Final Drainage Report

Leeper Industrial Park

(**JN: 21087)**

3700 E. 64th Avenue Commerce City, CO

April 27, 2022 Revised: July 22, 2022 Revised: August 18, 2022

Prepared for:

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<u>Certification</u>

ENGINEER CERTIFICATION OF DRAINAGE REPORT

or under my direct supervision in accorda	the Preliminary Drainage design of Leeper Industrial Park was prepared by me ince with the provisions of Commerce City Storm Drainage Design and I understand that Commerce City does not and will not assume liability for
Date	
Registered Professional Engineer State of Colorado PE No. 45332 For and on behalf of Proof Civil Co.	

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I. Introduction

This final drainage report for Leeper Industrial Park will address the on-site stormwater conveyance and treatment for the development in accordance with criteria set forth by applicable governing agencies as well as previously approved relevant drainage studies.

II. General Location and Description

A. Project Location

The subject property is a 20.08 industrial facility located at 3700 E. 64th Avenue in Commerce City, Colorado. The property consists of Lot 3, and a previously unplatted parcel in the Leeper Industrial Park Subdivision. The property is bound to the west by Monroe Street, to the north by an unplatted parcel, to the east by other lots within the Leeper Industrial Park Subdivision and Colorado Boulevard, and to the south by East 64th Avenue.

B. Project Description

The property is an existing industrial facility with two offices, auxillary buildings, storage yard area, and associated drivelanes. Aside from the existing buildings, the groundcover of the property consists largely of existing recycled asphalt. A significant portion of the site (approximately 60% of the site area) along the western boundary lies on a buried inactive landfill. The site contains permanent and temporary easements for energy pipeline purposes. No wetlands are known to exist onsite.

C. Floodplain Information

According to FEMA Flood Insurance Rate Map Panel #08001C0604H, the subject site is located within flood hazard area Zone X. Zone X is defined as area outside the 0.2-percent-chance (or 500-year) flood. Refer to Appendix A for the applicable FEMA flood map.

D. Soils Description

According to the United States Department of Agriculture Natural Resources Conservation Service (NRCS) National Cooperative Soil Survey, onsite soils are identified as Terrace Escarpments and Vona Sandy Loam and are classified as Hydrologic Soil Group A. Group A is sand, loamy sand or sandy loam types of soils. It has low runoff potential and high infiltration rates even when thoroughly wetted. They consist chiefly of deep, well to excessively drained sands or gravels and have a high rate of water transmission. See Appendix A for the site soil map.

III. Historic Drainage

A. Existing Drainage Pattern

The site generally drains from south to north and west to east at a general slope of 0.5%. Flows are then generally conveyed to Monroe Street, and eventually to the O'Brien Canal in the existing condition. The site is covered by compacted earth with little vegetation.

B. Existing Basins

The existing site is divided into drainage basins described as follows:

a. Basin EX-A (9.25 Acres)

Basin EX-A consists of the western portion of the development. The basin is covered with buildings, small concrete pads, and largely made up of recycled earth storage area and undeveloped slope down to Monroe Street. Runoff generated from Basin EX-A sheet flows north and west to Monroe Street. The existing basin is 68% impervious.

b. Basin EX-B (9.60 Acres)

Basin EX-B consists of an eastern portion of the bulk area of the site. The basin is covered with buildings, small concrete pads, driveways, and largely made up of recycled asphalt storage yard. Runoff generated from Basin EX-B sheet flows north and east to a low point within the site. Flows either percolate into the soil at this location or overflow into Basin EX-A. The existing basin is 83% impervious.

c. Basin EX-C (1.64 Acres)

Basin EX-C consists generally of access to the site from Colorado Boulevard. The basin is covered with asphalt roadway and recycled asphalt storage yard. Runoff generated from Basin EX-C flows onto neighboring properties and the Colorado Boulevard right-of-way. The existing basin is 62% impervious.

IV. Drainage Criteria

A. Regulation

Methods described in the UDFCD Urban Storm Drainage Criteria Manual and in the Commerce City Storm Drainage Design and Technical Criteria were used for the drainage design of the Site.

B. Hydrology

The Rational Method analysis, utilizing the Intensity-Duration-Frequency curves for the area established by the National Oceanic and Atmospheric Administration was used to determine the on-site runoff generated for the 5-year (minor), and 100-year (major) storm events. Runoff coefficients were based on the type of proposed development outlined in the UDFCD manual. Runoff coefficients used in the analysis were weighted according to the existing and proposed land uses in each basin or sub-basin and the time of concentration values have been calculated for each of the basins or sub-basins per Urban Drainage criteria. Detention storage and release rate have been calculated using the UDFCD full-spectrum design criteria. Hydrologic calculations can be found in Appendix B.

V. Drainage Design

A. General Concept

Proposed on-site drainage design will follow historical drainage patterns. The site will not be altered in any way with the exception of the addition of fresh recycled asphalt for some storage areas and the introduction of an infiltration pond.

B. Proposed Drainage Basins

The improved site is divided into drainage basins described as follows:

a. Basin A (7.96 Acres)

Basin A consists of the western portion of the development. The basin is covered with buildings, small concrete pads, aggregate all-weather access material for fire lane, and largely made up of recycled asphalt storage yard. Runoff generated from Basin A will sheet flow north and west to Monroe Street. A Mile High Flood District grass swale has been designed along the sites western boundary to provide additional water quality to the runoff from the basin. The basin is 68% impervious.

b. Basin B (10.09 Acres)

Basin B consists of an eastern portion of the bulk area of the site. The basin is covered with buildings, small concrete pads, driveways, aggregate all-weather access material for fire lane, and largely made up of recycled asphalt storage yard. Runoff generated from B will sheet flow toward a proposed infiltration pond. Flows from Basin B will infiltrate into the soil and recharge groundwater. Minimal depth grading has been proposed in order to maximize the size of Basin B and direct runoff toward the infiltration basin to the extent possible. The entire site cannot be graded toward the basin due to restrictions of cut over the existing landfill. The basin is 69% impervious.

c. Basin C (1.26 Acres)

Basin C consists generally of access to the site from Colorado Boulevard. The basin is covered with asphalt roadway, aggregate all-weather access material for fire lane, recycled asphalt storage yard. Runoff generated from Basin C will flow onto neighboring properties and the Colorado Boulevard right-of-way to match historical drainage patterns. The basin is 40% impervious.

C. Storage

As the O'Brien Canal barricades the natural drainage pattern of the relatively flat existing site, conventional methods of detention and release are not feasible for the site. In order to prevent discharge of stormwater into the Canal, site drainage will be directed to a proposed infiltration pond. To prevent any overflow from the infiltration pond to the O'Brien Canal, the ponds have been sized to contain the entire 100-year runoff event (see Appendix C for site basin characteristics) with a pond capacity of 2.97 acre-ft. The 100-year water surface elevation is more than one foot below the crest of the basin, so freeboard in excess of one foot has been provided.

The surface infiltration rate of 1.0 in/hr. determined via borehole infiltration testing in the pond area has been used to determine the overall infiltration rate of the pond. The infiltration rate observed was 2.0 in/hr, but a 0.5 scale down factor applied. Given the proposed pond bottom area, the pond will infiltrate 97% the 100-year event runoff within 63.4 hours, complying the state regulation of 72 hours or less. Similarly, the pond will infiltrate 99% of the 100-year event runoff volume within 63.6 hours, in compliance with the state regulation of 120 hours or less. See Appendix C for pond volume calculations.

Water quality for Basins B and C is provided by the infiltration ponds. Water quality for Basin A is provided by the MHFD water quality swale along the site's western boundary.

D. Groundwater Management

No groundwater impacts are anticipated at this time. The Infiltration Report has been provided in the report appendix.

VI. Conclusion

A. Compliance with Standards

This report presents the description and calculations for the drainage analysis and design of Leeper Industrial Park. The drainage system was designed in accordance with the Commerce City Storm Drainage Design and Technical Criteria and the UDFCD Urban Storm Drain Criteria Manual. As impacts to the subject site are minimal and historic drainage patterns will be maintained, the site will not have adverse effect on downstream properties.

B. Variances from Criteria

No variances from applicable criteria are being requested as a part of this drainage design.

VII. References

(2016, June). *Urban Storm Drainage Criteria Manual Volumes* 1, 2, and 3. Mile High Flood District.

(2022) Storm Drainage Design and Technical Criteria Manual. City of Commerce City Department of Public Works



NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD 88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by flood control structures. Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NAD83, GRS1980 spheroid. Differences in datum, spheroid, projection or UTM zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988. These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at http://www.ngs.noaa.gov/ or contact the National Geodetic Survey at the following address:

NGS Information Services NOAA, N/NGS12 National Geodetic Survey SSMC- 3, #9202 1315 East- West Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242, or visit its website at http://www.ngs.noaa.gov/.

Base map information shown on this FIRM was provided by the Adams County and Commerce City GIS departments. The coordinate system used for the production of the digital FIRM is Universe Transverse Mercator, Zone 13N, referenced to North American Datum of 1983 and the GRS 80 spheroid, Western Hemisphere.

This map reflects more detailed and up-to-date stream channel configurations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result. the Flood Profiles and Floodway Data tables in the Flood Insurance Study report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact

Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each

Contact the FEMA Map Service Center at 1-800-358-9616 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study report, and/or digital versions of this map. The FEMA Map Service Center may also be reached by Fax at 1-800-358-9620 and its website at http://www.msc.fema.gov/.

If you have questions about this map or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or visit the FEMA website at http://www.fema.gov/.

This digital Flood Insurance Rate Map (FIRM) was produced through a cooperative partnership between the State of Colorado Water Conservation Board, the Urban Drainage and Flood Control District, and the Federal Emergency Management Agency (FEMA). The State of Colorado Water Conservation Board and the Urban Drainage and Flood Control District have implemented a long-term approach of floodplain management to reduce the costs associated with flooding. As part of this effort, both the State of Colorado and the Urban Drainage and Flood Control District have joined in Cooperating Technical Partner agreements with FEMA to produce this digital FIRM.

Additional flood hazard information and resources are available from local communities, the Colorado Water Conservation Board, and the Urban Drainage and







LEGEND SPECIAL FLOOD HAZARD AREAS (SFHAs) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood. **ZONE A** No Base Flood Elevations determined. ZONE AE Base Flood Elevations determined. Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined. Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities Special Flood Hazard Area formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined. Coastal flood zone with velocity hazard (wave action); Base FLOODWAY AREAS IN ZONE AE The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights. OTHER FLOOD AREAS Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance OTHER AREAS Areas determined to be outside the 0.2% annual chance floodplain. Areas in which flood hazards are undetermined, but possible. COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS OTHERWISE PROTECTED AREAS (OPAs) CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas. Floodplain boundary Floodway boundary Zone D boundary •••••• CBRS and OPA boundary Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities. ~~~~ 513 ~~~~~ Base Flood Elevation line and value; elevation in feet* Base Flood Elevation value where uniform within zone; elevation in feet* * Referenced to the North American Vertical Datum of 1988 (NAVD 88) (23)- - - - - - - - (23) Geographic coordinates referenced to the North American 97°07'30", 32°22'30" Datum of 1983 (NAD 83) 1000-meter Universal Transverse Mercator grid ticks, zone 13 5000-foot grid ticks: Alabama State Plane coordinate system, east zone (FIPSZONE 0101), Transverse Mercator Bench mark (see explanation in Notes to Users section of MAP REPOSITORIES Refer to Map Repositories list on Map Index EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP August 16, 1995 EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL March 5, 2007 - to update map format For community map revision history prior to countywide mapping, refer to the Community Map History table located in the Flood Insurance Study report for this jurisdiction. To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620. PANEL 0604H **FIRM** FLOOD INSURANCE RATE MAP ADAMS COUNTY, COLORADO AND INCORPORATED AREAS **PANEL 604 OF 1150** (SEE MAP INDEX FOR FIRM PANEL LAYOUT) **CONTAINS: COMMUNITY** ADAMS COUNTY COMMERCE CITY, CITY OF 080006 THORNTON, CITY OF 080007 Notice to User: The Map Number shown below should be used when placing map orders; the **Community Number** shown above should be used on insurance applications for the subject APATETONAPATE



Federal Emergency Management Agency

MAP NUMBER 08001C0604H

MAP REVISED

MARCH 5. 2007



MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:20.000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D **Soil Rating Polygons** Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil **Water Features** line placement. The maps do not show the small areas of A/D contrasting soils that could have been shown at a more detailed Streams and Canals Transportation B/D Rails ---Please rely on the bar scale on each map sheet for map measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available -Local Roads Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. Soil Survey Area: Adams County Area, Parts of Adams and Denver Counties, Colorado Survey Area Data: Version 15, Sep 13, 2018 Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. Not rated or not available Date(s) aerial images were photographed: Jun 10, 2014—Aug **Soil Rating Points** 21, 2014 The orthophoto or other base map on which the soil lines were A/D compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. B/D

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
Tc	Terrace escarpments	A	13.2	38.5%
VoA	Vona sandy loam, 0 to 1 percent slopes	А	21.1	61.5%
Totals for Area of Intere	est		34.3	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher



NOAA Atlas 14, Volume 8, Version 2 Location name: Commerce City, Colorado, USA* Latitude: 39.8126°, Longitude: -104.9436° Elevation: m/ft**

* source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials

PF tabular

PDS	-based po	int precip	itation fre	quency es	stimates v	vith 90% c	onfidenc	e interva	als (in inc	hes) ¹
Duration				Average	recurrence	interval (ye	ars)			
Daration	1	2	5	10	25	50	100	200	500	1000
5-min	0.218 (0.171-0.278)	0.268 (0.210-0.342)	0.359 (0.280-0.459)	0.443 (0.344-0.569)	0.570 (0.434-0.771)	0.678 (0.502-0.923)	0.795 (0.568-1.11)	0.922 (0.633-1.31)	1.10 (0.728-1.61)	1.25 (0.800-1.83)
10-min	0.319 (0.250-0.407)	0.392 (0.308-0.501)	0.525 (0.411-0.673)	0.648 (0.504-0.833)	0.835 (0.636-1.13)	0.993 (0.735-1.35)	1.16 (0.832-1.62)	1.35 (0.926-1.92)	1.62 (1.07-2.35)	1.83 (1.17-2.68)
15-min	0.389 (0.305-0.496)	0.478 (0.375-0.611)	0.641 (0.501-0.820)	0.790 (0.614-1.02)	1.02 (0.775-1.38)	1.21 (0.897-1.65)	1.42 (1.01-1.97)	1.65 (1.13-2.34)	1.97 (1.30-2.87)	2.23 (1.43-3.27)
30-min	0.548 (0.430-0.699)	0.673 (0.528-0.859)	0.898 (0.701-1.15)	1.10 (0.858-1.42)	1.42 (1.08-1.91)	1.68 (1.24-2.29)	1.96 (1.40-2.73)	2.27 (1.56-3.23)	2.71 (1.79-3.95)	3.07 (1.96-4.49)
60-min	0.681 (0.535-0.869)	0.834 (0.654-1.07)	1.11 (0.867-1.42)	1.36 (1.06-1.75)	1.75 (1.33-2.36)	2.07 (1.53-2.81)	2.42 (1.73-3.36)	2.79 (1.92-3.97)	3.33 (2.20-4.85)	3.77 (2.41-5.52)
2-hr	0.814 (0.645-1.03)	0.995 (0.788-1.26)	1.32 (1.04-1.68)	1.62 (1.27-2.06)	2.08 (1.59-2.77)	2.46 (1.84-3.31)	2.87 (2.07-3.94)	3.32 (2.30-4.67)	3.95 (2.63-5.69)	4.47 (2.89-6.47)
3-hr	0.885 (0.705-1.11)	1.08 (0.859-1.36)	1.43 (1.13-1.80)	1.75 (1.38-2.21)	2.23 (1.73-2.96)	2.64 (1.99-3.53)	3.08 (2.24-4.21)	3.56 (2.48-4.97)	4.24 (2.84-6.06)	4.79 (3.11-6.89)
6-hr	1.05 (0.847-1.31)	1.27 (1.02-1.58)	1.67 (1.34-2.08)	2.03 (1.62-2.54)	2.57 (2.01-3.37)	3.03 (2.30-4.00)	3.52 (2.58-4.75)	4.05 (2.85-5.59)	4.80 (3.25-6.79)	5.41 (3.55-7.69)
12-hr	1.30 (1.05-1.60)	1.56 (1.26-1.92)	2.02 (1.63-2.49)	2.43 (1.96-3.01)	3.05 (2.39-3.94)	3.56 (2.72-4.64)	4.10 (3.03-5.46)	4.68 (3.33-6.39)	5.51 (3.76-7.69)	6.17 (4.09-8.67)
24-hr	1.58 (1.29-1.92)	1.89 (1.55-2.31)	2.43 (1.99-2.97)	2.91 (2.36-3.57)	3.60 (2.85-4.58)	4.16 (3.21-5.35)	4.75 (3.54-6.23)	5.37 (3.85-7.22)	6.23 (4.30-8.58)	6.91 (4.64-9.61)
2-day	1.84 (1.53-2.22)	2.21 (1.83-2.67)	2.84 (2.34-3.43)	3.37 (2.77-4.09)	4.12 (3.28-5.16)	4.72 (3.67-5.98)	5.33 (4.01-6.90)	5.97 (4.31-7.91)	6.84 (4.76-9.28)	7.51 (5.09-10.3)
3-day	1.99 (1.66-2.39)	2.38 (1.98-2.85)	3.02 (2.51-3.63)	3.57 (2.95-4.31)	4.35 (3.48-5.41)	4.97 (3.89-6.25)	5.60 (4.24-7.20)	6.26 (4.55-8.24)	7.15 (5.01-9.64)	7.85 (5.35-10.7)
4-day	2.11 (1.77-2.52)	2.50 (2.09-2.98)	3.16 (2.63-3.77)	3.71 (3.08-4.46)	4.51 (3.62-5.58)	5.14 (4.04-6.43)	5.78 (4.40-7.40)	6.46 (4.72-8.46)	7.38 (5.19-9.90)	8.09 (5.54-11.0)
7-day	2.41 (2.04-2.85)	2.81 (2.37-3.33)	3.49 (2.94-4.14)	4.07 (3.41-4.84)	4.89 (3.97-6.00)	5.54 (4.39-6.88)	6.21 (4.76-7.87)	6.91 (5.09-8.96)	7.86 (5.57-10.4)	8.59 (5.94-11.6)
10-day	2.68 (2.28-3.15)	3.10 (2.63-3.65)	3.80 (3.21-4.48)	4.40 (3.70-5.20)	5.24 (4.27-6.38)	5.91 (4.71-7.28)	6.59 (5.08-8.29)	7.29 (5.40-9.39)	8.24 (5.88-10.9)	8.98 (6.24-12.0)
20-day	3.47 (2.98-4.04)	3.95 (3.39-4.59)	4.74 (4.05-5.52)	5.39 (4.58-6.31)	6.31 (5.19-7.57)	7.01 (5.64-8.52)	7.73 (6.02-9.59)	8.46 (6.33-10.7)	9.43 (6.80-12.3)	10.2 (7.15-13.4)
30-day	4.11 (3.55-4.74)	4.66 (4.02-5.39)	5.57 (4.78-6.44)	6.31 (5.39-7.33)	7.32 (6.05-8.71)	8.09 (6.55-9.75)	8.86 (6.94-10.9)	9.63 (7.24-12.1)	10.6 (7.71-13.7)	11.4 (8.06-14.9)
45-day	4.87 (4.23-5.59)	5.56 (4.83-6.39)	6.66 (5.77-7.67)	7.55 (6.50-8.72)	8.74 (7.26-10.3)	9.63 (7.83-11.5)	10.5 (8.26-12.8)	11.3 (8.58-14.2)	12.4 (9.06-15.9)	13.2 (9.42-17.2)
60-day	5.50 (4.80-6.28)	6.33 (5.51-7.23)	7.64 (6.63-8.74)	8.68 (7.50-9.98)	10.1 (8.37-11.8)	11.1 (9.03-13.1)	12.0 (9.50-14.6)	13.0 (9.85-16.1)	14.2 (10.3-18.0)	15.0 (10.7-19.4)

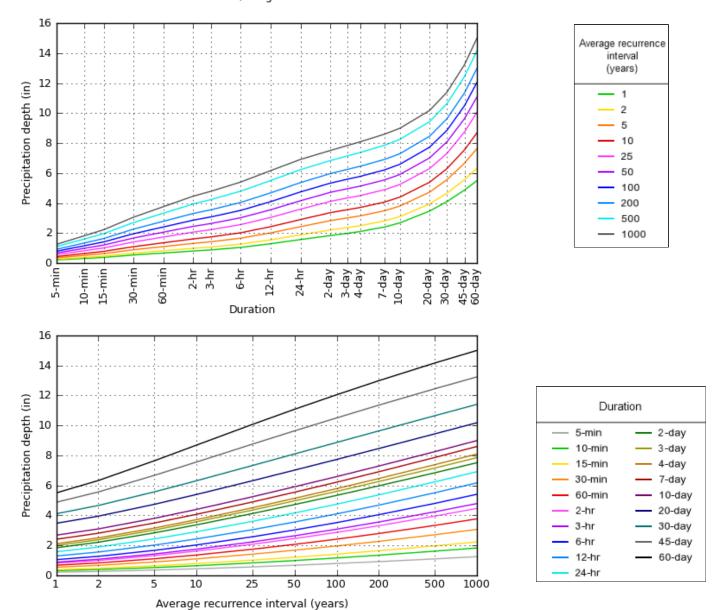
¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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PDS-based depth-duration-frequency (DDF) curves Latitude: 39.8126°, Longitude: -104.9436°



NOAA Atlas 14, Volume 8, Version 2

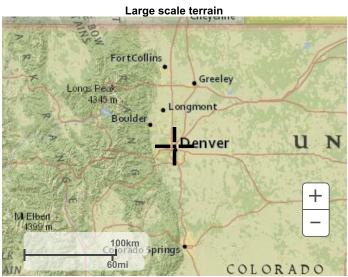
Created (GMT): Wed May 1 16:58:04 2019

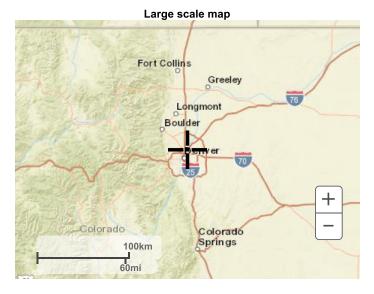
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Maps & aerials

Small scale terrain







Large scale aerial



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US Department of Commerce
National Oceanic and Atmospheric Administration
National Weather Service
National Water Center
1325 East West Highway
Silver Spring, MD 20910
Questions?: HDSC.Questions@noaa.gov

Disclaimer

AMERICAN GEOSERVICES

Infiltration Testing Report





GEOTECHNICAL & MATERIALS ENVIRONMENTAL STRUCTURAL CIVIL ENGINEERING AND SCIENCE 888-276-4027

April 01, 2020

PROJECT NO: 0156-D20

CLIENT: Mr. John Draft

Reference: Infiltration Test Report, 3740 E. 64th Avenue, Commerce City, CO

Dear Mr. Draft,

At your request, we have completed the above referenced services for the referenced project in accordance with the American GeoServices, LLC (AGS) proposal. Results of our evaluation and design recommendations are described below.

PROJECT INFORMATION

The site is located as shown in Figure 1 and Figure 2. The parcel is located in a commercial/industrial area. The proposed development will consist of building a roadway and associated structures. We do not anticipate significant site grading (fill placement) for this project.

INFILTRATION TESTING

In March 2020, we performed three soil explorations at locations B1 through B3 as shown in Figure 2 as a profile borehole. In addition, three infiltration tests were performed within proximity of locations B1 through B3. Details of subsurface exploration and infiltration testing results are summarized below. Also, see attached soil borehole logs in an appendix.

Subsurface soil conditions: In boreholes B1 through B3, generally medium stiff to stiff sandy silts (ML) to medium dense silty sands (SM) were encountered extending to a maximum explored depth of 8 feet. A restricting or limiting layer was not noted. Groundwater table was not noted. Soil mottling suggesting or the possible indication of perched high groundwater table was not noted. It should be noted that soil classification and identification is based on commonly accepted methods employed in the practice of geotechnical engineering. In some cases, the stratigraphic boundaries shown on Boring Logs represents transitions between soil types rather than distinct lithological boundaries. It should be recognized that subsurface conditions often vary both with depth and laterally between individual boring locations.

Seasonal High Water Table: Subsurface exploration did not reveal the presence of a seasonal high water table. No water seepage, static water table, or soil caving was noted. In our opinion, seasonal high or perched groundwater conditions may not exist within 5 feet below existing ground surface during heavy rains, throughout the site. This observation may not be indicative of other times or at locations other than the site. Some variations in the groundwater level may be experienced in the future. The magnitude of the variation will largely depend upon the duration and intensity of precipitation, temperature and the surface and subsurface drainage characteristics of the surrounding area.

Field Infiltration Rate: We performed three infiltration tests in general accordance with EPA test procedures and Commerce City, CO general guidelines. Following infiltration rates and results were noted in the field.

Test	Test Depth	SCS Soil Description	Groundwater Table	Field Infiltration
Location	n (Ft)	(USCS Soil	(Ft)	Rate
		Classification)		(in/hr)
B1	2.0	Silt loam (ML)	Not encountered	2.5
B2	2.0	Silt loam (ML)	Not encountered	2.0
В3	2.5	Silty sandy loam (SM)	Not encountered	4.0

Design Infiltration Rate: The field infiltration rate should be scaled down by the factor of 0.5: Therefore, design infiltration rate = 2.0*0.5 = 1.0 inch/hour.

Setback: All infiltration facilities should have a setback of 10 feet from proposed structures to minimize the adverse impact of any local mounting of groundwater table.

LIMITATIONS

The given infiltration rates obtained in the field may vary from location to location due to variations in subsurface soil conditions. Moreover, design storm events may not accurately account for actual storm events during the design life of the drainage structures. Therefore, the potential for overflow should be considered and properly discharged into suitable receptacles in a controlled manner. All stormwater disposal systems should be designed in such a way that the groundwater quality of local aquifers is not adversely affected.

Recommendations contained in this report are based on our field observations and subsurface explorations, limited laboratory evaluation, and our present knowledge of the proposed construction. It is possible that soil conditions could vary between or beyond the points explored. If soil conditions are encountered during construction that differ from those described herein, we

should be notified so that we can review and make any supplemental recommendations necessary. If the scope of the proposed construction, including the proposed loads or structural locations, changes from that described in this report, our recommendations should also be reviewed and revised by AGS.

Local regulations regarding land or facility use, on and off-site conditions, or other factors may change over time, and additional work may be required with the passage of time. Based on the intended use of the report within one year from the date of report preparation, AGS may recommend additional work and report updates. Non-compliance with any of these requirements by the client or anyone else will release AGS from any liability resulting from the use of this report by any unauthorized party. Client agrees to defend, indemnify, and hold harmless AGS from any claim or liability associated with such unauthorized use or non-compliance.

In this report, we have presented judgments based partly on our understanding of the proposed construction and partly on the data we have obtained. This report meets professional standards expected for reports of this type in this area. Our company is not responsible for the conclusions, opinions or recommendations made by others based on the data we have presented. This report has been prepared exclusively for the client, its' engineers and subcontractors for the purpose of design and construction of the proposed structure. No other engineer, consultant, or contractor shall be entitled to rely on information, conclusions or recommendations presented in this document without the prior written approval of AGS.

We appreciate the opportunity to be of service to you on this project. If we can provide additional assistance or observation and testing services during design and construction phases, please call us at 1 888 276 4027.





Sam Adettiwar, MS, PE, GE, P.Eng, M.ASCE Senior Engineer Attachments



NOTE:

SCHEMATIC PLAN TO SHOW APPROXIMATE SUBSURFACE EXPLORATION LOCATION ONLY; NOT SURVEYED.



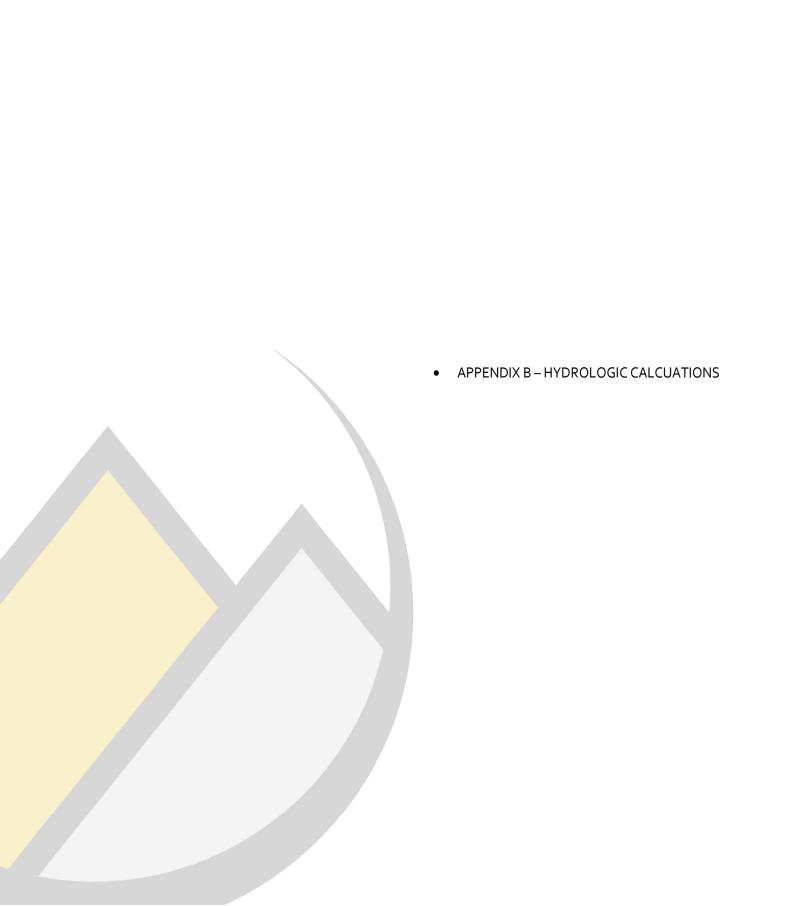
LEGEND:

DESIGNATES INFILTRATION TEST LOCATION, BY AMERICAN GEOSERVICES, LLC., MARCH 2020 SEE EXPLORATION LOG IN APPENDIX FOR FURTHER DETAILS.

REFERENCE: LEEPER INDUSTRIAL PARK DEVELOPMENT PLAN



FIGURE 2: SCHEMATIC SITE PLAN



Project No.: 21087

Drainage Basin Imperviousness

Soil Type : A

	Roof	Concrete	Recycled Asphalt	Asphalt	Playground	Gravel	Undeveloped						
Imperviousness:	90%	90%	89%	100%	10%	40%	2%	Total Area	Composite		Runoff Co	efficients	
Basin Name				Areas (sq.	ft.)			(sq.ft.)	% lmp.	C ₂	C ₅	C ₁₀	C ₁₀₀
EX-A	3,556	4,832	294,715	1,234			98,423	402,760	68%	0.51	0.52	0.54	0.64
EX-B	8,024	645	373,790	3,746			31,763	417,968	83%	0.65	0.67	0.69	0.75
EX-C			29,704	17,121			24,645	71,470	62%	0.45	0.46	0.48	0.59
Total Existing	11,580	5,477		22,101			154,831	892,198	5%	0.02	0.02	0.02	0.15
А	3,556	4,400	234,002	1,234			103,574	346,766	63%	0.46	0.48	0.49	0.60
В	8,024	419	325,726	2,846			102,719	439,734	69%	0.52	0.53	0.55	0.65
С			20,520	2,990			31,638	55,148	40%	0.25	0.26	0.28	0.42
Total Proposed	11,580	4,819	580,248	7,070			237,931	841,648	65%	0.47	0.49	0.51	0.61



Project No.: 21087

By: JGD

SF2 - Time of Concentration

			Initia	al/Overland	Time			Travel Time			Time of Co	ncentration	Final
								Conveyance			Comp. T _C	Regional	
Basin ID	Area (AC.)	C ₅	L _i (ft.)	S (%)	T _i (min.)	L _t (ft.)	S (%)	Factor	Vel (fps)	T _t (min.)	(min.)	T _c (Min.)	T _c (Min.)
EX-A	9.25	0.52	373	0.50	25.3	559	1.2	10	1.1	8.5	33.8	19.1	19.1
EX-B	9.60	0.67	500	0.50	21.7	121	0.7	10	0.8	2.4	24.1	13.1	13.1
EX-C	1.64	0.46	17	2.00	3.8	227	0.5	15	1.1	3.6	7.3	18.6	7.3
Α	7.96	0.48	373	0.50	27.3	559	1.2	10	1.1	8.5	35.8	20.0	20.0
В	10.09	0.53	500	0.50	28.8	121	0.7	10	0.8	2.4	31.2	15.6	15.6
С	1.27	0.26	17	2.00	4.9	227	0.5	15	1.1	3.6	8.5	22.9	8.5

Project No.: 21087 By: JGD

SF₃ - Minor Storm

1-hr Point Rainfall **0.83** in. (2-year Event)

				Direct	Runoff				Total	Runoff		Str	eet	Tr	avel Tin	ne	
	Design			Tc	CA	_		Tc	CA			Slope		Length		tt	
Description	Point	(ac.)	C ₅	(min.)	(ac.)	(in/hr)	Q (cfs)	(min.)	(ac.)	(in/hr)	Q (cfs)	(%)	(cfs)	(ft)	(fps)	(min.)	Comments
EX-A		9.25	0.52	19.1	4.8	1.67	8.10										
EX-B		9.60	0.67	13.1	6.5	2.00	12.93										
EX-C		1.64	0.46	7.3	0.8	2.51	1.91										
Total		20.48					22.94										
А		7.96	0.48	20.0	3.8	1.63	6.20										
В		10.09	0.53	15.6	5.4	1.85	9.96										
С		1.27	0.26	8.5	0.3	2.39	0.80		·	·							
Total		19.32					16.96										



Project No.: 21087 By: JGD

SF₃ - Minor Storm

1-hr Point Rainfall 1.11 in. (5-year Event)

				Direct	Runoff				Total	Runoff		Str	eet	Tr	avel Tin	ne	
	Design	Area		Тс	CA	_		Tc	CA	_		Slope	Flow	Length	Vel.	tt	
Description	Point	(ac.)	C ₅	(min.)	(ac.)	(in/hr)	Q (cfs)	(min.)	(ac.)	(in/hr)	Q (cfs)	(%)	(cfs)	(ft)	(fps)	(min.)	Comments
EX-A		9.25	0.52	19.1	4.8	2.24	10.84										
EX-B		9.60	0.67	13.1	6.5	2.68	17.29										
EX-C		1.64	0.46	7.3	0.8	3.36	2.56										
Total		20.48					30.68										
Α		7.96	0.48	20.0	3.8	2.18	8.29										
В		10.09	0.53	15.6	5.4	2.47	13.32										
С		1.27	0.26	8.5	0.3	3.19	1.07										
Total		19.32					22.68										
				·								·					

Project No.: 21087 By: JGD

SF₃ - Major Storm

1-hr Point Rainfall 2.42 in. (100-year Event)

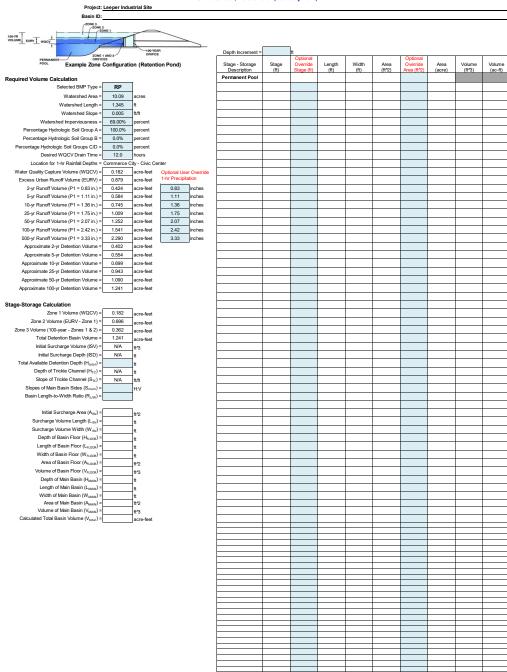
				Direct	Runoff				Total	Runoff		Str	eet	Tr	avel Tin	ne	
	Design			Tc	CA	_		Тс	CA	_		Slope	Flow	Length		tt	
Description	Point	(ac.)	C ₁₀₀	(min.)	(ac.)	(in/hr)	Q (cfs)	(min.)	(ac.)	(in/hr)	Q (cfs)	(%)	(cfs)	(ft)	(fps)	(min.)	Comments
EX-A		9.25	0.64	19.1	5.9	4.88	28.82										
EX-B		9.60	0.75	13.1	7.2	5.84	42.20										
EX-C		1.64	0.59	7.3	1.0	7.33	7.10										
Total		20.48					78.12										
А		7.96	0.60	20.0	4.8	4.75	22.79										
В		10.09	0.65	15.6	6.5	5.39	35.18										
С		1.27	0.42	8.5	0.5	6.96	3.69										
Total		19.32					61.66										





DETENTION BASIN STAGE-STORAGE TABLE BUILDER

UD-Detention, Version 3.07 (February 2017)



21087 UD-Deterlion y3.07, Basin 8/29/2022, 7:33 PM

Project : Leeper Industrial Park

Project No.: 21087

Calculated By : JGD

Date : 4/27/2022

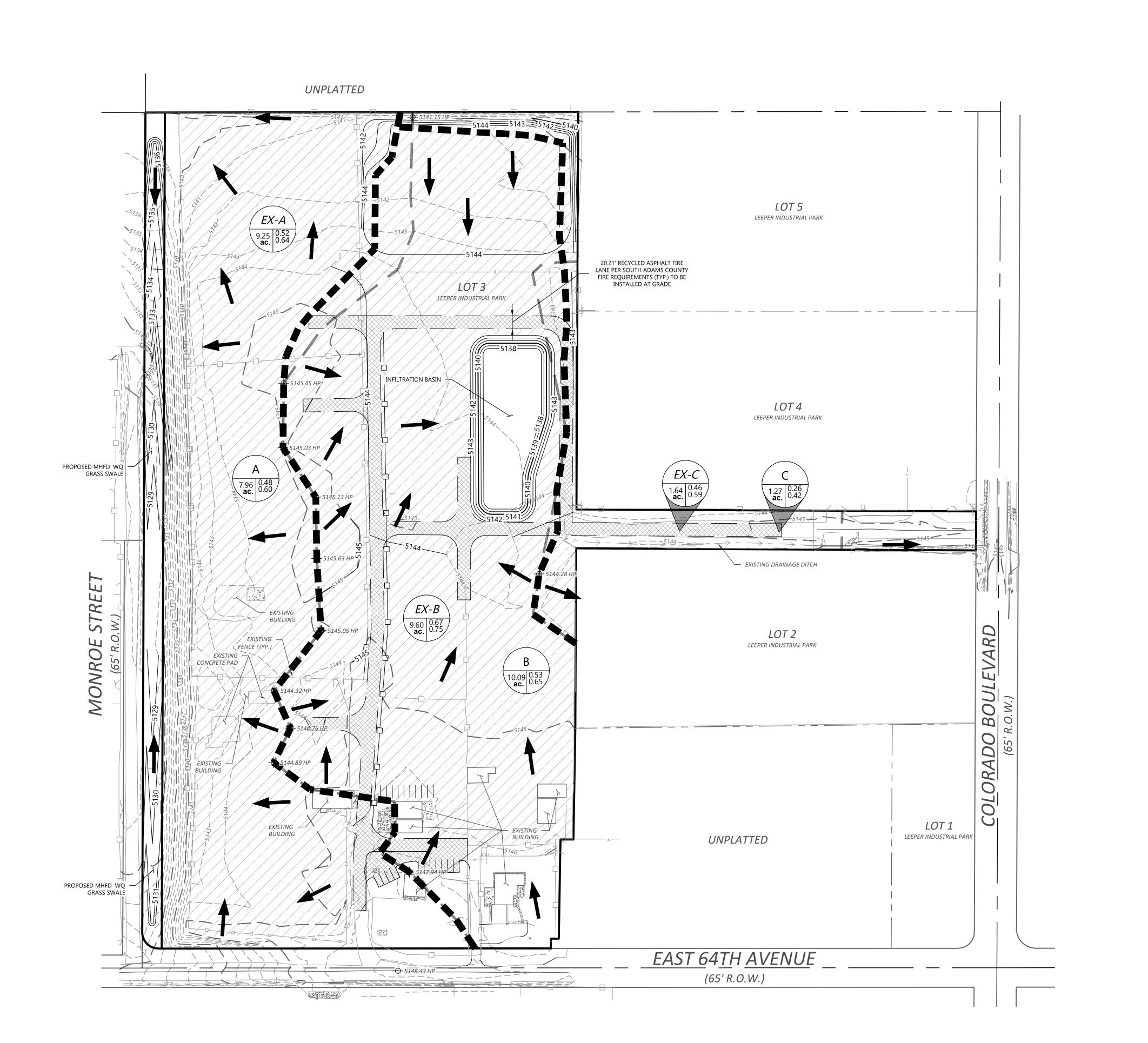
Pond Volume by Contour Area

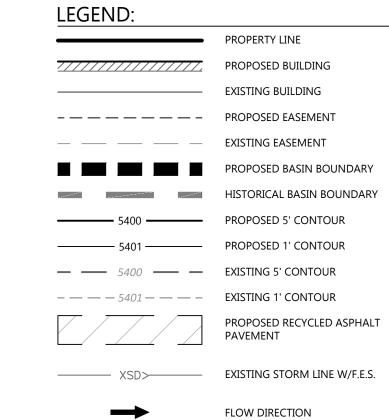
		-		
Contour Elevation	Areas (sq.ft.)	Area (Acre)	Volume (ft³)	Cumulative Volume (ac-ft)
5138	19,156	0.44	0	0.00
5139	21,729	0.50	20,429	0.47
5140	24,402	0.56	43,482	1.00
5141	27,176	0.62	69,258	1.59
5142	30,056	0.69	97,862	2.25
5143	33,025	0.76	129,391	2.97

	UD-BMP (Version 3.07, Ma	rch 2018) Sheet 1
Designer:	Jason DeYoung	
Company:	Proof Civil Consulting Engineers	
Date:	July 22, 2022	
Project:	Leeper Industrial Park	
Location:	64th Avenue & Monroe Street	
1. Design Di	ischarge for 2-Year Return Period	Q ₂ = 5.54 cfs
2. Hydraulic	Residence Time	
A) : Leng	th of Grass Swale	L _S = 285.0 ft
B) Calcul	lated Residence Time (based on design velocity below)	T _{HR} = 4.8 minutes
3. Longitudir	nal Slope (vertical distance per unit horizontal)	
A) Availa	ble Slope (based on site constraints)	$S_{avail} = 0.008$ ft / ft
B) Desigr	n Slope	$S_D = 0.007$ ft / ft
4. Swale Ge	ometry	
A) Chann	nel Side Slopes (Z = 4 min., horiz. distance per unit vertical)	Z = 16.00 ft / ft
B) Botton	n Width of Swale (enter 0 for triangular section)	W _B = 0.00 ft
5. Vegetation	n	Choose One
A) Type o	of Planting (seed vs. sod, affects vegetal retardance factor)	● Grass From Seed ♀ Grass From Sod
6. Design Ve	elocity (0.95 ft / s maximum for desirable 5-minute residence time)	V ₂ =[ft / s
7. Design Flo	ow Depth (1 foot maximum)	D ₂ = 0.59 ft
A) Flow A	Area	$A_2 = \underline{\hspace{1cm}} 5.6 \underline{\hspace{1cm}} sq ft$
B) Top W	/idth of Swale	W _T = 18.9 ft
		F = 0.32
C) Froude	Number (0.50 maximum)	F = 0.32
D) Hydrai	ulic Radius	R _H = 0.29
E) Veloci	ty-Hydraulic Radius Product for Vegetal Retardance	VR = 0.29
F) Manni	ng's n (based on SCS vegetal retardance curve E for seeded grass)	n = 0.055
,		
G) Cumu	llative Height of Grade Control Structures Required	$H_D = $
8. Underdrai (Is an un	in nderdrain necessary?)	Choose One WYES O NO AN UNDERDRAIN IS REQUIRED IF THE DESIGN SLOPE < 2.0%
9. Soil Prepa (Describe	aration soil amendment)	
10. Irrigation		Choose One
N		
Notes:		

21087 UD-BMP_v3.07, GS 7/22/2022, 11:49 AM







PROPOSED SPOT GRADE

25.25

EXISTING SPOT GRADE

2.00%

SLOPE AND DIRECTION

HP

HIGH POINT

LP

LOW POINT

GB

GRADE BREAK

GB GRADE BREAK

A1

BASIN ID

BASIN IDENTIFICATION

0.80
0.90

5.VR RUNGE

BASIN ACREAGE BASIN IDENTIFICATION TAG

5-YR RUNOFF
COEFFICIENT
100-YR RUNOFF

FOR AND ON BEHALF OF PROOF CIVIL CO.

DRAINAGE PLAN
LEEPER INDUSTRIAL PARK

DRAWING NO.

DRN-1