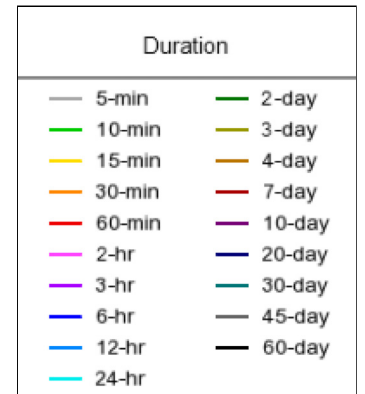
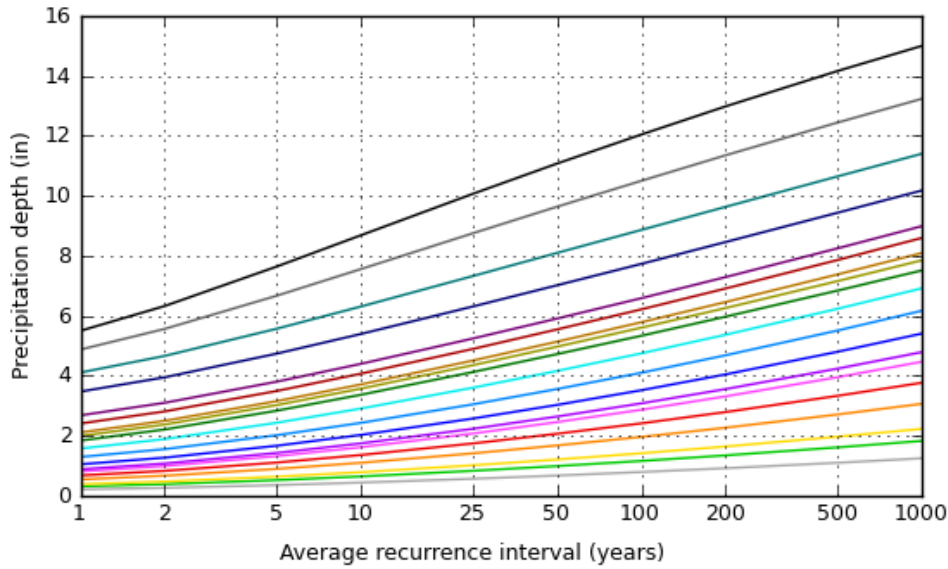
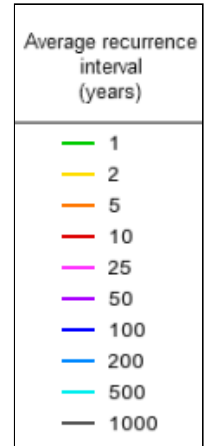
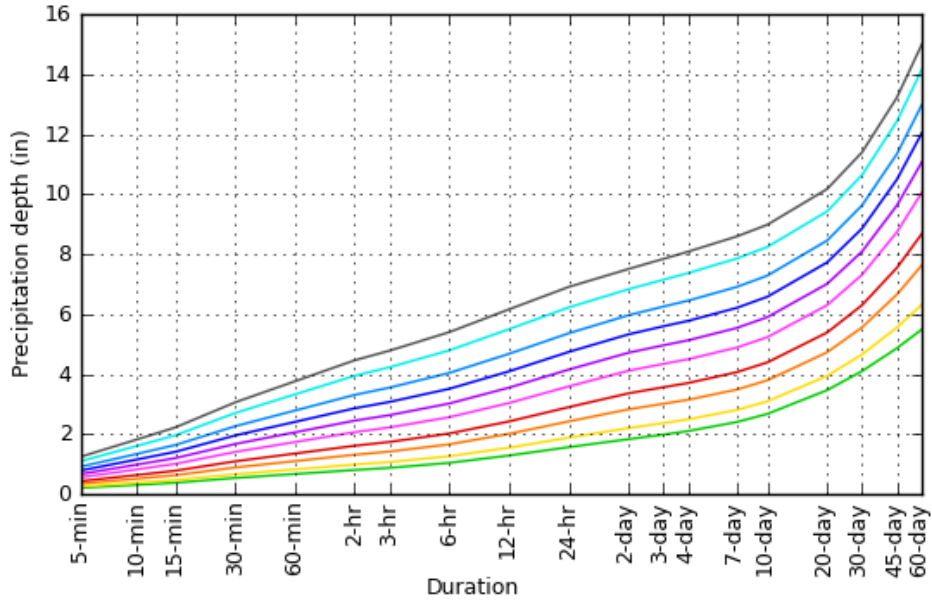
<b>PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches)<sup>1</sup></b>										
Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	0.218 (0.171-0.278)	0.268 (0.210-0.342)	0.359 (0.280-0.459)	0.443 (0.344-0.569)	0.570 (0.434-0.771)	0.678 (0.502-0.923)	0.795 (0.568-1.11)	0.922 (0.633-1.31)	1.10 (0.728-1.61)	1.25 (0.800-1.83)
10-min	0.319 (0.250-0.407)	0.392 (0.308-0.501)	0.525 (0.411-0.673)	0.648 (0.504-0.833)	0.835 (0.636-1.13)	0.993 (0.735-1.35)	1.16 (0.832-1.62)	1.35 (0.926-1.92)	1.62 (1.07-2.35)	1.83 (1.17-2.68)
15-min	0.389 (0.305-0.496)	0.478 (0.375-0.611)	0.641 (0.501-0.820)	0.790 (0.614-1.02)	1.02 (0.775-1.38)	1.21 (0.897-1.65)	1.42 (1.01-1.97)	1.65 (1.13-2.34)	1.97 (1.30-2.87)	2.23 (1.43-3.27)
30-min	0.548 (0.430-0.699)	0.673 (0.528-0.859)	0.898 (0.701-1.15)	1.10 (0.858-1.42)	1.42 (1.08-1.91)	1.68 (1.24-2.29)	1.96 (1.40-2.73)	2.27 (1.56-3.23)	2.71 (1.79-3.95)	3.07 (1.96-4.49)
60-min	0.681 (0.535-0.869)	0.834 (0.654-1.07)	1.11 (0.867-1.42)	1.36 (1.06-1.75)	1.75 (1.33-2.36)	2.07 (1.53-2.81)	2.42 (1.73-3.36)	2.79 (1.92-3.97)	3.33 (2.20-4.85)	3.77 (2.41-5.52)
2-hr	0.814 (0.645-1.03)	0.995 (0.788-1.26)	1.32 (1.04-1.68)	1.62 (1.27-2.06)	2.08 (1.59-2.77)	2.46 (1.84-3.31)	2.87 (2.07-3.94)	3.32 (2.30-4.67)	3.95 (2.63-5.69)	4.47 (2.89-6.47)
3-hr	0.885 (0.705-1.11)	1.08 (0.859-1.36)	1.43 (1.13-1.80)	1.75 (1.38-2.21)	2.23 (1.73-2.96)	2.64 (1.99-3.53)	3.08 (2.24-4.21)	3.56 (2.48-4.97)	4.24 (2.84-6.06)	4.79 (3.11-6.89)
6-hr	1.05 (0.847-1.31)	1.27 (1.02-1.58)	1.67 (1.34-2.08)	2.03 (1.62-2.54)	2.57 (2.01-3.37)	3.03 (2.30-4.00)	3.52 (2.58-4.75)	4.05 (2.85-5.59)	4.80 (3.25-6.79)	5.41 (3.55-7.69)
12-hr	1.30 (1.05-1.60)	1.56 (1.26-1.92)	2.02 (1.63-2.49)	2.43 (1.96-3.01)	3.05 (2.39-3.94)	3.56 (2.72-4.64)	4.10 (3.03-5.46)	4.68 (3.33-6.39)	5.51 (3.76-7.69)	6.17 (4.09-8.67)
24-hr	1.58 (1.29-1.92)	1.89 (1.55-2.31)	2.43 (1.99-2.97)	2.91 (2.36-3.57)	3.60 (2.85-4.58)	4.16 (3.21-5.35)	4.75 (3.54-6.23)	5.37 (3.85-7.22)	6.23 (4.30-8.58)	6.91 (4.64-9.61)
2-day	1.84 (1.53-2.22)	2.21 (1.83-2.67)	2.84 (2.34-3.43)	3.37 (2.77-4.09)	4.12 (3.28-5.16)	4.72 (3.67-5.98)	5.33 (4.01-6.90)	5.97 (4.31-7.91)	6.84 (4.76-9.28)	7.51 (5.09-10.3)
3-day	1.99 (1.66-2.39)	2.38 (1.98-2.85)	3.02 (2.51-3.63)	3.57 (2.95-4.31)	4.35 (3.48-5.41)	4.97 (3.89-6.25)	5.60 (4.24-7.20)	6.26 (4.55-8.24)	7.15 (5.01-9.64)	7.85 (5.35-10.7)
4-day	2.11 (1.77-2.52)	2.50 (2.09-2.98)	3.16 (2.63-3.77)	3.71 (3.08-4.46)	4.51 (3.62-5.58)	5.14 (4.04-6.43)	5.78 (4.40-7.40)	6.46 (4.72-8.46)	7.38 (5.19-9.90)	8.09 (5.54-11.0)
7-day	2.41 (2.04-2.85)	2.81 (2.37-3.33)	3.49 (2.94-4.14)	4.07 (3.41-4.84)	4.89 (3.97-6.00)	5.54 (4.39-6.88)	6.21 (4.76-7.87)	6.91 (5.09-8.96)	7.86 (5.57-10.4)	8.59 (5.94-11.6)
10-day	2.68 (2.28-3.15)	3.10 (2.63-3.65)	3.80 (3.21-4.48)	4.40 (3.70-5.20)	5.24 (4.27-6.38)	5.91 (4.71-7.28)	6.59 (5.08-8.29)	7.29 (5.40-9.39)	8.24 (5.88-10.9)	8.98 (6.24-12.0)
20-day	3.47 (2.98-4.04)	3.95 (3.39-4.59)	4.74 (4.05-5.52)	5.39 (4.58-6.31)	6.31 (5.19-7.57)	7.01 (5.64-8.52)	7.73 (6.02-9.59)	8.46 (6.33-10.7)	9.43 (6.80-12.3)	10.2 (7.15-13.4)
30-day	4.11 (3.55-4.74)	4.66 (4.02-5.39)	5.57 (4.78-6.44)	6.31 (5.39-7.33)	7.32 (6.05-8.71)	8.09 (6.55-9.75)	8.86 (6.94-10.9)	9.63 (7.24-12.1)	10.6 (7.71-13.7)	11.4 (8.06-14.9)
45-day	4.87 (4.23-5.59)	5.56 (4.83-6.39)	6.66 (5.77-7.67)	7.55 (6.50-8.72)	8.74 (7.26-10.3)	9.63 (7.83-11.5)	10.5 (8.26-12.8)	11.3 (8.58-14.2)	12.4 (9.06-15.9)	13.2 (9.42-17.2)
60-day	5.50 (4.80-6.28)	6.33 (5.51-7.23)	7.64 (6.63-8.74)	8.68 (7.50-9.98)	10.1 (8.37-11.8)	11.1 (9.03-13.1)	12.0 (9.50-14.6)	13.0 (9.85-16.1)	14.2 (10.3-18.0)	15.0 (10.7-19.4)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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**PF graphical**

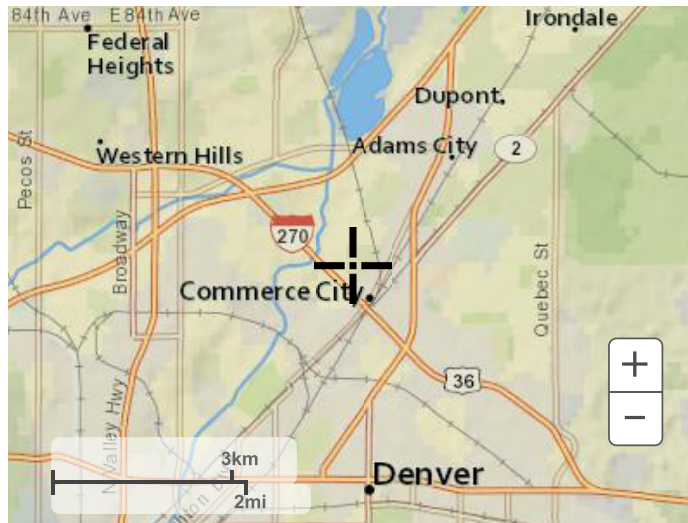
PDS-based depth-duration-frequency (DDF) curves  
 Latitude: 39.8126°, Longitude: -104.9436°



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**Maps & aerials**

Small scale terrain



Large scale terrain



Large scale map



Large scale aerial





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[US Department of Commerce](#)  
[National Oceanic and Atmospheric Administration](#)  
[National Weather Service](#)  
[National Water Center](#)  
1325 East West Highway  
Silver Spring, MD 20910  
Questions?: [HDSC.Questions@noaa.gov](mailto:HDSC.Questions@noaa.gov)

[Disclaimer](#)

# AMERICAN GEOSERVICES

Infiltration Testing Report



April 01, 2020

**PROJECT NO: 0156-D20**

CLIENT: Mr. John Draft

Reference: Infiltration Test Report, 3740 E. 64<sup>th</sup> Avenue, Commerce City, CO

Dear Mr. Draft,

At your request, we have completed the above referenced services for the referenced project in accordance with the American GeoServices, LLC (AGS) proposal. Results of our evaluation and design recommendations are described below.

**PROJECT INFORMATION**

The site is located as shown in Figure 1 and Figure 2. The parcel is located in a commercial/industrial area. The proposed development will consist of building a roadway and associated structures. We do not anticipate significant site grading (fill placement) for this project.

**INFILTRATION TESTING**

In March 2020, we performed three soil explorations at locations B1 through B3 as shown in Figure 2 as a profile borehole. In addition, three infiltration tests were performed within proximity of locations B1 through B3. Details of subsurface exploration and infiltration testing results are summarized below. Also, see attached soil borehole logs in an appendix.

**Subsurface soil conditions:** In boreholes B1 through B3, generally medium stiff to stiff sandy silts (ML) to medium dense silty sands (SM) were encountered extending to a maximum explored depth of 8 feet. A restricting or limiting layer was not noted. Groundwater table was not noted. Soil mottling suggesting or the possible indication of perched high groundwater table was not noted. It should be noted that soil classification and identification is based on commonly accepted methods employed in the practice of geotechnical engineering. In some cases, the stratigraphic boundaries shown on Boring Logs represents transitions between soil types rather than distinct lithological boundaries. It should be recognized that subsurface conditions often vary both with depth and laterally between individual boring locations.

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Colorado Springs, CO 80921  
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Pueblo, CO 81008  
Ph: (719) 761 6072

**Seasonal High Water Table:** Subsurface exploration did not reveal the presence of a seasonal high water table. No water seepage, static water table, or soil caving was noted. In our opinion, seasonal high or perched groundwater conditions may not exist within 5 feet below existing ground surface during heavy rains, throughout the site. This observation may not be indicative of other times or at locations other than the site. Some variations in the groundwater level may be experienced in the future. The magnitude of the variation will largely depend upon the duration and intensity of precipitation, temperature and the surface and subsurface drainage characteristics of the surrounding area.

**Field Infiltration Rate:** We performed three infiltration tests in general accordance with EPA test procedures and Commerce City, CO general guidelines. Following infiltration rates and results were noted in the field.

Test Location	Test Depth (Ft)	SCS Soil Description (USCS Soil Classification)	Groundwater Table (Ft)	Field Infiltration Rate (in/hr)
B1	2.0	Silt loam (ML)	Not encountered	2.5
B2	2.0	Silt loam (ML)	Not encountered	2.0
B3	2.5	Silty sandy loam (SM)	Not encountered	4.0

**Design Infiltration Rate:** The field infiltration rate should be scaled down by the factor of 0.5: Therefore, design infiltration rate =  $2.0 \times 0.5 = 1.0$  inch/hour.

**Setback:** All infiltration facilities should have a setback of 10 feet from proposed structures to minimize the adverse impact of any local mounting of groundwater table.

## LIMITATIONS

The given infiltration rates obtained in the field may vary from location to location due to variations in subsurface soil conditions. Moreover, design storm events may not accurately account for actual storm events during the design life of the drainage structures. Therefore, the potential for overflow should be considered and properly discharged into suitable receptacles in a controlled manner. All stormwater disposal systems should be designed in such a way that the groundwater quality of local aquifers is not adversely affected.

Recommendations contained in this report are based on our field observations and subsurface explorations, limited laboratory evaluation, and our present knowledge of the proposed construction. It is possible that soil conditions could vary between or beyond the points explored. If soil conditions are encountered during construction that differ from those described herein, we

should be notified so that we can review and make any supplemental recommendations necessary. If the scope of the proposed construction, including the proposed loads or structural locations, changes from that described in this report, our recommendations should also be reviewed and revised by AGS.

Local regulations regarding land or facility use, on and off-site conditions, or other factors may change over time, and additional work may be required with the passage of time. Based on the intended use of the report within one year from the date of report preparation, AGS may recommend additional work and report updates. Non-compliance with any of these requirements by the client or anyone else will release AGS from any liability resulting from the use of this report by any unauthorized party. Client agrees to defend, indemnify, and hold harmless AGS from any claim or liability associated with such unauthorized use or non-compliance.

In this report, we have presented judgments based partly on our understanding of the proposed construction and partly on the data we have obtained. This report meets professional standards expected for reports of this type in this area. Our company is not responsible for the conclusions, opinions or recommendations made by others based on the data we have presented. This report has been prepared exclusively for the client, its' engineers and subcontractors for the purpose of design and construction of the proposed structure. No other engineer, consultant, or contractor shall be entitled to rely on information, conclusions or recommendations presented in this document without the prior written approval of AGS.

We appreciate the opportunity to be of service to you on this project. If we can provide additional assistance or observation and testing services during design and construction phases, please call us at 1 888 276 4027.

Sincerely,



Sam Adettiwar, MS, PE, GE, P.Eng, M.ASCE  
Senior Engineer  
Attachments



NOTE:  
SCHEMATIC PLAN TO SHOW APPROXIMATE SUBSURFACE EXPLORATION LOCATION ONLY; NOT SURVEYED.

LEGEND:  
 DESIGNATES INFILTRATION TEST LOCATION, BY AMERICAN GEOSERVICES, LLC., MARCH 2020 SEE EXPLORATION LOG IN APPENDIX FOR FURTHER DETAILS.

REFERENCE:  
LEEPER INDUSTRIAL  
PARK DEVELOPMENT  
PLAN



FIGURE 2: SCHEMATIC SITE PLAN



- APPENDIX B – HYDROLOGIC CALCUATIONS

## Drainage Basin Imperviousness

Soil Type : A

Imperviousness :	Roof	Concrete	Recycled Asphalt	Asphalt	Playground	Gravel	Undeveloped						
	90%	90%	89%	100%	10%	40%	2%	Total Area	Composite	Runoff Coefficients			
Basin Name	Areas (sq.ft.)							(sq.ft.)	% Imp.	C <sub>2</sub>	C <sub>5</sub>	C <sub>10</sub>	C <sub>100</sub>
EX-A	3,556	4,832	294,715	1,234			98,423	402,760	68%	0.51	0.52	0.54	0.64
EX-B	8,024	645	373,790	3,746			31,763	417,968	83%	0.65	0.67	0.69	0.75
EX-C			29,704	17,121			24,645	71,470	62%	0.45	0.46	0.48	0.59
<b>Total Existing</b>	<b>11,580</b>	<b>5,477</b>		<b>22,101</b>			<b>154,831</b>	<b>892,198</b>	<b>5%</b>	<b>0.02</b>	<b>0.02</b>	<b>0.02</b>	<b>0.15</b>
A	3,556	4,400	234,002	1,234			103,574	346,766	63%	0.46	0.48	0.49	0.60
B	8,024	419	325,726	2,846			102,719	439,734	69%	0.52	0.53	0.55	0.65
C			20,520	2,990			31,638	55,148	40%	0.25	0.26	0.28	0.42
<b>Total Proposed</b>	<b>11,580</b>	<b>4,819</b>	<b>580,248</b>	<b>7,070</b>			<b>237,931</b>	<b>841,648</b>	<b>65%</b>	<b>0.47</b>	<b>0.49</b>	<b>0.51</b>	<b>0.61</b>



### SF2 - Time of Concentration

Basin ID	Area (AC.)	C <sub>s</sub>	Initial/Overland Time			Travel Time					Time of Concentration		Final
			L <sub>i</sub> (ft.)	S (%)	T <sub>i</sub> (min.)	L <sub>t</sub> (ft.)	S (%)	Conveyance Factor	Vel (fps)	T <sub>t</sub> (min.)	Comp. T <sub>c</sub> (min.)	Regional T <sub>c</sub> (Min.)	T <sub>c</sub> (Min.)
EX-A	9.25	0.52	373	0.50	25.3	559	1.2	10	1.1	8.5	33.8	19.1	19.1
EX-B	9.60	0.67	500	0.50	21.7	121	0.7	10	0.8	2.4	24.1	13.1	13.1
EX-C	1.64	0.46	17	2.00	3.8	227	0.5	15	1.1	3.6	7.3	18.6	7.3
A	7.96	0.48	373	0.50	27.3	559	1.2	10	1.1	8.5	35.8	20.0	20.0
B	10.09	0.53	500	0.50	28.8	121	0.7	10	0.8	2.4	31.2	15.6	15.6
C	1.27	0.26	17	2.00	4.9	227	0.5	15	1.1	3.6	8.5	22.9	8.5

Project : Leeper Industrial Park  
 Project No. : 21087

Date : 4/27/2022  
 By : JGD

### SF<sub>3</sub> - Minor Storm

1-hr Point Rainfall **0.83** in. (2-year Event)

Description	Design Point	Direct Runoff						Total Runoff				Street		Travel Time			Comments
		Area (ac.)	C <sub>s</sub>	Tc (min.)	CA (ac.)	I (in/hr)	Q (cfs)	Tc (min.)	CA (ac.)	I (in/hr)	Q (cfs)	Slope (%)	Flow (cfs)	Length (ft)	Vel. (fps)	tt (min.)	
EX-A		9.25	0.52	19.1	4.8	1.67	8.10										
EX-B		9.60	0.67	13.1	6.5	2.00	12.93										
EX-C		1.64	0.46	7.3	0.8	2.51	1.91										
<b>Total</b>		<b>20.48</b>					<b>22.94</b>										
A		7.96	0.48	20.0	3.8	1.63	6.20										
B		10.09	0.53	15.6	5.4	1.85	9.96										
C		1.27	0.26	8.5	0.3	2.39	0.80										
<b>Total</b>		<b>19.32</b>					<b>16.96</b>										

### SF<sub>3</sub> - Minor Storm

1-hr Point Rainfall **1.11** in. (5-year Event)

Description	Design Point	Direct Runoff						Total Runoff				Street		Travel Time			Comments
		Area (ac.)	C <sub>s</sub>	T <sub>c</sub> (min.)	CA (ac.)	I (in/hr)	Q (cfs)	T <sub>c</sub> (min.)	CA (ac.)	I (in/hr)	Q (cfs)	Slope (%)	Flow (cfs)	Length (ft)	Vel. (fps)	tt (min.)	
EX-A		9.25	0.52	19.1	4.8	2.24	10.84										
EX-B		9.60	0.67	13.1	6.5	2.68	17.29										
EX-C		1.64	0.46	7.3	0.8	3.36	2.56										
<b>Total</b>		<b>20.48</b>					<b>30.68</b>										
A		7.96	0.48	20.0	3.8	2.18	8.29										
B		10.09	0.53	15.6	5.4	2.47	13.32										
C		1.27	0.26	8.5	0.3	3.19	1.07										
<b>Total</b>		<b>19.32</b>					<b>22.68</b>										

### SF3 - Major Storm

1-hr Point Rainfall **2.42** in. (100-year Event)

Description	Design Point	Direct Runoff						Total Runoff				Street		Travel Time			Comments
		Area (ac.)	C <sub>100</sub>	Tc (min.)	CA (ac.)	I (in/hr)	Q (cfs)	Tc (min.)	CA (ac.)	I (in/hr)	Q (cfs)	Slope (%)	Flow (cfs)	Length (ft)	Vel. (fps)	tt (min.)	
EX-A		9.25	0.64	19.1	5.9	4.88	28.82										
EX-B		9.60	0.75	13.1	7.2	5.84	42.20										
EX-C		1.64	0.59	7.3	1.0	7.33	7.10										
<b>Total</b>		<b>20.48</b>					<b>78.12</b>										
A		7.96	0.60	20.0	4.8	4.75	22.79										
B		10.09	0.65	15.6	6.5	5.39	35.18										
C		1.27	0.42	8.5	0.5	6.96	3.69										
<b>Total</b>		<b>19.32</b>					<b>61.66</b>										

- APPENDIX C – INFILTRATION BASIN CALCULATIONS



Project : Leeper Industrial Park  
Project No. : 21087

Calculated By : JGD  
Date : 4/27/2022

### Pond Volume by Contour Area

Contour Elevation	Areas (sq.ft.)	Area (Acre)	Volume (ft <sup>3</sup> )	Cumulative Volume (ac-ft)
5138	19,156	0.44	0	0.00
5139	21,729	0.50	20,429	0.47
5140	24,402	0.56	43,482	1.00
5141	27,176	0.62	69,258	1.59
5142	30,056	0.69	97,862	2.25
5143	33,025	0.76	129,391	2.97

## Design Procedure Form: Grass Swale (GS)

UD-BMP (Version 3.07, March 2018)

Sheet 1 of 1

**Designer:** Jason DeYoung  
**Company:** Proof Civil Consulting Engineers  
**Date:** July 22, 2022  
**Project:** Leeper Industrial Park  
**Location:** 64th Avenue & Monroe Street

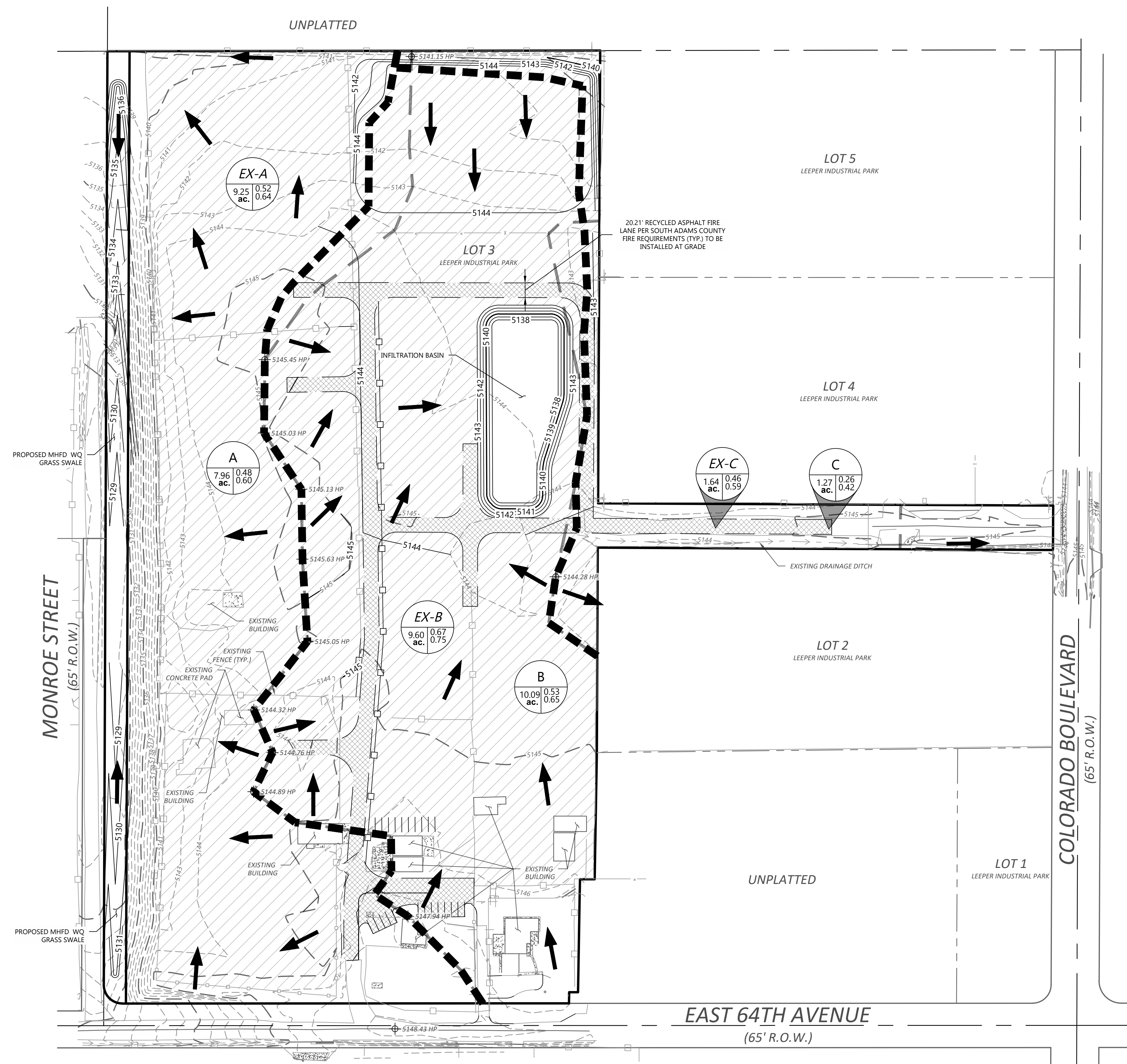
1. Design Discharge for 2-Year Return Period	$Q_2 = $ <input style="width: 50px;" type="text" value="5.54"/> cfs
2. Hydraulic Residence Time A) : Length of Grass Swale B) Calculated Residence Time (based on design velocity below)	$L_S = $ <input style="width: 50px;" type="text" value="285.0"/> ft $T_{HR} = $ <input style="width: 50px;" type="text" value="4.8"/> minutes
3. Longitudinal Slope (vertical distance per unit horizontal) A) Available Slope (based on site constraints) B) Design Slope	$S_{avail} = $ <input style="width: 50px;" type="text" value="0.008"/> ft / ft $S_D = $ <input style="width: 50px;" type="text" value="0.007"/> ft / ft
4. Swale Geometry A) Channel Side Slopes (Z = 4 min., horiz. distance per unit vertical) B) Bottom Width of Swale (enter 0 for triangular section)	$Z = $ <input style="width: 50px;" type="text" value="16.00"/> ft / ft $W_B = $ <input style="width: 50px;" type="text" value="0.00"/> ft
5. Vegetation A) Type of Planting (seed vs. sod, affects vegetal retardance factor)	<div style="border: 1px solid black; padding: 5px;">                 Choose One <span style="float: right;">_____</span>  <input checked="" type="radio"/> Grass From Seed    <input type="radio"/> Grass From Sod             </div>
6. Design Velocity (0.95 ft / s maximum for desirable 5-minute residence time)	$V_2 = $ <input style="width: 50px;" type="text" value="0.99"/> ft / s
7. Design Flow Depth (1 foot maximum) A) Flow Area B) Top Width of Swale C) Froude Number (0.50 maximum) D) Hydraulic Radius E) Velocity-Hydraulic Radius Product for Vegetal Retardance F) Manning's n (based on SCS vegetal retardance curve E for seeded grass) G) Cumulative Height of Grade Control Structures Required	$D_2 = $ <input style="width: 50px;" type="text" value="0.59"/> ft $A_2 = $ <input style="width: 50px;" type="text" value="5.6"/> sq ft $W_T = $ <input style="width: 50px;" type="text" value="18.9"/> ft $F = $ <input style="width: 50px;" type="text" value="0.32"/> $R_H = $ <input style="width: 50px;" type="text" value="0.29"/> $VR = $ <input style="width: 50px;" type="text" value="0.29"/> $n = $ <input style="width: 50px;" type="text" value="0.055"/> $H_D = $ <input style="width: 50px;" type="text" value="0.10"/> ft
8. Underdrain (Is an underdrain necessary?)	<div style="border: 1px solid black; padding: 5px;">                 Choose One <span style="float: right;">_____</span>  <input checked="" type="radio"/> YES    <input type="radio"/> NO             </div> <div style="text-align: right; font-size: small; color: blue; margin-top: 5px;"> <b>AN UNDERDRAIN IS REQUIRED IF THE DESIGN SLOPE &lt; 2.0%</b> </div>
9. Soil Preparation (Describe soil amendment)	_____ _____ _____
10. Irrigation	<div style="border: 1px solid black; padding: 5px;">                 Choose One <span style="float: right;">_____</span>  <input checked="" type="radio"/> Temporary    <input type="radio"/> Permanent             </div>

Notes: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_





- APPENDIX D – DRAINAGE PLAN



**LEGEND:**

- PROPERTY LINE
- ▨ PROPOSED BUILDING
- ▨ EXISTING BUILDING
- - - PROPOSED EASEMENT
- - - EXISTING EASEMENT
- ▬ PROPOSED BASIN BOUNDARY
- ▬ HISTORICAL BASIN BOUNDARY
- 5400 — PROPOSED 5' CONTOUR
- 5401 — PROPOSED 1' CONTOUR
- - - 5400 - - - EXISTING 5' CONTOUR
- - - 5401 - - - EXISTING 1' CONTOUR
- ▨ PROPOSED RECYCLED ASPHALT PAVEMENT
- XSD — EXISTING STORM LINE W/F.E.S.
- FLOW DIRECTION
- ⊕ 25.25 PROPOSED SPOT GRADE
- ⊕ 25.25 EXISTING SPOT GRADE
- ↘ 2.00% SLOPE AND DIRECTION
- HP HIGH POINT
- LP LOW POINT
- GB GRADE BREAK

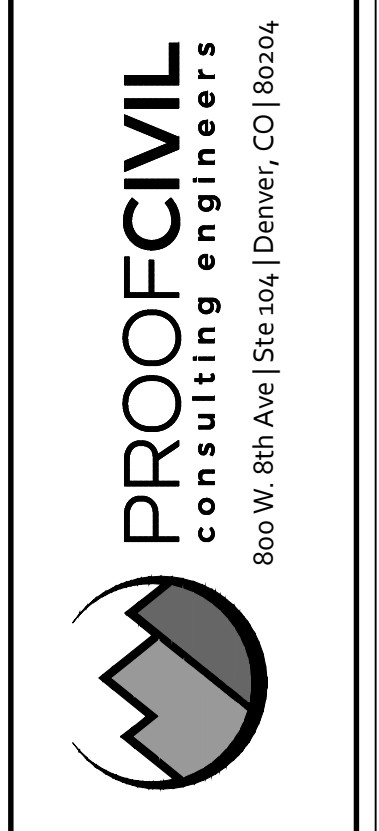
**BASIN ID**

**BASIN IDENTIFICATION TAG**

**BASIN ACREAGE**

**5-YR RUNOFF COEFFICIENT**

**100-YR RUNOFF COEFFICIENT**



SEAL:

FOR AND ON BEHALF OF PROOF CIVIL CO.

REVISIONS		NO.	DATE	DESCRIPTION
PROJ. NO.:	21087			
DATE:	4/30/19			
DRAWN BY:	MRR			
CHECKED BY:	JGD			

**DRAINAGE PLAN**

**LEEPER INDUSTRIAL PARK**

**COLORADO**

**COMMERCE CITY**

DRAWING NO.

**DRN-1**