FINAL DRAINAGE REPORT

FOR

REUNION CENTER FILING NO. 1, AMENDMENT NO. 1 CITY OF COMMERCE CITY, COLORADO

Prepared for:

Clayton Properties Group II, Inc. dba Oakwood Homes 4908 Tower Road Denver, CO 80249 Contact: Jim Hayes Phone: 303-486-8644

Prepared by:



CORE Consultants, Inc. 3473 South Broadway Englewood, CO 80113 Contact: Justin Simpson, PE Phone: 303-703-4444 CORE Project Number: 18-004

April 26, 2024



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Appendix A Hydrologic Computations

Appendix B Hydraulic Computations

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Back Pocket

Drainage Maps



Engineer's Statement:

I hereby certify that this final study for Reunion Center Filing No. 1, Amendment No. 1, was prepared by me (or under my direct supervision) in accordance with the provisions of the City of Commerce City Storm Drainage Design and Technical Criteria Manual for the owners thereof. I understand that the City of Commerce City does not, and will not, assume liability for drainage facilities designed by others.

Justin Simpson, P.E. Registered Professional Engineer State of Colorado No. 54521



I. GENERAL LOCATION AND DESCRIPTION

A. Location

Reunion Center Filing No. 1, Amendment No. 1 is located within the SE 1/4 Of Section 09, Township 2 South, Range 66 West of the Sixth Principal Meridian, City of Commerce, County of Adams, State of Colorado. The project is a separate filing within the Reunion Village 1 overall development. The site is at the southwest corner of the intersection of Tower Road and Homestead Trail. The Site is bounded by Homestead Trail to the north, future Reunion Center Filing No. 1, Amendment No. 2 to the west, Tower Road to the east, and E 105th Avenue to the south. Reunion Center Filing No. 1 Amendment No. 2 is currently in the design phase by the same developer and is anticipated to be constructed after Amendment No. 1. North of Homestead Trail is "The Stead School" and an undeveloped portion of Reunion Center Filing No. 1. East of Tower Road is an undeveloped Parcel of Reunion Filing No. 33. South of E 105th Avenue is proposed commercial sites within Reunion Ridge Filing No.1. See "Reunion Center – Duet & Commercial Phase" construction Documents completed by JR. Engineering. A vicinity map is included in Appendix A.

The site is located within the Third Creek Major Drainage Basin that is tributary to the South Platte River. The proposed storm system will outfall into an existing detention and water quality pond, that is located within the southeastern portion of the site. Design for this pond (Pond 108a) is found in the Final Drainage Report for Reunion Center – Duet & Commercial Phase (Master Report) completed on November 30, 2023. This pond is expected to be constructed prior to or during the construction for Filing 1 Amendment 1. Coordination with the engineers tasked with the design of the surrounding infrastructure is necessary to ensure the facilities are properly sized and connected.

B. Description of Property

The site is approximately +/- 9 acres, with slopes ranging from two to 25 percent, and is currently undeveloped.

According to information from the United States Department of Agriculture's (USDA) Natural Resource Conservation Service (NRCS), soils on-site are Ascalon-Vona sandy loam and Ascalon sandy loam (annotated AvC and AsB, respectively). These soils are further classified as belonging to Hydrologic Soil Groups (HSG) B. Group B soils have moderate infiltration rates when thoroughly wetted and consist chiefly of moderately deep to deep, moderately well to well drained soils with moderately fine to moderately course textures. Soils maps are included in Appendix A.

The site lies within Zone X (areas determined to be outside the 0.2% annual chance floodplain) on Flood Insurance Rate Map (FIRM) 08001C0344H, revised March 5, 2007, published by the Federal Emergency Management Agency (FEMA). There are no major drainageways within the site; however, an existing detention pond exists along the south property boundary that will be replaced by the Reunion Center infrastructure construction by others. A floodplain map is included in Appendix A.



Existing ground cover consists of 100 percent tillage. Vegetation in the developed condition will include short lawns, ornamental trees, and shrubs wherever buildings and hardscape are not proposed. A detention pond exists on-site along the south property boundary. This pond will be removed during construction; however, multiple other ponds will be built (by others) within the site and south of the site that will store and treat developed runoff from the site.

An 8' Utility Easement (Rec. No. 2020000123227) is located along the North, West, and South along Homestead Trail, Walden St, and E 105th Ave respectively. A drainage Easement with a Rec. No. 2020000123227 is in the Southwest corner of the site. On the East side of the site a 10' Utility Easement (Rec. No. 2020000123227) exists next to a 10' United Power Utility Easement (Rec. No. 20050722000778740). Another 10' United Power Utility Easement (Rec. No. 20040630000553010) runs along the East side of the site on the South side until it breaks away and runs Northeast toward Tower Rd.

Proposed site improvements include 84 residential units, configured so that two units share a common wall, and associated roadway and utility infrastructure.

The Master Report has been conducted by JR Engineering and was approved by Commerce City on June 2, 2020. This report includes references and is consistent with previously done outfall studies including the *Third Creek and Barr Lake Drainage Outfall Planning Study* by Kiowa Engineering Corporation, dated July 1990, and the *Third Creek (Downstream of DIA) Outfall Systems Planning Study Update*, by Kiowa Engineering Corporation, dated September 2005. The Master Report also states it complies with the FHAD completed by Matrix Design Group in November of 2018.

This report includes discussion and calculations for the drainage facilities proposed with both Amendment No. 1 and Amendment No. 2 since both have the same Owner, have been designed together, and will be constructed at approximately the same time. The facilities associated with the separate amendments have been labeled as such throughout the report and Drainage Maps.

II. DRAINAGE BASINS AND SUB-BASINS

A. Major Basin Description

The site is located within the Third Creek Major Drainage Basin that is tributary to the South Platte River.

There are no regulatory floodplains within the site. There are no nearby irrigation facilities, to our knowledge, that will influence or be influenced by the local drainage.

B. Sub-Basin Description

Developed runoff from the site will surface drain to proposed storm infrastructure and will drain to existing detention and water quality pond (by others) that is in the southeastern portion of the site. Proposed hydrologic calculations are included in Appendix A and a Proposed Drainage Map is included in the Back Pocket of this report.



Runoff from offsite enters from 105th Ave. As is further described in the basins below.

Proposed sub-basin descriptions:

A2.1

Consists of lot area, roadway area, concrete walks, and landscape area. Runoff flows overland into the proposed roadway, where it is conveyed to a proposed Type R sump inlet at DP A2.1. The proposed storm sewer conveys flows to the south and outfalls into the detention pond (by others). In the case of inlet clogging, emergency overflow from the sump inlet will overtop the road crown and drain to the inlet at DP A2.2.

A2.2

Consists of lot area, roadway area, concrete walks, and landscape area. Runoff flows overland into the proposed roadway, where it is conveyed to a proposed Type R sump inlet at DP A2.2. The proposed storm sewer conveys flows to the south and outfalls into the detention pond (by others). In the case of inlet clogging, emergency overflow from the sump inlet will overtop the road crown and drain to the inlet at DP A2.1.

A3.1

Consists of lot area, roadway area, concrete walks, and landscape area. Runoff flows overland into the proposed roadway, where it is conveyed to a proposed Type R sump inlet at DP A3.1. The proposed storm sewer conveys flows to the south and outfalls into the detention pond (by others). In the case of inlet clogging, emergency overflow from the sump inlet will overtop the road crown and drain to the inlet at DP A3.2.

A3.2

Consists of lot area, roadway area, concrete walks, and landscape area. Runoff flows overland into the proposed roadway, where it is conveyed to a proposed Type R sump inlet at DP A3.2. The proposed storm sewer conveys flows to the south and outfalls into the detention pond (by others). In the case of inlet clogging, emergency overflow from the sump inlet will overtop the road crown and drain to the inlet at DP A3.1.

A4.1

Consists of lot area, roadway area, concrete walks, and landscape area. Runoff flows overland into the proposed roadway, where it is conveyed to a proposed Type R sump inlet at DP A4.1. Offsite flows enter from E 105th Ave. at the Southwestern intersection of Box Elder Way. Flows enter from the south and flow into the proposed system by inlets on Box Elder way. The proposed storm sewer conveys flows to the south and outfalls into the detention pond (by others). In the case of inlet clogging, emergency overflow from the sump inlet will overtop the road crown and drain to the inlet at DP A4.2.



A4.2

Consists of lot area, roadway area, concrete walks, and landscape area. Runoff flows overland into the proposed roadway, where it is conveyed to a proposed Type R sump inlet at DP A4.2. Offsite flows enter from E 105th Ave at the Southeastern corner of the intersection with Box Elder way. The flows come from the south and enter the proposed system through inlets on Box Elder Way. The proposed storm sewer conveys flows to the south and outfalls into the detention pond (by others). In the case of inlet clogging, emergency overflow from the sump inlet will overtop the road crown and drain to the inlet at DP A4.1.

B.1

Consists of lot area, roadway area, concrete walks, and landscape area. Runoff flows overland into the proposed roadway, where it is conveyed to a proposed Type R sump inlet at DP B.1. The proposed storm sewer conveys flows to the south and outfalls into the detention pond (by others). In the case of inlet clogging, emergency overflow from the sump inlet will overtop the road crown and drain to the inlet at DP B.3.

<u>B.2</u>

Consists of lot area, roadway area, concrete walks, and landscape area. Runoff flows overland into the proposed roadway, where it is conveyed to a proposed Type R on-grade inlet at DP B.3. The proposed storm sewer conveys flows to the south and outfalls into the detention pond (by others). In the case of inlet clogging, emergency overflow from the sump inlet will overtop the road crown and drain to the inlet at DP B.1.

<u>B.3</u>

Consists of lot area, roadway area, concrete walks, and landscape area. Runoff flows overland into the proposed roadway, where it is conveyed to a proposed Type R sump inlet at DP B.3. The proposed storm sewer conveys flows to the south and outfalls into the detention pond (by others). In the case of inlet clogging, emergency overflow from the sump inlet will overtop the road crown and drain to the inlet at DP B.1.

D2

Consists of lot area, roadway area, concrete walks, and landscape area. Runoff flows overland off-site into the existing roadway, where it is conveyed to an existing Type R sump inlet at DP D2.

D3

Consists of lot area, roadway area, concrete walks, and landscape area. Runoff flows overland off-site into the existing roadway, where it is conveyed to an existing Type R sump inlet at DP D3.

D2.1

Consists of lot area, roadway area, concrete walks, and landscape area. Runoff flows overland into the proposed roadway, where it is conveyed to a proposed Type 13 valley sump inlet at DP D2.1. The proposed storm sewer conveys flows to the south and outfalls into the detention pond (by others). In the case of inlet clogging, emergency overflow from the sump inlet will overtop the road crown and drain to the inlet at DP D2.2.



D2.2

Consists of lot area, roadway area, concrete walks, and landscape area. Runoff flows overland into the proposed roadway, where it is conveyed to a proposed Type R sump inlet at DP A2.2. The proposed storm sewer flows to the south and outfalls into the detention pond (by others). In the case of inlet clogging, emergency overflow from the sump inlet will overtop the road crown and drain to the inlet at DP D2.1.

III. DRAINAGE DESIGN CRITERIA

A. Regulations

This Drainage Addendum is in accordance with the guidelines set forth by the Commerce City Drainage Manual and the Mile High Flood District (MHFD) Urban Storm Drainage Criteria Manual (USDCM. These manuals were used as a basis of design for the site.

B. Development Criteria Reference and Constraints

This report conforms to the Preliminary Drainage Report for Reunion Center - Village 1 (Master Report), dated March 5, 2020, by JR Engineering and The Final Drainage Report For Reunion Center – Duets & Commercial Phase, dated November 30, 2023 by JR Engineering. These reports detail the drainage plan for the overall Reunion Center development. Excerpts from the Master Report are included in Appendix C.

The Master Report designates this Filing No. 1, Amendment No. 1 site and the adjacent Amendment No. 2 site as included in sub-basin B8 that drains to Pond 108a. The design for the receiving pond infrastructure accounts for sub-basin B8 at an imperviousness of 76 percent. The combined imperviousness for the proposed Filing No. 1, Amendments No. 1 and 2 sites is approximately 66.3 percent; therefore, the site is in conformance with the Master Report and will not adversely impact the downstream infrastructure.

The design of the proposed storm system was constrained by the need to connect to the relatively shallow existing storm infrastructure at the upstream end. Site grading was constrained by the lack of available fill material on-site. These two factors contributed to the challenge of maintaining adequate cover over the proposed storm pipes.

C. Hydrological Criteria

On-site hydrologic calculations were performed using a proprietary rational method workbook, developed by CORE in Microsoft Excel, to estimate peak overland runoff flows resulting from the minor (5-year) and major (100-year) storm events. The workbook utilizes rainfall data provided the Master Report. The hydrologic soil group on the site is Ascalon-Vona sandy loam with slopes from 1%-5%. A small portion of the Northeast corner of the site is Ascalon sandy loam, with 0%-3% slopes. See Appendix A for more hydrologic soil group information.



D. Hydraulic Criteria

Streets within the proposed development have been classified as local roads and include a 4.5-inch mountable curb and six-inch vertical curb. This traffic classification corresponds to drainage classification Type A, per the City Criteria. Street and Inlet capacities were determined using the MHFD workbook, UD-Inlet_v4.060xlsm, with values based on the Type A drainage classification and curb type. Hydraulic analysis and stormwater routing of the proposed storm sewer was completed using StormCAD v10.03.01.08 software by Bentley, with junction losses modeled per Table 2 of the supplemental MHFD publication, Modeling Hydraulic and Energy Gradients in Storm Sewers, dated October 6, 2009, by AMEC.

E. Stormwater Quality

Runoff from the site is directed via proposed storm sewer to detention pond 108a located in the southeastern portion of Filing 1 Amendment 1. Flows will then travel via existing storm sewer in Tower Road to the existing water quality pond 105 located to the east of Tower Road. These ponds have been designed by others to provide water quality treatment and flood attenuation for the developed site; therefore, meeting MS4 requirements. The *Final Drainage Report For Reunion Center – Duet & Commercial Phase*, dated November 30, 2023 by JR Engineering and Amendment #2 to Preliminary Drainage Report for Reunion Center – Village 1, dated November 6, 2023 by JR Engineering contains calculations for the existing storm sewer infrastructure and pond design (See Appendix C).

IV. DRAINAGE FACILITY DESIGN

A. General Concept

Runoff from the proposed residential development generally surface drains into the proposed Type A roadway curb and gutter. These flows are captured by proposed storm sewer inlets and conveyed south to the existing detention and water quality pond that is located in Filing 1 Amendment 1.

B. Specific Details

The proposed storm sewer system will connect to the existing storm infrastructure of the overall Reunion Center - Village 1 development at the upstream end to the north and the downstream end will outfall into the existing detention pond. Developed runoff from the site will be detained and treated for water quality by ponds that are a part of the existing infrastructure (by others). The existing and proposed storm sewer infrastructure will be owned and maintained by the City.

V. CONCLUSIONS

A. Compliance with Standards

This report and associated calculations comply with the City of Commerce City "Storm Drainage Design and Technical Criteria Manual," the Mile High Flood District's "Urban Storm Drainage Criteria Manual," the "Amendment #2 to Preliminary Drainage Report for Reunion Center - Village 1" by JR Engineering, and the "Final Drainage Report for Reunion Center - Duet & Commercial Phase" by JR Engineering.



The project meets the requirements set forth within Chapter 14 of the City of Commerce City Storm Drainage Criteria Manual as it incorporates numerous methods to disconnect impervious areas. Methods include, but are not limited to, detached sidewalk within public ROW to provide water quality treatment of runoff prior to stormwater flows entering the public ROW, roof drains discharged to grass lined swales between the homes, driveways reduce pollutants and provide additional imperviousness for stormwater runoff, offset and disconnected alleyways within the residential blocks, and storm water will discharge into a water quality pond adjacent to the site to provide additional stormwater treatment measures. See attached Disconnected Impervious Map Exhibit.

B. Drainage Concept

The drainage plan for the overall Reunion Center - Village 1 development is set forth by the Master Report, which designates the maximum allowable imperviousness for this Filing No. 1, Amendment No. 1 site. Developed runoff from the site will be captured by the proposed storm sewer system that will connect to existing storm sewer infrastructure and be conveyed to Existing Detention and Water Quality Ponds (by others), per the Master Report. The imperviousness of the site is less than the maximum allowable set forth by the Master Report; therefore, flows will not adversely impact the downstream infrastructure.



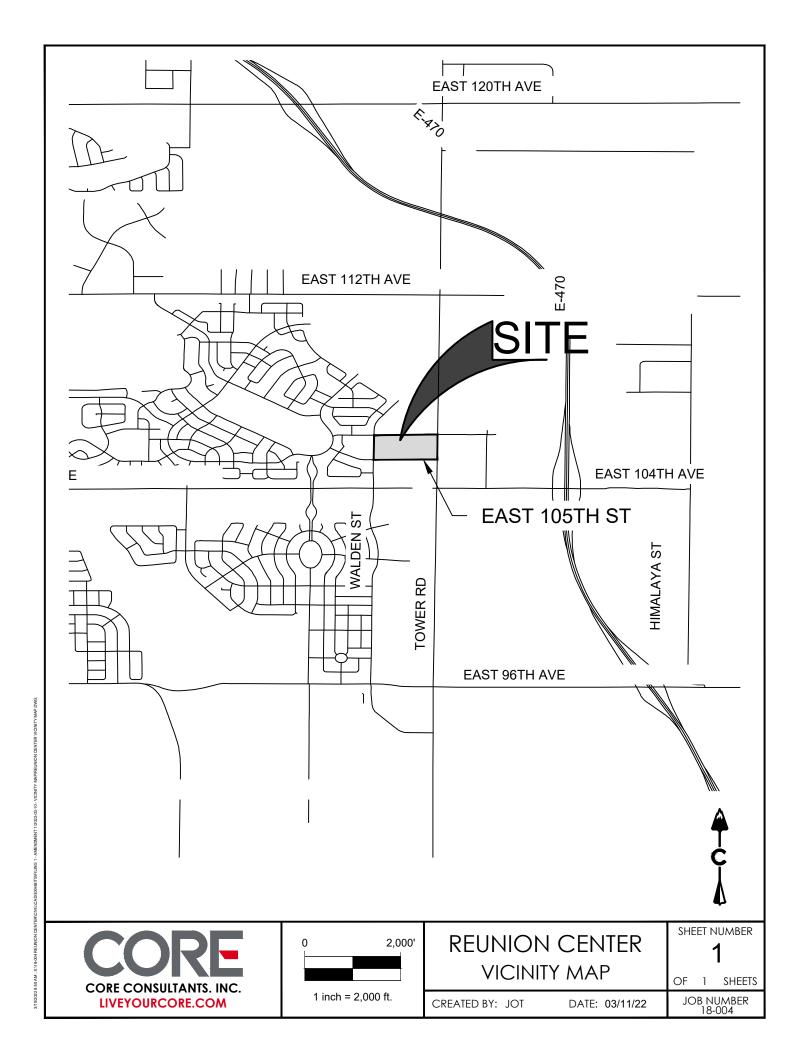
VI. REFERENCES

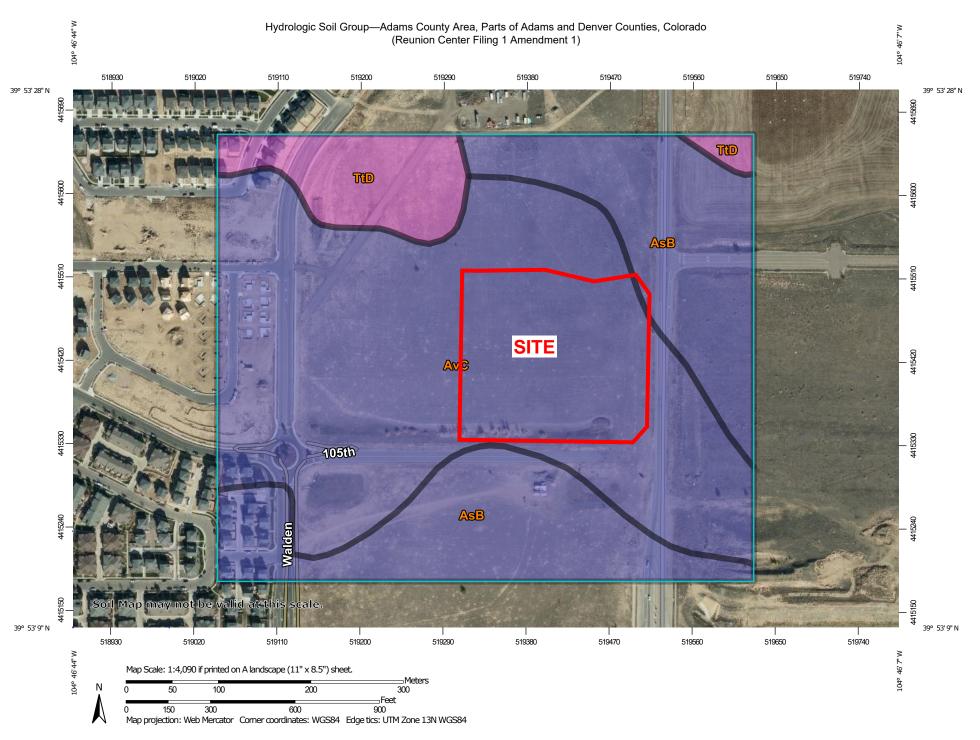
- A. <u>Storm Drainage and Technical Criteria Manual</u>; City of Commerce City Department of Public Works, February 2023.
- B. <u>Urban Storm Drainage Criteria Manual (Volumes 1, 2, and 3)</u>; Urban Drainage and Flood Control District, January 2016 and latest revisions.
- C. <u>Modeling Hydraulic and Energy Gradients in Storm Sewers;</u> AMEC Earth & Environmental, Inc., October 6, 2009.
- D. <u>Web Soil Survey</u>, Soil Survey Staff (Natural Resources Conservation Service), United States Department of Agriculture. Available online at the following link: https://websoilsurvey.sc.egov.usda.gov/. Accessed April 5, 2021.
- E. <u>Flood Insurance Rate Map (FIRM) No. 08001C0339H</u>, Federal Emergency Management Agency, Revised March 16, 2016. Available online at the following link: https://msc.fema.gov/portal/home. Accessed April 5, 2021.
- F. <u>Third Creek and Barr Lake Drainage Outfall Planning Study</u>; Kiowa Engineering Corporation, July 1990.
- G. <u>Third Creek (Downstream of DIA) Outfall Systems Planning Study Update;</u> Kiowa Engineering Corporation, September 2005.
- H. Third Creek Flood Hazard Area Delineation Report; Matrix Design Group, Inc., November 2018.
- I. <u>Final Drainage Report for Reunion Center Duet & Commercial Phase</u>; JR Engineering, November 30, 2023
- J. <u>Amendment #2 to Preliminary Drainage Report for Reunion Center Village 1</u>; JR Engineering, November 6, 2023

Computer Modeling Programs:

- A. <u>StormCAD</u> by Bentley Systems, Inc., Version 10.03.01.08.
- B. Inlet Management Version 5.02. MHFD. August 2022

APPENDIX A HYDROLOGIC COMPUTATIONS





MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:20.000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D **Soil Rating Polygons** Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil **Water Features** line placement. The maps do not show the small areas of A/D contrasting soils that could have been shown at a more detailed Streams and Canals Transportation B/D Rails ---Please rely on the bar scale on each map sheet for map measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available -Local Roads Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. Soil Survey Area: Adams County Area, Parts of Adams and Denver Counties, Colorado Survey Area Data: Version 17, Jun 4, 2020 Soil map units are labeled (as space allows) for map scales 1:50.000 or larger. Not rated or not available Date(s) aerial images were photographed: Oct 3, 2018—Dec 4. **Soil Rating Points** 2018 The orthophoto or other base map on which the soil lines were A/D compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. B/D

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
AsB	Ascalon sandy loam, 0 to 3 percent slopes	В	22.9	32.9%
AvC	Ascalon-Vona sandy loams, 1 to 5 percent slopes	В	40.7	58.4%
TtD	Truckton loamy sand, 3 to 9 percent slopes	А	6.1	8.7%
Totals for Area of Interes	est		69.6	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified

Tie-break Rule: Higher

NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more distalled information in areas where Base Flood Elevations for the control of the

Ceased Base Food Elevations shown on the resp page of principles of of 19 frost American Vertical belows of 188 (NAV) Sol. Users of the FRM should be aware that coastal flood elevations are also provided in the Summay of Sillivate Elevations state in the Flood instances Solly report to the state of the Flood in the Solid Instances Solly report to the Flood Instances Solidy report to the selection and/or floodplain management purposes when they are higher than the elevations shown on the Flood Instances Solid Report Solid Instances S

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Soxyl report for this jurisdiction.

Centein areas not in Special Flood Hazard Areas may be protected by **flood** control structures. Refer to Section 2.4 "Flood Protection Measurer" of the Flood insanae Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercalor (UTM) 2009 15. The horizontal datum was UMASS. GRESTING TO THE PROJECTION OF THE PROJECTI

Flood inventions on this map are referenced to \$0 Morth. American Vertical Dollars of 1986, These flood elevisions must be compared to directain and ground elevations indexended to the same vertical distum. For information reparating conversion between the National discontini Vertical Datum of 1926. Survey whether at http://www.nga.nca.gov/ or contact the National Geodelic Survey at the following address:

NGS Information Services NOAA, NNGS12 National Geodetic Survey SSMC- 3, #9202 1315 East-West Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for banch marks shown on this map, please contact the information Services Branch of the National Geodetic Survey at (301) 713-3242, or visit its website at http://www.ngs.nosa.gov/.

Base map information shown on this FIRM was provided by the Adams County and Commerce City GIS departments. The coordinate system used for the produl of the digital FIRM is Universe Transverse Mercator, Zone 13N, referenced to North American Datum of 1883 and the GRS 80 spharoid, Western Hemisphere.

This may neffects move detailed and up to date attents channel configurations have those the configurations. Then those above on the provious FRM for this jurisdiction. The faccions and floodways that were transferred from the previous FRM may have been adjusted to conform to those may detain channel configurations. As a Study report (which contains authoritative hydraulic date) may reflect stream channel distances that offer from what is shown on this map.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

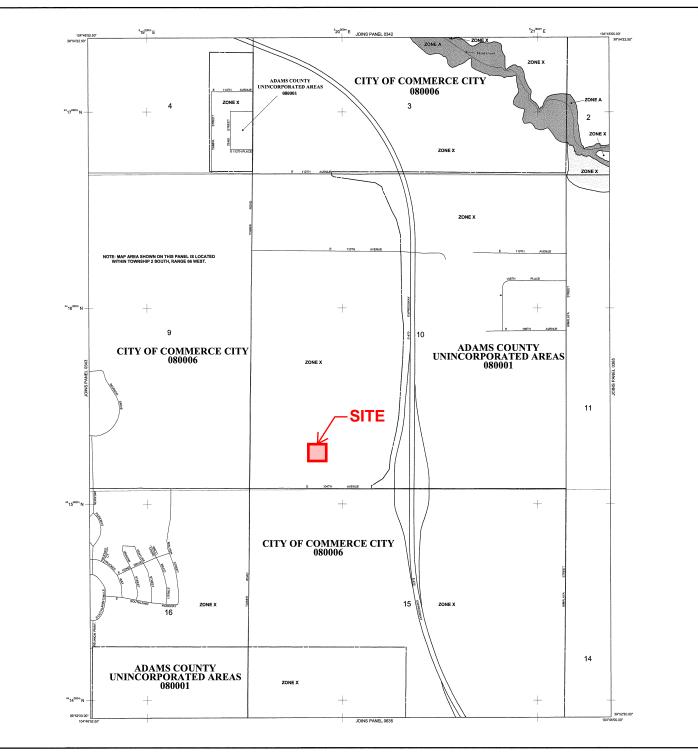
Contact the FEMA Map Service Center at 1-800-368-9616 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study report, and/or digital versions of this map. The FEMA Map Service Center may size be reached by Fax at 1-800-389-3602 and its versions of the size of t

If you have questions about this map or questions concerning the Nationa Flood insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627 or visit the FEMA website at http://www.fema.gov/.

This digital Flood insurance Ratio Map (FRMI) was produced through a cooperative partnership between the State of Colondo Water Contenvictor Board, the United Dislange and Rod Colondo David and the Reddal Enterprising Management Land David Colondo Colondo David Colondo Colondo David Colondo David Colondo Colondo David Colondo Colondo David Colondo Colond







LEGEND

SPECIAL FLOOD HAZARD AREAS (SPHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined. ZONE AH

Flood depths of 1 to 3 feet (usually sheet flow on sloping terrein); average depths determined. For areas of alluvial fan flooding, velocities also determined.

ZONE X

Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with distinge areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

Areas determined to be outside the 0.2% annual chance floodolein

Areas in which flood hazards are undetermined, but possible.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs)

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas

----- Floodway brundary

Zone D boundary CBRS and OPA boundary

Boundary dividing Special Flood Hazard Areas of Base Flood Elevations, flood depths or flood velocities

Base Flood Elevation line and value; elevation in feet*

A Cross section line

② - - - - - ② 97*07'90", 32*22'30"

Geographic coordinates referenced to the North American Detum of 1963 (NAD 83)

oot grid ticks: Alabama State Plane coordinate , east zone (FIPSZONE 0101), Transverse Mercator

Bench mark (see explanation in Notes to Users section of this FIRM panel)

River Mile MAP REPOSITORIES Refer to Map Repositories list on Map Index

August 16, 1985

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL
March 5, 2007 - to update map format.

For community map revision history prior to countywide mapping, refer to the Community Nap History table located in the Flood Insurence Study report for this jurisdiction.

To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood insurance Program at 1-800-638-6620.



PANEL 0344H

FIRM FLOOD INSURANCE RATE MAP ADAMS COUNTY,

COLORADO AND INCORPORATED AREAS

PANEL 344 OF 1150

CONTAINS:

ADAMS COUNTY 080001 0344 H COMMERCE CITY, CITY OF 080006 0344 H



MAP REVISED

08001C0344F

Federal Emergency Management Agency

Reunion Center Filing No. 1, Amendment No. 1 & 2 $_{\rm CORE\ Project\ \#:\ 18-004}$

Prepared By: ACJ

COMPOSITE BASIN - IMPERVIOUSNESS CALCULATIONS

-REFERENCE UDFCD Vol.1 RUNOFF Table 6-3

		Residential			Other				Lav	vns					Soil Type	
		Duet Product	N/A	N/A	N/A	Asphalt	Roof/ Concrete	Gravel	2-7% Slope	>7% Slope	Historic			Soil Type A Area	Soil Type B Area	Soil Type C Area
% Imperv.		65.00%	55.00%	45.00%	85.00%	100.00%	90.00%	40.00%	2.00%	2.00%	2.00%					
	Design											Total	Percent			
BASIN	Point	Area	Area	Area	Area	Area	Area	Area	Area	Area	Area	Area	Impervious	Area	Area	
FILING NO.1, AM	ENDMENT	NO. 1														
A2.1	A2.1	0.09	-	_	-	0.20	0.04	-	0.04	-	-	0.38	79.3%	-	0.38	-
A2.2	A2.2	0.85	-	-	-	0.45	0.09	-	0.08	-	-	1.48	73.9%	-	1.48	-
A3.1	A3.1	0.04	-	-	-	0.09	0.02	=	0.02	-	-	0.17	78.4%	-	0.17	-
A3.2	A3.2	0.28	-	-	-	0.20	0.07	-	0.33	-	-	0.88	51.5%	-	0.88	-
A4.1	A4.1	1.09	-	-	-	0.35	0.02	-	0.54	-	-	2.00	54.3%	-	2.00	-
A4.2	A4.2	0.40	-	-	-	0.25	0.02	-	0.06	-	-	0.73	71.9%	-	0.73	-
B1	B1	1.92	-	-	-	0.67	0.12	-	0.15	-	-	2.86	70.9%	-	2.86	-
B2	B2	0.06	-	-	-	80.0	-	-	0.06	-	-	0.20	62.4%	-	0.20	-
В3	В3	0.69	-	-	-	0.28	0.09	-	0.27	-	-	1.34	61.5%	-	1.34	-
D2	D2	0.38	=	=	=	0.04	0.01	=	0.03	=	-	0.45	64.6%	-	0.45	=
D3	D3	0.44	=	=	=	-	-	=	0.09	=	- 1	0.52	54.7%	-	0.52	=
D2.1	D2.1	0.02	=	ı	=	0.05	-	=	0.00	-	ı	0.06	89.6%	-	0.06	-
D2.2	D2.2	0.05	=	ı	=	0.15	-	=	0.03	-	ı	0.23	79.0%	-	0.23	-
SUBTOTAL		6.32	=	=	=	2.80	0.48	=.	1.70	=	-	11.30	65.3%		11.30	
		-	-	=	=	=	-	=,	=	-	-	-		-	-	=
FILING NO. 1, AM	MENDMENT	NO. 2														
A5.1	A5.1	1.00	=	=	=	0.32	0.01	=	0.00	=	- 1	1.34	73.6%	-	1.34	-
A6.1	A6.1	0.22	=	=	=	0.38	0.02	=	0.03	=	- 1	0.65	82.7%	-	0.65	-
C1.1	C1.1	0.22	=	=	=	0.10	-	=	0.01	=	- 1	0.32	73.7%	-	0.32	-
C2.1	C2.1	0.12	=	=	=	0.05	0.01	=	0.01	=	- 1	0.19	71.5%	-	0.19	-
D1	D1	0.95	-	-	-	-	0.03	-	0.06	-	-	1.03	61.8%	-	1.03	-
D4	D4	0.08	-	-	-	0.09	0.01	-	0.18	-	-	0.37	43.8%	-	0.37	-
D5	D5	0.27	-	-	-	-	0.01	-	0.01	-	-	0.29	64.1%	-	0.29	-
D1.1	D1.1	1	-	-	-	0.06	-	-	-	-	-	0.06	100.0%	-	0.06	-
D1.2	D1.2	-	-	-	-	0.04	0.01	=	0.02	-	-	0.07	63.1%	=	0.07	-
SUBTOTAL A2		2.86	-	-	-	1.03	0.09	=	0.34	-	-	4.32	69.0%	=	4.32	-
		-	-	-	-	-	-	-	-	-	-	-		-	-	-
TOTAL		9.18	-	-	-	3.83	0.58	-	2.03	-	-	15.62	66.3%	-	15.62	-

CORE Project #: 18-004
Prepared By: ACJ

COMPOSITE DEVELOPED BASIN
WEIGHTED "C" CALCULATIONS
-REFERENCE UDFCD Vol.1 RUNOFF Table 6-4

i = % imperviousness/100 expressed as a decimal

C_A = Runoff coefficient for NRCS HSG A soils

C_B = Runoff coefficient for NRCS HSG B soils

 C_{CD} = Runoff coefficient for NRCS HSG C and D soils.

Natural Resource Conservation Service (NRCS)

Table 6-4. Runoff coefficient equations based on NRCS soil group and storm return period

	Andre 0-1. Administrative equations based on three son group and storm retain period														
NRCS				Storm Ret	urn Period										
Soil Group	2-Year	5-Year	10-Year	25-Year	50-Year	100-Year	500-Year								
A	C _A =	C _A =	C _A =	C _A =	C _A =	C _A =	C _A =								
	0.84i ^{1.302}	0.86i ^{1.276}	0.87i ^{1.232}	0.84i ^{1.124}	0.85i+0.025	0.78i+0.110	0.65i+0.254								
В	C _B =	C _B =	C _B =	C _B =	C _B =	C _B =	C _B =								
	0.84i ^{1.169}	0.86i ^{1.088}	0.81i+0.057	0.63i+0.249	0.56i+0.328	0.47i+0.426	0.37i+0.536								
C/D	C _{C/D} =	C _{C/D} =	C _{C/D} =	$C_{C/D} =$	C _{C/D} =	C _{C/D} =	C _{C/D} =								
	0.83i ^{1.122}	0.82i+0.035	0.74i+0.132	0.56i+0.319	0.49i+0.393	0.41i+0.484	0.32i+0.588								

Total Weighted Runoff Coefficients, C												
2-Year	5-Year	10-Year	100-Year									
0.40	0.42	0.45	0.56									

Basin ID	% Imperv.	i	Soil Type	I	Runoff Co	efficients,	С	Basin	Total	W	leighted Runo	ff Coefficients,	С
BUSIII ID	% imperv.	1	3011 Type	2-Year	5-Year	10-Year	100-Year	Area	Area	2-Year	5-Year	10-Year	100-Year
FILING NO.1, AA	VENDWENT NO	D. 1											
			Α	0.62	0.64	0.65	0.73						
A2.1	79.3%	0.79	В	0.64	0.67	0.70	0.80	0.38	0.38	0.64	0.67	0.70	0.80
			C or D	0.64	0.69	0.72	0.81						
			Α	0.57	0.58	0.60	0.69						
A2.2	73.9%	0.74	В	0.59	0.62	0.66	0.77	1.48	1.48	0.59	0.62	0.66	0.77
			C or D	0.59	0.64	0.68	0.79						
			Α	0.61	0.63	0.65	0.72						
A3.1	78.4%	0.78	В	0.63	0.66	0.69	0.79	0.17	0.17	0.63	0.66	0.69	0.79
			C or D	0.63	0.68	0.71	0.81						
			Α	0.35	0.37	0.38	0.51						
A3.2	51.5%	0.52	В	0.39	0.42	0.47	0.67	0.88	0.88	0.39	0.42	0.47	0.67
			C or D	0.39	0.46	0.51	0.70						
			Α	0.38	0.39	0.41	0.53						
A4.1	54.3%	0.54	В	0.41	0.44	0.50	0.68	2.00	2.00	0.41	0.44	0.50	0.68
			C or D	0.42	0.48	0.53	0.71						
			Α	0.55	0.56	0.58	0.67						
A4.2	71.9%	0.72	В	0.57	0.60	0.64	0.76	0.73	0.73	0.57	0.60	0.64	0.76
			C or D	0.57	0.62	0.66	0.78						

Basin ID	97 January	i	Soil Type	ı	Runoff Co	efficients,	С	Basin	Total	l w	eighted Runo	ff Coefficients,	С
Basin ID	% Imperv.	1	Soil Type	2-Year	5-Year	10-Year	100-Year	Area	Area	2-Year	5-Year	10-Year	100-Year
			Α	0.54	0.55	0.57	0.66						
B1	70.9%	0.71	В	0.56	0.59	0.63	0.76	2.86	2.86	0.56	0.59	0.63	0.76
			C or D	0.56	0.62	0.66	0.77						
			Α	0.45	0.47	0.49	0.60						
B2	62.4%	0.62	В	0.48	0.51	0.56	0.72	0.20	0.20	0.48	0.51	0.56	0.72
			C or D	0.49	0.55	0.59	0.74						
			Α	0.45	0.46	0.48	0.59						
В3	61.5%	0.61	В	0.48	0.51	0.55	0.71	1.34	1.34	0.48	0.51	0.55	0.71
			C or D	0.48	0.54	0.59	0.74						
			Α	0.48	0.49	0.51	0.61						
D2	64.6%	0.65	В	0.50	0.53	0.58	0.73	0.45	0.45	0.50	0.53	0.58	0.73
			C or D	0.51	0.57	0.61	0.75						
			Α	0.38	0.40	0.41	0.54						
D3	54.7%	0.55	В	0.41	0.45	0.50	0.68	0.52	0.52	0.41	0.45	0.50	0.68
			C or D	0.42	0.48	0.54	0.71						
			Α	0.73	0.75	0.76	0.81						
D2.1	89.6%	0.90	В	0.74	0.76	0.78	0.85	0.06	0.06	0.74	0.76	0.78	0.85
			C or D	0.73	0.77	0.79	0.85						
			Α	0.62	0.64	0.65	0.73						
D2.2	79.0%	0.79	В	0.64	0.67	0.70	0.80	0.23	0.23	0.64	0.67	0.70	0.80
			C or D	0.64	0.68	0.72	0.81						
FILING NO. 1, A	MENDMENT NO	O. 2											
			Α	0.56	0.58	0.60	0.68						
A5.1	73.6%	0.74	В	0.59	0.62	0.65	0.77	1.34	1.34	0.59	0.62	0.65	0.77
			C or D	0.59	0.64	0.68	0.79						
			Α	0.66	0.68	0.69	0.76						
A6.1	82.7%	0.83	В	0.67	0.70	0.73	0.81	0.65	0.65	0.67	0.70	0.73	0.81
			C or D	0.67	0.71	0.74	0.82						
			Α	0.56	0.58	0.60	0.69						
C1.1	73.7%	0.74	В	0.59	0.62	0.65	0.77	0.32	0.32	0.59	0.62	0.65	0.77
			C or D	0.59	0.64	0.68	0.79						
			Α	0.54	0.56	0.58	0.67						
C2.1	71.5%	0.72	В	0.57	0.60	0.64	0.76	0.19	0.19	0.57	0.60	0.64	0.76
			C or D	0.57	0.62	0.66	0.78						

Desir ID	07 Imamanı	i	Call Tyma	F	Runoff Co	efficients,	С	Basin	Total	W	eighted Runo	ff Coefficients,	С
Basin ID	% Imperv.	1	Soil Type	2-Year	5-Year	10-Year	100-Year	Area	Area	2-Year	5-Year	10-Year	100-Year
			Α	0.29	0.30	0.31	0.45						
D1	43.8%	0.44	В	0.32	0.35	0.41	0.63	1.03	1.03	0.32	0.35	0.41	0.63
			C or D	0.33	0.39	0.46	0.66						
			Α	0.64	0.54	0.65	0.71						
D4	69.0%	0.69	В	0.64	0.57	0.71	0.79	0.37	0.37	0.64	0.57	0.71	0.79
			C or D	0.65	0.60	0.75	0.82						
			Α	0.47	0.49	0.50	0.61						
D5	64.1%	0.64	В	0.50	0.53	0.58	0.73	0.29	0.29	0.50	0.53	0.58	0.73
			C or D	0.50	0.56	0.61	0.75						
			Α	0.84	0.86	0.87	0.89						
D1.1	100.0%	1.00	В	0.84	0.86	0.87	0.90	0.06	0.06	0.84	0.86	0.87	0.90
			C or D	0.83	0.86	0.87	0.89						
			Α	0.46	0.48	0.49	0.60						
D1.2	63.1%	0.63	В	0.49	0.52	0.57	0.72	0.07	0.07	0.49	0.52	0.57	0.72
			C or D	0.50	0.55	0.60	0.74						
			Α	0.52	0.54	0.55	0.65						
SUBTOTAL A2	69.0%	0.69	В	0.54	0.57	0.62	0.75	4.32	4.32	0.54	0.57	0.62	0.75
			C or D	0.55	0.60	0.64	0.77						
										-	-	-	-
			Α	0.49	0.51	0.52	0.63						
TOTAL	66.3%	0.66	В	0.52	0.55	0.59	0.74	15.62	15.62	0.52	0.55	0.59	0.74
			C or D	0.52	0.58	0.62	0.76						

CORE Project #: 18-004
Prepared By: ACJ

TIME OF CONCENTRATION CALCULATIONS

-REFERENCE UDFCD Vol.1 Section 2.4

SF-2

NRCS Conveyance factors, K -REFERENCE UDFCD Vol.1 RUNOFF Table 6-2

Heavy Meadow 2.50 Short Grass Pasture & Lawns 7.00 Grassed Waterway

15.00

Tillage/field 5.00 10.00 Paved Area & Shallow Gutter 20.00 Nearly Bare Ground SUB-BASIN INITIAL / OVERLAND CHANNEL / TRAVEL TIME T(c) CHECK FINAL (URBANIZED BASINS) DATA TIME T(c) T(†) % IMPER-DRAIN AREA C(5) Slope Coeff. Velocity T(†) COMP. USDCM Length Slope T(i) Length VIOUS **BASIN** % ac. ft. % min ft. fps min. T(c) Eq. 6-5 min. 17 0.9 20 A2.1 0.38 0.67 2.0 2.6 422 1.9 3.6 6.2 79.3% 16.1 6.2 A2.2 0.62 2.6 3.4 478 20 3.8 7.2 73.9% 7.2 1.48 28 1.1 2.1 17.4 A3.1 0.17 0.66 17 2.0 2.6 166 1.0 20 2.0 1.4 4.0 78.4% 14.1 5.0 A3.2 0.88 0.42 57 2.0 7.4 280 1.3 20 2.3 2.1 9.5 51.5% 19.8 9.5 A4.1 2.00 0.44 70 0.7 11.0 574 0.7 20 1.7 5.6 16.6 54.3% 23.5 16.6 A4.2 0.73 0.60 2.0 5.8 248 0.7 20 1.7 2.4 8.2 71.9% 16.3 8.2 66 В1 2.86 0.59 76 0.8 8.6 596 0.7 20 1.6 14.8 70.9% 20.4 14.8 6.1 B2 0.20 0.51 63 2.0 6.7 75 1.2 20 2.2 0.6 7.2 62.4% 16.0 7.2 В3 1.34 0.51 94 2.0 8.3 385 1.3 20 2.3 2.8 11.1 61.5% 18.7 11.1 D2 0.45 0.53 87 7.6 20 2.0 162 0.6 1.5 1.8 9.4 64.6% 17.0 9.4 D3 0.45 0.7 20 20.9 0.52 78 2.0 8.3 358 1.7 3.5 11.8 54.7% 11.8 D2.1 0.06 0.76 8 2.0 1.4 120 1.4 20 2.4 8.0 2.2 89.6% 11.6 5.0 D2.2 0.23 0.67 20 2.0 2.8 203 1.4 20 2.4 1.4 4.2 79.0% 14.0 5.0 SUBTOTAL 11.30 0.00 0 0.0 65.3% 5.0 A5.1 1.34 0.62 27 1.3 20 2.1 73.6% 18.0 8.6 4.2 553 1.1 4.4 8.6 A6.1 0.65 0.70 32 0.1 10.5 359 1.2 20 2.2 2.7 13.2 82.7% 14.6 13.2 C1.1 0.32 0.62 2.0 2.9 0.7 20 2.4 73.7% 16.0 18 239 1.6 5.4 5.4 C2.1 20 71.5% 0.19 0.60 66 2.0 5.9 102 0.7 1.7 1.0 6.9 14.9 6.9 D1 1.03 0.35 64 2.0 8.6 995 8.0 20 1.8 9.0 17.7 61.8% 25.7 17.7 D4 0.37 0.57 31 1.0 5.3 498 1.0 20 2.0 4.1 9.3 43.8% 23.9 9.3 D5 0.29 0.53 1.0 5.7 1.0 20 2.0 9.8 64.1% 19.6 9.8 31 498 4.1 D1.1 0.06 0.86 2.0 159 1.0 20 2.0 100.0% 10.1 5.0 0.3 1.3 1.7 D1.2 0.07 0.52 26 2.0 4.2 40 1.0 20 2.0 0.3 4.6 63.1% 15.6 5.0 SUBTOTAL A2 4.32 0.57 69.0% 5.0 0 TOTAL 15.62 0.55 66.3% 5.0 0

 CORE Project #:
 18-004

 Prepared By:
 ACJ

RATIONAL METHOD PEAK RUNOFF

5-Year STORM Rainfall Depth-Duration-Frequency (1-hr) = 1.12

SF-3

-REFERENCE UDFCD Vol.1 EQ 5-1 & EQ 6-1

Е	BASIN INFORMATOR	1		DIR	ECT RUN	OFF	
DESIGN	DRAIN	AREA	5yr Runoff	T(c)	СхА	I	Q
POINT	BASIN	ac.	COEFF	min		in/hr	cfs
A2.1	A2.1	0.38	0.67	6.2	0.25	3.58	0.90
A2.2	A2.2	1.48	0.62	7.2	0.92	3.41	3.13
A3.1	A3.1	0.17	0.66	5.0	0.11	3.80	0.42
A3.2	A3.2	0.88	0.42	9.5	0.37	3.10	1.14
A4.1	A4.1	2.00	0.44	16.6	0.88	2.42	2.14
A4.2	A4.2	0.73	0.60	8.2	0.44	3.26	1.43
B1	B1	2.86	0.59	14.8	1.69	2.56	4.34
B2	B2	0.20	0.51	7.2	0.10	3.41	0.35
В3	В3	1.34	0.51	11.1	0.68	2.91	1.97
D2	D2	0.45	0.53	9.4	0.24	3.11	0.75
D3	D3	0.52	0.45	11.8	0.23	2.83	0.66
D2.1	D2.1	0.06	0.76	5.0	0.05	3.80	0.19
D2.2	D2.2	0.23	0.67	5.0	0.15	3.80	0.58
	SUBTOTAL	11.30		5.0		3.80	0.00
	FILING NO. 1,	AMENDME	NT NO. 2				
A5.1	A5.1	1.34	0.62	8.6	0.82	3.21	2.64
A6.1	A6.1	0.65	0.70	13.2	0.45	2.69	1.22
C1.1	C1.1	0.32	0.62	5.4	0.20	3.73	0.75
C2.1	C2.1	0.19	0.60	6.9	0.12	3.46	0.40
D1	D1	1.03	0.35	17.7	0.36	2.35	0.85
D4	D4	0.37	0.57	9.3	0.21	3.11	0.67
D5	D5	0.29	0.53	9.8	0.15	3.06	0.47
D1.1	D1.1	0.06	0.86	5.0	0.05	3.80	0.19
D1.2	D1.2	0.07	0.52	5.0	0.03	3.80	0.13
	SUBTOTAL A2	4.32		5.0		3.80	0.00
	TOTAL	15.62		5.0		3.80	0.00

 CORE Project #:
 18-004

 Prepared By:
 ACJ

RATIONAL METHOD PEAK RUNOFF

100-YR STORM

SF-3 Rainfall Depth-Duration-Frequency (1-hr) = 2.53

-REFERENCE UDFCD Vol.1 EQ 5-1 & EQ 6-1

B.A	ASIN INFORMATO	DIR	ECT RUN	OFF			
DESIGN	DRAIN	AREA	100YR RUNNOFF	T(c)	СхА	I	Q
POINT	BASIN	ac.	COEFF	min		in/hr	cfs
A2.1	A2.1	0.38	0.80	6.18	0.302	8.086	2.44
A2.2	A2.2	1.48	0.77	7.18	1.143	7.714	8.82
A3.1	A3.1	0.17	0.79	5.00	0.133	8.581	1.14
A3.2	A3.2	0.88	0.67	9.45	0.590	6.995	4.13
A4.1	A4.1	2.00	0.68	16.59	1.360	5.472	7.44
A4.2	A4.2	0.73	0.76	8.24	0.558	7.360	4.10
B1	B1	2.86	0.76	14.76	2.174	5.788	12.58
B2	B2	0.20	0.72	7.24	0.144	7.692	1.11
В3	В3	1.34	0.71	11.10	0.955	6.563	6.27
D2	D2	0.45	0.73	9.38	0.330	7.016	2.32
D3	D3	0.52	0.68	11.82	0.357	6.392	2.28
D2.1	D2.1	0.06	0.85	5.00	0.055	8.581	0.47
D2.2	D2.2	0.23	0.80	5.00	0.183	8.581	1.57
	SUBTOTAL	11.30					
			MENT NO. 2				
A5.1	A5.1	1.34	0.77	8.58	1.031	7.251	7.47
A6.1	A6.1	0.65	0.81	13.25	0.528	6.081	3.21
C1.1	C1.1	0.32	0.77	5.37	0.250	8.419	2.11
C2.1	C2.1	0.19	0.76	6.87	0.147	7.823	1.15
D1	D1	1.03	0.63	17.67	0.653	5.304	3.46
D4	D4	0.37	0.79	9.34	0.296	7.028	2.08
D5	D5	0.29	0.73	9.79	0.209	6.903	1.44
D1.1	D1.1	0.06	0.90	5.00	0.052	8.581	0.44
D1.2	D1.2	0.07	0.72	5.00	0.047	8.581	0.41
	SUBTOTAL A2	4.32					
	TOTAL	15.62					

	RUNOFF SUMMARY TABLE												
	DIRE	CT RUNOF	F										
		AREA	5-Year RUNOFF	100-Year RUNOFF									
DESIGN POINT	BASIN	(AC)	(CFS)	(CFS)									
	LING NO. 1,		ENT NO. 1										
A2.1	A2.1	0.38	0.90	2.44									
A2.2	A2.2	1.48	3.13	8.82									
A3.1	A3.1	0.17	0.42	1.14									
A3.2	A3.2	0.88	1.14	4.13									
A4.1	A4.1	2.00	2.14	7.44									
A4.2	A4.2	0.73	1.43	4.10									
B1	B1	2.86	4.34	12.58									
B2	B2	0.20	0.35	1.11									
B3	B3	1.34	1.97	6.27									
D2	D2	0.45	0.75	2.32									
D3	D3	0.52	0.66	2.28									
D2.1	D2.1	0.06	0.19	0.47									
D2.2	D2.2	0.23	0.58	1.57									
SUBTOTAL		11.30	17.99	54.67									
FI	LING NO. 1,	AMENDMI	ENT NO. 2										
A5.1	A5.1	1.34	2.64	7.47									
A6.1	A6.1	0.65	1.22	3.21									
C1.1	C1.1	0.32	0.75	2.11									
C2.1	C2.1	0.19	0.40	1.15									
D1	D1	1.03	0.85	3.46									
D4	D4	0.37	0.67	2.08									
D5	D5	0.29	0.47	1.44									
D1.1	D1.1	0.06	0.19	0.44									
D1.2	D1.2	0.07	0.13	0.41									
SUBTOTAL A2		4.32	7.30	21.77									
_				_									

CORE Project #: 14-004
Prepared By: -LH

IMPERVIOUS CALCULATIONS

-REFERENCE UDFCD Vol.1 RUNOFF Table 6-3

			Residential 8	& Commercia	l											
			Single Family	,	Multi-Family				Landsca	ipe Area		_		Soil Type		
		0.25 acres or less	0.25 - 0.75 acres	2.5 acres or larger	Attached	Roof/ Concrete	Asphalt/ Ponded Water	Packed Gravel	2-7% Slope	>7% Slope	Historic			Soil Type A Area	Soil Type B Area	Soil Type C/D Area
% Imperv.		45.00%	30.00%	12.00%	75.00%	90.00%	100.00%	40.00%	2.00%	2.00%	2.00%					
	Design		•	•			•	•		•		Total	Percent			
BASIN	Point	Area (ac)	Area (ac)	Area (ac)	Area (ac)	Area (ac)	Area (ac)	Area (ac)	Area (ac)	Area (ac)	Area (ac)	Area (ac)	Impervious	Area (ac)	Area (ac)	Area (ac)
H1	H1	-	-	-	-	-	-	-	-	-	5.85	5.85	2.0%	-	-	5.85
H2	H2	-	-	-	-	-	-	-	-	-	11.52	11.52	2.0%	-	-	11.52
		-	-	-	-	-	-	-	-	-	-	-		-	-	-
TOTAL		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	17.37	17.37	2.0%			

CORE Project #: 14-004
Prepared By: -LH

COMPOSITE DEVELOPED BASIN WEIGHTED "C" CALCULATIONS -REFERENCE UDFCD Vol.1 RUNOFF Table 6-4

i = % imperviousness/100 expressed as a decimal

C_A = Runoff coefficient for NRCS HSG A soils

$$\begin{split} &C_{\text{B}} = \text{Runoff coefficient for NRCS HSG B soils} \\ &C_{\text{CD}} = \text{Runoff coefficient for NRCS HSG C and D soils}. \end{split}$$

Natural Resource Conservation Service (NRCS)

Table 6-4. Runoff coefficient equations based on NRCS soil group and storm return period

NRCS			Storm Return Period					
Soil Group	2-Year	5-Year	10-Year	25-Year	50-Year	100-Year	500-Year	
A	C _A =	C _A =	C _A =	C _A =	C _A =	C _A =	C _A =	
	$0.84i^{1.302}$	0.86i ^{1.276}	0.87i ^{1.232}	$0.84i^{1.124}$	0.85i+0.025	0.78i+0.110	0.65i+0.25	
В	C _B =	C _B =	C _B =	C _B =	C _B =	C _B =	C _B =	
	$0.84i^{1.169}$	0.86i ^{1.088}	0.81i+0.057	0.63i+0.249	0.56i+0.328	0.47i+0.426	0.37i+0.53	
C/D	C _{C/D} =	C _{C/D} =	C _{C/D} =	C _{C/D} =	C _{C/D} =	C _{C/D} =	C _{C/D} =	
	$0.83i^{1.122}$	0.82i+0.035	0.74i+0.132	0.56i+0.319	0.49i+0.393	0.41i+0.484	0.32i+0.58	

	_							
1	Total Weighted Runoff Coefficients, C							
	2-Year	5-Year	10-Year	100-Year				
	0.01	0.05	0.15	0.49				
	W	Weighted Runoff Coefficients, C						
	2-Year	5-Year	10-Year	100-Year				
	_		_					

Basin ID	% Imperv.		Soil Type	F	Runoff Co	efficients,	C	Basin	Total	W	eighted Runof	f Coefficients,	С
Busin ID	∕₀ iiiipeiv.	•	3011 Type	2-Year	5-Year	10-Year	100-Year	Area	Area	2-Year	5-Year	10-Year	100-Year
			Α	0.01	0.01	0.01	0.13						
H1	2.0%	0.02	В	0.01	0.01	0.07	0.44		5.85	0.01	0.05	0.15	0.49
			C or D	0.01	0.05	0.15	0.49	5.85					
			Α	0.01	0.01	0.01	0.13						
H2	2.0%	0.02	В	0.01	0.01	0.07	0.44		11.52	0.01	0.05	0.15	0.49
			C or D	0.01	0.05	0.15	0.49	11.52					

CORE Project #: 14-004
Prepared By: -LH

TIME OF CONCENTRATION CALCULATIONS | BASIN A

-REFERENCE UDFCD Vol.1 Section 2.4 NRCS Conveyance factors, K -REFERENCE UDFCD Vol.1 RUNOFF Table 6-2

SF-2 Heavy Meadow 3 Short Grass Pasture & Lawns 7 Grassed Waterway 15

Tillage/field 5 Nearly Bare Ground 10 Paved Area & Shallow Gutter 20

	SUB-BASIN		INIT	TAL / OVER	LAND	CHAN	INEL / TRAV	/EL TIME				T(c) (CHECK	FINAL
	DATA			TIME			T(†)					(URBANIZ	ED BASINS)	T(c)
DRAIN	AREA	C(5)	Length	Slope	T(i)	Length	Slope	Coeff.	Velocity	T(†)	COMP.	% IMPER-	USDCM	
BASIN	ac.		ft.	%	min	ft.	%		fps	min.	T(c)	VIOUS	Eq . 6-5	min.
H1	5.85	0.05	78	9.5	8.0	949	0.7	7	0.6	27.7	35.7	2.0%		35.7
H2	11.52	0.05	294	3.3	22.0	942	0.4	7	0.5	34.2	56.2	2.0%		56.2

CORE Project #: 14-004
Prepared By: -LH

RATIONAL METHOD PEAK RUNOFF

5-Year STORM Rainfall Depth-Duration-Frequency (1-hr) = 1.12

SF-3

-REFERENCE UDFCD Vol.1 EQ 5-1 & EQ 6-1

BASI	n informa	NOT	DIRECT RUNOFF				
DESIGN	DRAIN	AREA	5yr Runoff	T(c)	СхА	I	Q
POINT	BASIN	ac.	COEFF	min		in/hr	cfs
H1	H1	5.85	0.05	35.7	0.30	1.58	0.48
H2	H2	11.52	0.05	56.2	0.59	1.18	0.70
	TOTAL	17.37	0.05		0.89		1.18

 CORE Project #:
 14-004

 Prepared By:
 -LH

RATIONAL METHOD PEAK RUNOFF

100-YR STORM

SF-3 Rainfall Depth-Duration-Frequency (1-hr) = 2.53

-REFERENCE UDFCD Vol.1 EQ 5-1 & EQ 6-1

ВА	BASIN INFORMATON					OFF	
DESIGN	DRAIN	AREA	100YR RUNNOFF	T(c)	СхА		Q
POINT	BASIN	ac.	COEFF	min		in/hr	cfs
H1	H1	5.85	0.49	35.7	2.88	3.58	10.30
H2	H2	11.52	0.49	56.2	5.67	2.67	15.15
	TOTAL	17.37	0.49		8.55		25.45

	RUNOFF SUMMARY TABLE							
DIRECT RUNOFF								
DESIGN AREA RUNOFF RUNOF POINT BASIN (AC) (CFS) (CFS)								
H1	H1	5.85	0.48	10.30				
H2	H2	11.52	0.70	15.15				
Total		17.37	1.18	25.45				

12/4/2023 Page 6 of 6

APPENDIX B HYDRAULIC COMPUTATIONS

MHFD-Inlet, Version 5.02 (August 2022) INLET MANAGEMENT

Worksheet Protected

Major Flow Bypassed Downstream, Q_b (cfs)

INLET NAME

Site Type (Urban or Rural)	URBAN		
	UKDAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET	STREET
Hydraulic Condition	In Sump	In Sump	In Sump
Inlet Type	CDOT Type R Curb Opening	CDOT Type R Curb Opening	CDOT Type R Curb Opening
SER-DEFINED INPUT			
User-Defined Design Flows			
Minor Q _{Known} (cfs)	2.1	1.4	3.1
Major Q _{Known} (cfs)	7.4	4.1	8.8
Bypass (Carry-Over) Flow from Upstream	Inlets must be organized from upstream	am (left) to downstream (right) in order f	or bypass flows to be linked.
Receive Bypass Flow from:	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Received
Minor Bypass Flow Received, Q _b (cfs)	0.0	0.0	0.0
Major Bypass Flow Received, Q _b (cfs)	0.0	0.0	0.0
Watershed Characteristics Subcatchment Area (acres)			
Percent Impervious			
NRCS Soil Type			
Overland Slope (ft/ft) Overland Length (ft)			
Overland Length (ft) Channel Slope (ft/ft)			
Overland Length (ft)			
Overland Length (ft) Channel Slope (ft/ft) Channel Length (ft) Minor Storm Rainfall Input			
Overland Length (ft) Channel Slope (ft/ft) Channel Length (ft) Minor Storm Rainfall Input Design Storm Return Period, T _r (years)			
Overland Length (ft) Channel Slope (ft/ft) Channel Length (ft) Minor Storm Rainfall Input			
Overland Length (ft) Channel Slope (ft/ft) Channel Length (ft) Minor Storm Rainfall Input Design Storm Return Period, T _r (years) One-Hour Precipitation, P ₁ (inches)			
Overland Length (ft) Channel Slope (ft/ft) Channel Length (ft) Minor Storm Rainfall Input Design Storm Return Period, T _r (years) One-Hour Precipitation, P ₁ (inches) Major Storm Rainfall Input			
Overland Length (ft) Channel Slope (ft/ft) Channel Length (ft) Minor Storm Rainfall Input Design Storm Return Period, T _r (years) One-Hour Precipitation, P ₁ (inches)			

Inlet A4.2

N/A

Inlet A2.2

N/A

Inlet A4.1

N/A

MHFD-Inlet, Version 5.02 (August 2022) INLET MANAGEMENT

Worksheet Protected

INLET NAME	Inlet A2.1	Inlet D2.1	Inlet D2.2
Site Type (Urban or Rural)	URBAN	URBAN	URBAN
nlet Application (Street or Area)	STREET	STREET	STREET
Hydraulic Condition	In Sump	In Sump	In Sump
Inlet Type	CDOT Type R Curb Opening	CDOT/Denver 13 Valley Grate	CDOT Type R Curb Opening
SER-DEFINED INPUT			
User-Defined Design Flows			
Minor Q _{Known} (cfs)	0.9	0.2	0.6
Major Q _{Known} (cfs)	2.4	0.5	1.6
Bypass (Carry-Over) Flow from Upstream	•		
Receive Bypass Flow from:	User-Defined	No Bypass Flow Received	No Bypass Flow Received
Minor Bypass Flow Received, Q _b (cfs)	3.0	0.0	0.0
Major Bypass Flow Received, Q _b (cfs)	8.7	0.0	0.0
Watershed Characteristics			
Subcatchment Area (acres)			
Percent Impervious			
NRCS Soil Type			
Watershed Profile			
Overland Slope (ft/ft)			
Overland Length (ft)			
Channel Slope (ft/ft)			
Channel Length (ft)			
Minor Storm Rainfall Input		1	
Design Storm Return Period, T _r (years)			
One-Hour Precipitation, P ₁ (inches)			
Major Storm Rainfall Input			
Design Storm Return Period, T _r (years)			
One-Hour Precipitation, P_1 (inches)			

Minor Total Design Peak Flow, Q (cfs)	3.9	0.2	0.6
Major Total Design Peak Flow, Q (cfs)	11.2	0.5	1.6
Minor Flow Bypassed Downstream, Q _b (cfs)	N/A	N/A	N/A
Major Flow Bypassed Downstream, Q _b (cfs)	N/A	N/A	N/A

MHFD-Inlet, Version 5.02 (August 2022) INLET MANAGEMENT

Worksheet Protected

URBAN STREET In Sump T Type R Curb Opening 0.4 1.1	URBAN STREET In Sump CDOT Type R Curb Opening 1.1 4.1	URBAN STREET In Sump CDOT Type R Curb Opening 4.3 12.6
In Sump T Type R Curb Opening 0.4	In Sump CDOT Type R Curb Opening 1.1	In Sump CDOT Type R Curb Opening 4.3
T Type R Curb Opening 0.4	CDOT Type R Curb Opening 1.1	CDOT Type R Curb Opening 4.3
0.4	1.1	4.3
1.1	4.1	12.6
User-Defined	No Bypass Flow Received	No Bypass Flow Received
1.0	0.0	0.0
4.0	0.0	0.0
	1.0	1.0 0.0

MHFD-Inlet, Version 5.02 (August 2022)

INLET MANAGEMENT

Worksheet Protected

INLET NAME	Inlet B3	
Site Type (Urban or Rural)	URBAN	
Inlet Application (Street or Area)	STREET	
Hydraulic Condition	In Sump	
Inlet Type	CDOT Type R Curb Opening	

USER-DEFINED INPUT

User-Defined Design Flows		
Minor Q _{Known} (cfs)	2.3	
Major Q _{Known} (cfs)	7.4	

Bypass (Carry-Over) Flow from Upstream

Receive Bypass Flow from:	No Bypass Flow Received	
Minor Bypass Flow Received, Q _b (cfs)	0.0	
Major Bypass Flow Received, Q _b (cfs)	0.0	

Watershed Characteristics

Subcatchment Area (acres)	
Percent Impervious	
NRCS Soil Type	

Watershed Profile

Overland Slope (ft/ft)	
Overland Length (ft)	
Channel Slope (ft/ft)	
Channel Length (ft)	

Minor Storm Rainfall Input

Design Storm Return Period	, T _r (years)	
One-Hour Precipitation, P ₁ (inches)	

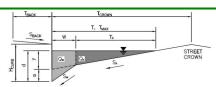
Major Storm Rainfall Input

Design Storm Return Period, T _r (years)	
One-Hour Precipitation, P ₁ (inches)	

CALCULATED OUTPUT

Minor Total Design Peak Flow, Q (cfs)	2.3
Major Total Design Peak Flow, Q (cfs)	7.4
Minor Flow Bypassed Downstream, Q _b (cfs)	N/A
Major Flow Bypassed Downstream, Q _b (cfs)	N/A

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Reunion Center Filing 1 - Amendment 1 - Basins Inlet ID: Inlet A4.1 ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)



Gutter Geometry: Maximum Allowable Width for Spread Behind Curb

Side Slope Behind Curb (leave blank for no conveyance credit behind curb) Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line Distance from Curb Face to Street Crown

Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

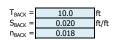
Manning's Roughness for Street Section (typically between 0.012 and 0.020)

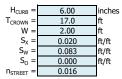
Max. Allowable Spread for Minor & Major Storm

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

Check boxes are not applicable in SUMP conditions

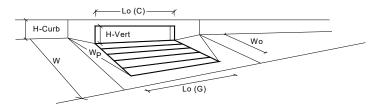
MINOR STORM Allowable Capacity is not applicable to Sump Condition MAJOR STORM Allowable Capacity is not applicable to Sump Condition





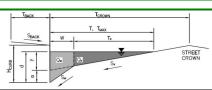
	Minor Storm	Major Storm	
$T_{MAX} =$	17.0	17.0	ft
$d_{MAX} =$	6.0	8.4	inches
_			_

	Minor Storm	Major Storm	
$Q_{allow} =$	SUMP	SUMP	cfs



Design Information (Input) CDOT Type R Curb Opening		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	2	2	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	6.0	inches
Grate Information	_	MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_o(G) =$	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C₀ (G) =	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	=" _
Length of a Unit Curb Opening	$L_o(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	Trt.
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.33	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	 "`
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.91	0.93	
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	N/A	N/A	
The state of the s	· · · Combination —	, .	.41.	_
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	$Q_a =$	6.9	8.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	Q PEAK REQUIRED =	2.1	7.4	cfs

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Reunion Center Filing 1 - Amendment 1 - Basins Inlet ID: Inlet A4.2 ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)



Gutter Geometry: Maximum Allowable Width for Spread Behind Curb

Side Slope Behind Curb (leave blank for no conveyance credit behind curb) Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line Distance from Curb Face to Street Crown

Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

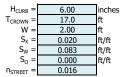
Max. Allowable Spread for Minor & Major Storm

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

Check boxes are not applicable in SUMP conditions

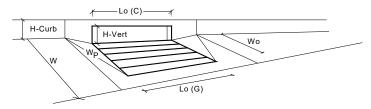
MINOR STORM Allowable Capacity is not applicable to Sump Condition MAJOR STORM Allowable Capacity is not applicable to Sump Condition

T_{BACK} = 10.0 0.020 ft/ft S_{BACK} 0.018



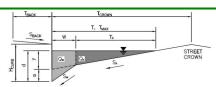
	Minor Storm	Major Storm	
$T_{MAX} =$	17.0	17.0	ft
$d_{MAX} =$	6.0	8.4	inches
_			_

Minor Storm **SUMP** Major Storm SUMP



Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =		Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	5.6	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_o(G) =$	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C₀ (G) =	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	=' -
Length of a Unit Curb Opening	$L_o(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	Tπ
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.30	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	1
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	1
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	N/A	N/A	
	-	*****	*****	
L		MINOR	MAJOR	7.4.
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	4.6 1.4	4.6 4.1	cfs cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	Q PEAK REQUIRED =	1.4	4.1	us

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Reunion Center Filing 1 - Amendment 1 - Basins Inlet ID: Inlet A2.2 ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)



Gutter Geometry: Maximum Allowable Width for Spread Behind Curb

Side Slope Behind Curb (leave blank for no conveyance credit behind curb) Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line Distance from Curb Face to Street Crown

Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

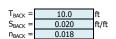
Manning's Roughness for Street Section (typically between 0.012 and 0.020)

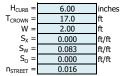
Max. Allowable Spread for Minor & Major Storm

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

Check boxes are not applicable in SUMP conditions

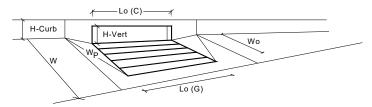
MINOR STORM Allowable Capacity is not applicable to Sump Condition MAJOR STORM Allowable Capacity is not applicable to Sump Condition





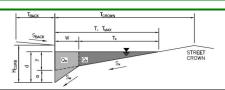
	Minor Storm	Major Storm	
$T_{MAX} =$	17.0	17.0	ft
$d_{MAX} =$	2.0	2.0	inches

	Minor Storm	Major Storm	
$Q_{allow} =$	SUMP	SUMP	cfs



Design Information (Input) CDOT Type R Curb Opening		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	2.0	2.0	inches
Grate Information	_	MINOR	MAJOR	Override Depths
Length of a Unit Grate	L ₀ (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	$A_{ratio} =$	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_o(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ſπ
Depth for Curb Opening Weir Equation	d _{Curb} =	0.02	0.02	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	1
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.79	0.79	1
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	N/A	N/A	
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes cloqged condition)	Q _a =	0.1	0.1	cfs
WARNING: Inlet Capacity < Q Peak for Minor and Major Storms	Q PEAK REQUIRED =	3.1	8.8	cfs
Transfer and Capacity - Q I can for Pintor and Piajor Storins	I. I			1

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Reunion Center Filing 1 - Amendment 1 - Basins Inlet ID: Inlet A2.1 ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)



Gutter Geometry: Maximum Allowable Width for Spread Behind Curb

Side Slope Behind Curb (leave blank for no conveyance credit behind curb) Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line

Distance from Curb Face to Street Crown

Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

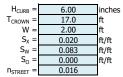
Max. Allowable Spread for Minor & Major Storm

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

Check boxes are not applicable in SUMP conditions

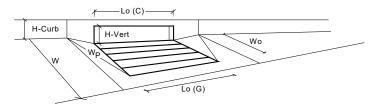
MINOR STORM Allowable Capacity is not applicable to Sump Condition MAJOR STORM Allowable Capacity is not applicable to Sump Condition

T_{BACK} : 10.0 0.020 ft/ft S_{BACK} 0.018



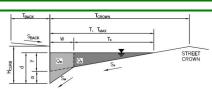
	Minor Storm	Major Storm	
$T_{MAX} =$	17.0	17.0	ft
d _{MAX} =	6.0	8.4	inches
-			

Q _{allow} =	SUMP	SUMP	cfs
	Minor Storm	Major Storm	



Design Information (Input) CDOT Type R Curb Opening		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	3	3	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	6.9	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	feet
Width of a Unit Grate	$W_o =$	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	$A_{ratio} =$	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_o(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	$H_{vert} =$	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	lft .
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.41	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	1
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.76	0.84	
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	N/A	N/A	1
	Combinación	·		_
		MINOR	MAJOR	-
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	6.5	11.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	Q PEAK REQUIRED =	3.9	11.2	cfs

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Reunion Center Filing 1 - Amendment 1 - Basins Inlet ID: Inlet D2.1 ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)



Gutter Geometry: Maximum Allowable Width for Spread Behind Curb

Side Slope Behind Curb (leave blank for no conveyance credit behind curb) Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line Distance from Curb Face to Street Crown

Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

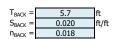
Manning's Roughness for Street Section (typically between 0.012 and 0.020)

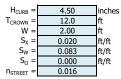
Max. Allowable Spread for Minor & Major Storm

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

Check boxes are not applicable in SUMP conditions

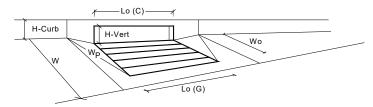
MINOR STORM Allowable Capacity is not applicable to Sump Condition MAJOR STORM Allowable Capacity is not applicable to Sump Condition





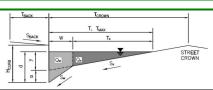
	Minor Storm	Major Storm	
$T_{MAX} =$	12.0	12.0	ft
$d_{MAX} =$	4.5	6.0	inches

	Minor Storm	Major Storm	
$Q_{allow} =$	SUMP	SUMP	cfs



MINOR	MAJOR	
DOT/Denver 1	13 Valley Grate	
2.00	2.00	inches
1	1	
4.4	4.4	inches
MINOR	MAJOR	Override Depths
3.00	3.00	feet
	1.73	feet
0.43	0.43	
0.50	0.50	
	3.30	
0.60	0.60	
MINOR	MAJOR	_
	N/A	feet
	-	inches
	N/A	inches
N/A	N/A	degrees
	N/A	feet
	N/A	
N/A	N/A	
MINOR	MAJOR	
		Trt.
N/A	N/A	ft
0.69	0.69	
N/A	N/A	
N/A	N/A	
MINIOD	MAIOD	
		cfs
0.2	0.5	cfs
	2.00 1 4.4 MINOR 3.00 1.73 0.43 0.50 3.30 0.60 MINOR N/A	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Reunion Center Filing 1 - Amendment 1 - Basins Inlet ID: Inlet D2.2 ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)



Gutter Geometry: Maximum Allowable Width for Spread Behind Curb

Side Slope Behind Curb (leave blank for no conveyance credit behind curb) Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line

Distance from Curb Face to Street Crown

Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

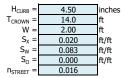
Max. Allowable Spread for Minor & Major Storm

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

Check boxes are not applicable in SUMP conditions

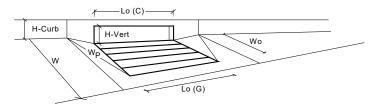
MINOR STORM Allowable Capacity is not applicable to Sump Condition MAJOR STORM Allowable Capacity is not applicable to Sump Condition

$T_{BACK} =$	16.0	ft
$S_{BACK} =$	0.020	ft/ft
n _{BACK} =	0.018	



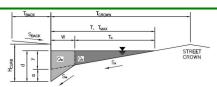
	Minor Storm	Major Storm	
T _{MAX} =	14.0	14.0	ft
d _{MAX} =	4.5	6.0	inches
-			

	Minor Storm	Major Storm	
$Q_{allow} =$	SUMP	SUMP	cfs



Design Information (Input) CDOT Type R Curb Opening		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	4.50	4.50	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	4.5	4.9	inches
Grate Information	_	MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_o(G) =$	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C₀ (G) =	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	=" _
Length of a Unit Curb Opening	$L_o(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	Trt.
Depth for Curb Opening Weir Equation	d _{Curb} =	0.21	0.24	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	1"
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	N/A	N/A	1
	· ·· Combination [.4	⊒
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	$Q_a =$	2.7	3.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	Q PEAK REQUIRED =	0.6	1.6	cfs

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Reunion Center Filing 1 - Amendment 1 - Basins Inlet ID: Inlet A3.1 ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)



Gutter Geometry: Maximum Allowable Width for Spread Behind Curb

Side Slope Behind Curb (leave blank for no conveyance credit behind curb) Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line Distance from Curb Face to Street Crown

Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

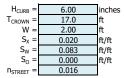
Max. Allowable Spread for Minor & Major Storm

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

Check boxes are not applicable in SUMP conditions

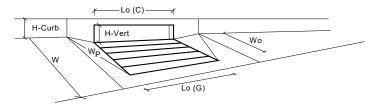
MINOR STORM Allowable Capacity is not applicable to Sump Condition MAJOR STORM Allowable Capacity is not applicable to Sump Condition

T_{BACK} : 10.0 0.020 ft/ft S_{BACK} 0.018



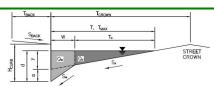
	Minor Storm	Major Storm	
$T_{MAX} =$	17.0	17.0	ft
d _{MAX} =	6.0	8.4	inches
-			

Q _{allow} =	SUMP	SUMP	cfs
	Minor Storm	Maior Storm	



Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	1
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	2	2	1
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	5.6	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_o(G) =$	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C₀ (G) =	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	=' -
Length of a Unit Curb Opening	$L_o(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	Tπ
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.30	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	1
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.91	0.91	1
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	N/A	N/A	
	_			
L	- F	MINOR	MAJOR	٦,
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	6.9	6.9	cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	Q PEAK REQUIRED =	1.5	5.2	cfs

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Reunion Center Filing 1 - Amendment 1 - Basins Inlet ID: Inlet A3.2 ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)



Gutter Geometry: Maximum Allowable Width for Spread Behind Curb Side Slope Behind Curb (leave blank for no conveyance credit behind curb) Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line Distance from Curb Face to Street Crown Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

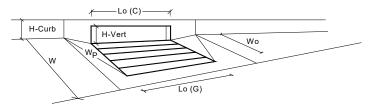
Max. Allowable Spread for Minor & Major Storm Max. Allowable Depth at Gutter Flowline for Minor & Major Storm Check boxes are not applicable in SUMP conditions

MINOR STORM Allowable Capacity is not applicable to Sump Condition MAJOR STORM Allowable Capacity is not applicable to Sump Condition

T _{BACK} =	10.0	lft .
S _{BACK} =	0.020	ft/ft
n _{BACK} =	0.018	1910
· · · DACK	0.010	ı
H _{CURB} =	6.00	inches
$T_{CROWN} =$	17.0	ft
W =	2.00	ft
$S_X =$	0.000	ft/ft
$S_W =$	0.083	ft/ft
$S_0 =$	0.000	ft/ft
n _{STREET} =	0.016	
•		•

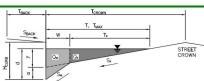
	Minor Storm	Major Storm	
$T_{MAX} =$	17.0	17.0	ft
$d_{MAX} =$	2.0	2.0	inches
-		П	_

	Minor Storm	Major Storm	
$Q_{allow} =$	SUMP	SUMP	cfs



Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	2.0	2.0	inches
Grate Information	_	MINOR	MAJOR	Override Depths
Length of a Unit Grate	L_o (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_o(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	$H_{vert} =$	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ſπ
Depth for Curb Opening Weir Equation	d _{Curb} =	0.02	0.02	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	1"
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.79	0.79	
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	N/A	N/A	
	Combination L	,	,,,,	
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	0.1	0.1	cfs
WARNING: Inlet Capacity < Q Peak for Minor and Major Storms	Q PEAK REQUIRED =	1.1	4.1	cfs

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Reunion Center Filing 1 - Amendment 1 - Basins Inlet ID: Inlet B1 ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)



Gutter Geometry: Maximum Allowable Width for Spread Behind Curb

Side Slope Behind Curb (leave blank for no conveyance credit behind curb) Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line Distance from Curb Face to Street Crown

Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

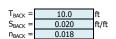
Manning's Roughness for Street Section (typically between 0.012 and 0.020)

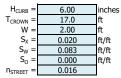
Max. Allowable Spread for Minor & Major Storm

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

Check boxes are not applicable in SUMP conditions

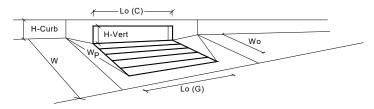
MINOR STORM Allowable Capacity is not applicable to Sump Condition MAJOR STORM Allowable Capacity is not applicable to Sump Condition





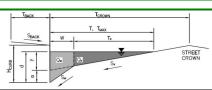
	Minor Storm	Major Storm	
$T_{MAX} =$	17.0	17.0	ft
d _{MAX} =	6.0	8.4	inches
-			

Q _{allow} =	SUMP	SUMP	cfs
	Minor Storm	Major Storm	



Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =		Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	3	3	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	7.5	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_o(G) =$	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C₀ (G) =	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	=' -
Length of a Unit Curb Opening	$L_o(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	Tπ
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.46	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	1
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.76	0.87	1
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	N/A	N/A	
	-	*****	*****	
		MINOR	MAJOR	7.4.
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	6.5 4.3	14.0 12.6	cfs cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	Q PEAK REQUIRED =	4.3	12.0	us

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Reunion Center Filing 1 - Amendment 1 - Basins Inlet ID: Inlet B3 ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)



Gutter Geometry: Maximum Allowable Width for Spread Behind Curb

Side Slope Behind Curb (leave blank for no conveyance credit behind curb) Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line Distance from Curb Face to Street Crown

Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

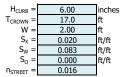
Max. Allowable Spread for Minor & Major Storm

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

Check boxes are not applicable in SUMP conditions

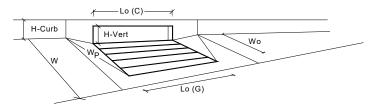
MINOR STORM Allowable Capacity is not applicable to Sump Condition MAJOR STORM Allowable Capacity is not applicable to Sump Condition

T_{BACK} : 10.0 0.020 ft/ft S_{BACK} 0.018



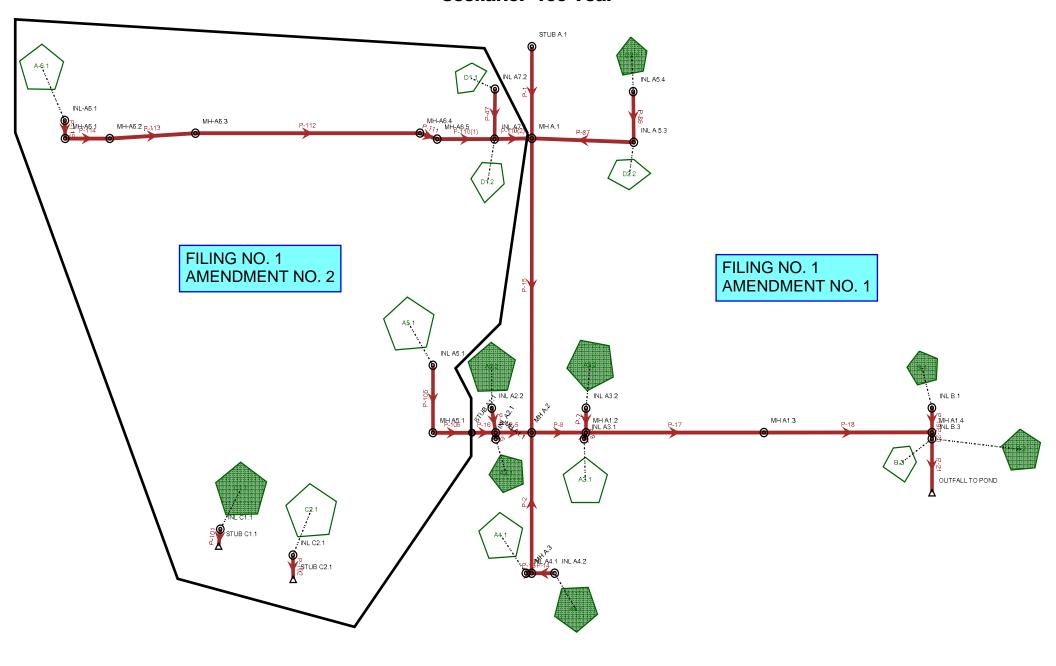
	Minor Storm	Major Storm	
$T_{MAX} =$	17.0	17.0	ft
d _{MAX} =	6.0	8.4	inches
-			

Q _{allow} =	SUMP	SUMP	cfs
	Minor Storm	Major Storm	



Design Information (Input) CDOT Type R Curb Opening		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	2	2	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	5.8	inches
Grate Information	_	MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_o(G) =$	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	
Length of a Unit Curb Opening	$L_o(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	Tπ
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.32	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.91	0.92	
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	N/A	N/A	
	-	*****	*****	
Tabel Talet Tatananting Consider (assumes also and assubition)	o -	MINOR	MAJOR	7-6-
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	6.9 2.3	7.6 7.4	cfs cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	Q PEAK REQUIRED =	2.3	7.4	us

Scenario: 100-Year



STORMCAD OUTPUT TABLES - REUNION CENTER FILING NO. 1, AMENDMENT NO. 1 5-Year Storm Event

Catchment Table - Time: 0.00 hours

Label	Outflow Element	Area (User Defined) (acres)	Runoff Coefficient (Rational)	Time of Concentration (min)	Catchment Intensity (in/h)	Catchment Rational Flow (cfs)
A2.2	INL A2.2	1.480	0.620	7.180	3.415	3.16
A3.2	INL A3.2	0.880	0.420	9.450	3.097	1.15
A3.1	INL A3.1	0.170	0.660	5.000	3.799	0.43
A2.1	INL A2.1	0.380	0.670	6.180	3.579	0.92
A4.1	INL A4.1	2.000	0.440	16.600	2.422	2.15
A4.2	INL A4.2	0.730	0.600	8.240	3.258	1.44
B.1	INL B.1	2.860	0.590	14.760	2.562	4.36
B.3	INL B.3	1.340	0.510	11.100	2.905	2.00
B.2	INL B.3	0.200	0.510	7.240	3.405	0.35
D2.1	INL A5.4	0.060	0.760	5.000	3.799	0.17
D2.2	INL A 5.3	0.230	0.670	5.000	3.799	0.59

Conduit Table - Time: 0.00 hours

Label	Notes	Start Node	Stop Node	Invert (Start)	Invert (Stop)	Length (ft)	Slope (Calculated)	Diameter (in)	Manning's n	Flow (cfs)	Velocity (ft/s)	Hydraulic Grade Line	Hydraulic Grade Line	Capacity (cfs)	Energy Grade Line	Energy Grade Line
				(ft)	(ft)	, ,	(ft/ft)	` ,		` '		(In) (ft)	(Out) (ft)		(In) (ft)	(Out) (ft)
P-1	24" RCP	STUB A.1	MH A.1	5,221.23	5,220.96	100.8	0.003	24.0	0.013	3.94	3.36	5,222.15	5,222.07	11.71	5,222.27	5,222.15
P-2	24" RCP	MH A.3	MH A.2	5,220.07	5,219.61	154.4	0.003	24.0	0.013	3.21	3.30	5,221.23	5,221.20	12.35	5,221.27	5,221.22
P-4	18" RCP	INL A2.2	MH A1.1	5,220.45	5,220.31	27.4	0.005	18.0	0.013	3.16	4.03	5,221.43	5,221.42	7.43	5,221.53	5,221.50
P-5	30" RCP	MH A1.1	MH A.2	5,220.11	5,219.89	42.7	0.005	30.0	0.013	6.32	4.75	5,221.19	5,221.20	29.17	5,221.34	5,221.29
P-6	18" RCP	INL A2.1	MH A1.1	5,220.35	5,220.31	7.0	0.005	18.0	0.013	0.92	2.86	5,221.42	5,221.42	7.43	5,221.42	5,221.42
P-7	18" RCP	INL A3.2	MH A1.2	5,219.72	5,219.29	27.0	0.016	18.0	0.013	1.15	4.61	5,220.79	5,220.79	13.26	5,220.80	5,220.79
P-8	18" RCP	MH A.2	MH A1.2	5,219.41	5,219.09	64.3	0.005	36.0	0.013	13.33	5.73	5,220.76	5,220.79	47.06	5,221.05	5,220.95
P-9	18" RCP	INL A3.1	MH A1.2	5,219.35	5,219.29	7.3	0.008	18.0	0.013	0.43	2.73	5,220.79	5,220.79	9.53	5,220.79	5,220.79
P-13	18" RCP	INL A4.1	MH A.3	5,220.30	5,220.26	6.8	0.006	24.0	0.013	2.15	3.76	5,221.27	5,221.27	17.34	5,221.31	5,221.30
P-14	18" RCP	INL A4.2	MH A.3	5,220.41	5,220.27	27.2	0.005	24.0	0.013	1.44	3.19	5,221.27	5,221.27	16.23	5,221.29	5,221.29
P-15	24" RCP	MH A.1	MH A.2	5,220.76	5,219.88	323.5	0.003	24.0	0.013	5.73	3.73	5,221.74	5,221.20	11.80	5,221.96	5,221.31
P-16	18" RCP	STUB A1.1	MH A1.1	5,221.24	5,221.10	28.3	0.005	18.0	0.013	2.63	3.83	5,221.86	5,221.72	7.39	5,222.09	5,221.95
P-17	18" RCP	MH A1.2	MH A1.3	5,218.89	5,217.83	210.8	0.005	36.0	0.013	14.39	5.87	5,220.10	5,218.97	47.29	5,220.55	5,219.50
P-18	18" RCP	MH A1.3	MH A1.4	5,217.64	5,216.64	199.1	0.005	36.0	0.013	14.22	5.84	5,218.84	5,218.32	47.16	5,219.29	5,218.51
P-19	18" RCP	INL B.1	MH A1.4	5,217.11	5,216.84	27.0	0.010	18.0	0.013	4.36	5.67	5,218.33	5,218.32	10.50	5,218.46	5,218.41
P-20	18" RCP	MH A1.4	INL B.3	5,216.44	5,216.40	7.0	0.005	36.0	0.013	17.83	6.21	5,217.79	5,217.71	47.16	5,218.31	5,218.28
P-21	18" RCP	INL B.3	OUTFALL TO POND	5,216.20	5,215.91	58.9	0.005	36.0	0.013	19.57	6.36	5,217.62	5,217.26	47.16	5,218.17	5,217.89
P-86	18" RCP	INL A5.4	INL A 5.3	5,221.87	5,221.60	25.5	0.011	18.0	0.013	0.17	2.27	5,222.08	5,222.09	10.81	5,222.10	5,222.09
P-87	18" RCP	INL A 5.3	MH A.1	5,221.40	5,220.86	52.3	0.010	18.0	0.013	0.76	3.49	5,222.07	5,222.07	10.67	5,222.08	5,222.08

STORMCAD OUTPUT TABLES - REUNION CENTER FILING NO. 1, AMENDMENT NO. 1 5-Year Storm Event

Manhole Table - Time: 0.00 hours

Label	Elevation (Rim) (ft)	Elevation (Invert) (ft)	Flow (Local Surface) (cfs)	Flow (Local from Inflow Collection)	Flow (Total Out) (cfs)	Headloss Method	Headloss Coeff.
	(10)	(10)	(CI3)	(cfs)	(CI3)		
STUB A.1	5,226.82	(N/A)	0.00	3.94	3.94	Standard	0.050
MH A1.4	5,224.41	5,216.64	0.00	0.00	17.83	Standard	1.020
MH A1.3	5,226.25	5,217.83	0.00	0.00	14.22	Standard	0.050
MH A1.2	5,224.95	5,219.09	0.00	0.00	14.39	Standard	1.520
MH A1.1	5,224.92	5,220.31	0.00	0.00	6.32	Standard	1.520
MH A.3	5,223.98	5,220.26	0.00	0.00	3.21	Standard	1.020
MH A.2	5,225.59	5,219.88	0.00	0.00	13.33	Standard	1.520
MH A.1	5,228.87	5,220.96	0.00	0.00	5.73	Standard	1.520
INL B.3	5,224.64	5,216.40	2.30	0.00	19.57	Standard	0.050
INL B.1	5,224.64	(N/A)	4.36	0.00	4.36	Standard	0.050
INL A5.4	5,228.14	(N/A)	0.17	0.00	0.17	Standard	0.050
INL A4.2	5,224.21	(N/A)	1.44	0.00	1.44	Standard	0.050
INL A4.1	5,224.21	(N/A)	2.15	0.00	2.15	Standard	0.050
INL A3.2	5,225.21	(N/A)	1.15	0.00	1.15	Standard	0.050
INL A3.1	5,225.19	(N/A)	0.43	0.00	0.43	Standard	0.050
INL A2.2	5,225.17	(N/A)	3.16	0.00	3.16	Standard	0.050
INL A2.1	5,225.15	(N/A)	0.92	0.00	0.92	Standard	0.050
INL A 5.3	5,228.01	5,221.60	0.59	0.00	0.76	Standard	1.320

Outfall Table - Time: 0.00 hours

Label	Notes	Elevation (Invert) (ft)	Flow (Total Out) (cfs)	Boundary Condition Type
OUTFALL TO POND	Dummy Null Structure for LandXML purposes	5,215.91	19.51	Free Outfall

STORMCAD OUTPUT TABLES - REUNION CENTER FILING NO. 1, AMENDMENT NO. 1 100-Year Storm Event

Catchment Table - Time: 0.00 hours

Label	Outflow Element	Area (User Defined)) Coefficient Concentration		Catchment Intensity	Catchment Rational Flow
		(acres)	(Rational)	(min)	(in/h) ´	(cfs)
A2.2	INL A2.2	1.480	0.770	7.180	7.713	8.86
A3.2	INL A3.2	0.880	0.670	9.450	6.996	4.16
A3.1	INL A3.1	0.170	0.790	5.000	8.581	1.16
A2.1	INL A2.1	0.380	0.800	6.180	8.086	2.48
A4.1	INL A4.1	2.000	0.680	16.600	5.470	7.50
A4.2	INL A4.2	0.730	0.760	8.240	7.359	4.12
B.1	INL B.1	2.860	0.760	14.760	5.787	12.68
B.3	INL B.3	1.340	0.710	11.100	6.563	6.29
B.2	INL B.3	0.200	0.720	7.240	7.692	1.12
D2.1	INL A5.4	0.060	0.850	5.000	8.581	0.44
D2.2	INL A 5.3	0.230	0.800	5.000	8.581	1.59

Conduit Table - Time: 0.00 hours

Label	Notes	Start Node	Stop Node	Invert (Start)	Invert (Stop)	Length (ft)	Slope (Calculated)	Diameter (in)	Manning's	Flow (cfs)	Velocity (ft/s)	Hydraulic Grade Line	Hydraulic Grade Line	Capacity (cfs)	Energy Grade Line	Energy Grade Line
				(ft)	(ft)	(1.5)	(ft/ft)	()		(0.0)	(195)	(In) (ft)	(Out) (ft)	(0.3)	(In) (ft)	(Out) (ft)
P-1	24" RCP	STUB A.1	MH A.1	5,221.23	5,220.96	100.8	0.003	24.0	0.013	8.25	2.63	5,224.54	5,224.40	11.71	5,224.65	5,224.51
P-2	24" RCP	MH A.3	MH A.2	5,220.07	5,219.61	154.4	0.003	24.0	0.013	10.54	3.36	5,223.32	5,222.98	12.35	5,223.49	5,223.16
P-4	18" RCP	INL A2.2	MH A1.1	5,220.45	5,220.31	27.4	0.005	18.0	0.013	8.86	5.01	5,223.56	5,223.37	7.43	5,223.95	5,223.76
P-5	30" RCP	MH A1.1	MH A.2	5,220.11	5,219.89	42.7	0.005	30.0	0.013	17.68	3.60	5,223.06	5,222.98	29.17	5,223.26	5,223.18
P-6	18" RCP	INL A2.1	MH A1.1	5,220.35	5,220.31	7.0	0.005	18.0	0.013	2.48	1.40	5,223.37	5,223.37	7.43	5,223.40	5,223.40
P-7	18" RCP	INL A3.2	MH A1.2	5,219.72	5,219.29	27.0	0.016	18.0	0.013	4.16	2.35	5,222.28	5,222.24	13.26	5,222.37	5,222.32
P-8	18" RCP	MH A.2	MH A1.2	5,219.41	5,219.09	64.3	0.005	36.0	0.013	34.74	4.91	5,222.41	5,222.24	47.06	5,222.79	5,222.61
P-9	18" RCP	INL A3.1	MH A1.2	5,219.35	5,219.29	7.3	0.008	18.0	0.013	1.16	0.66	5,222.24	5,222.24	9.53	5,222.24	5,222.24
P-13	18" RCP	INL A4.1	MH A.3	5,220.30	5,220.26	6.8	0.006	24.0	0.013	7.50	2.39	5,223.50	5,223.50	17.34	5,223.59	5,223.58
P-14	18" RCP	INL A4.2	MH A.3	5,220.41	5,220.27	27.2	0.005	24.0	0.013	4.12	1.31	5,223.50	5,223.50	16.23	5,223.53	5,223.52
P-15	24" RCP	MH A.1	MH A.2	5,220.76	5,219.88	323.5	0.003	24.0	0.013	12.77	4.07	5,224.01	5,222.98	11.80	5,224.27	5,223.24
P-16	18" RCP	STUB A1.1	MH A1.1	5,221.24	5,221.10	28.3	0.005	18.0	0.013	7.40	4.19	5,223.51	5,223.37	7.39	5,223.78	5,223.64
P-17	18" RCP	MH A1.2	MH A1.3	5,218.89	5,217.83	210.8	0.005	36.0	0.013	38.21	7.45	5,220.95	5,220.50	47.29	5,221.80	5,221.01
P-18	18" RCP	MH A1.3	MH A1.4	5,217.64	5,216.64	199.1	0.005	36.0	0.013	37.85	7.42	5,220.48	5,219.87	47.16	5,220.94	5,220.32
P-19	18" RCP	INL B.1	MH A1.4	5,217.11	5,216.84	27.0	0.010	18.0	0.013	12.68	7.18	5,220.26	5,219.87	10.50	5,221.06	5,220.67
P-20	18" RCP	MH A1.4	INL B.3	5,216.44	5,216.40	7.0	0.005	36.0	0.013	48.15	7.60	5,218.95	5,218.91	47.16	5,219.85	5,219.82
P-21	18" RCP	INL B.3	OUTFALL TO POND	5,216.20	5,215.91	58.9	0.005	36.0	0.013	53.49	7.57	5,218.86	5,218.29	47.16	5,219.88	5,219.52
P-86	18" RCP	INL A5.4	INL A 5.3	5,221.87	5,221.60	25.5	0.011	18.0	0.013	0.44	0.25	5,224.44	5,224.44	10.81	5,224.44	5,224.44
P-87	18" RCP	INL A 5.3	MH A.1	5,221.40	5,220.86	52.3	0.010	18.0	0.013	1.87	1.06	5,224.42	5,224.40	10.67	5,224.44	5,224.42

STORMCAD OUTPUT TABLES - REUNION CENTER FILING NO. 1, AMENDMENT NO. 1 100-Year Storm Event

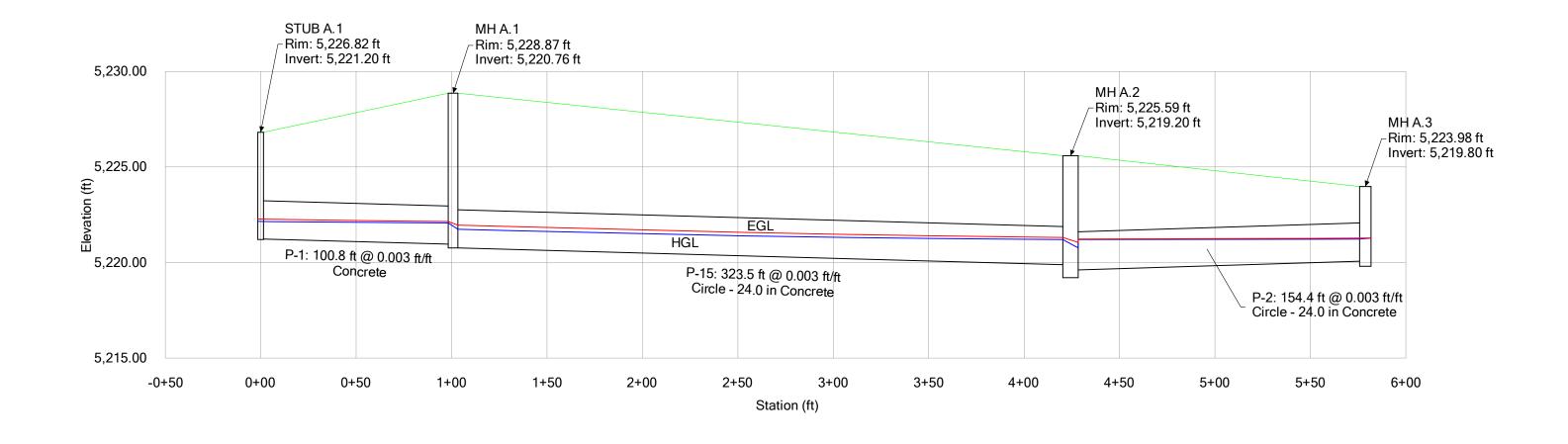
Manhole Table - Time: 0.00 hours

Label	Elevation (Rim) (ft)	Elevation (Invert) (ft)	Flow (Local Surface) (cfs)	Flow (Local from Inflow Collection)	Flow (Total Out) (cfs)	Headloss Method	Headloss Coeff.
	(-3)	(1.5)	(5.5)	(cfs)	(5.5)		
STUB A.1	5,226.82	(N/A)	0.00	8.25	8.25	Standard	0.050
MH A1.4	5,224.41	5,216.64	0.00	0.00	48.15	Standard	1.020
MH A1.3	5,226.25	5,217.83	0.00	0.00	37.85	Standard	0.050
MH A1.2	5,224.95	5,219.09	0.00	0.00	38.21	Standard	1.520
MH A1.1	5,224.92	5,220.31	0.00	0.00	17.68	Standard	1.520
MH A.3	5,223.98	5,220.26	0.00	0.00	10.54	Standard	1.020
MH A.2	5,225.59	5,219.88	0.00	0.00	34.74	Standard	1.520
MH A.1	5,228.87	5,220.96	0.00	0.00	12.77	Standard	1.520
INL B.3	5,224.64	5,216.40	7.25	0.00	53.49	Standard	0.050
INL B.1	5,224.64	(N/A)	12.68	0.00	12.68	Standard	0.050
INL A5.4	5,228.14	(N/A)	0.44	0.00	0.44	Standard	0.050
INL A4.2	5,224.21	(N/A)	4.12	0.00	4.12	Standard	0.050
INL A4.1	5,224.21	(N/A)	7.50	0.00	7.50	Standard	0.050
INL A3.2	5,225.21	(N/A)	4.16	0.00	4.16	Standard	0.050
INL A3.1	5,225.19	(N/A)	1.16	0.00	1.16	Standard	0.050
INL A2.2	5,225.17	(N/A)	8.86	0.00	8.86	Standard	0.050
INL A2.1	5,225.15	(N/A)	2.48	0.00	2.48	Standard	0.050
INL A 5.3	5,228.01	5,221.60	1.59	0.00	1.87	Standard	1.320

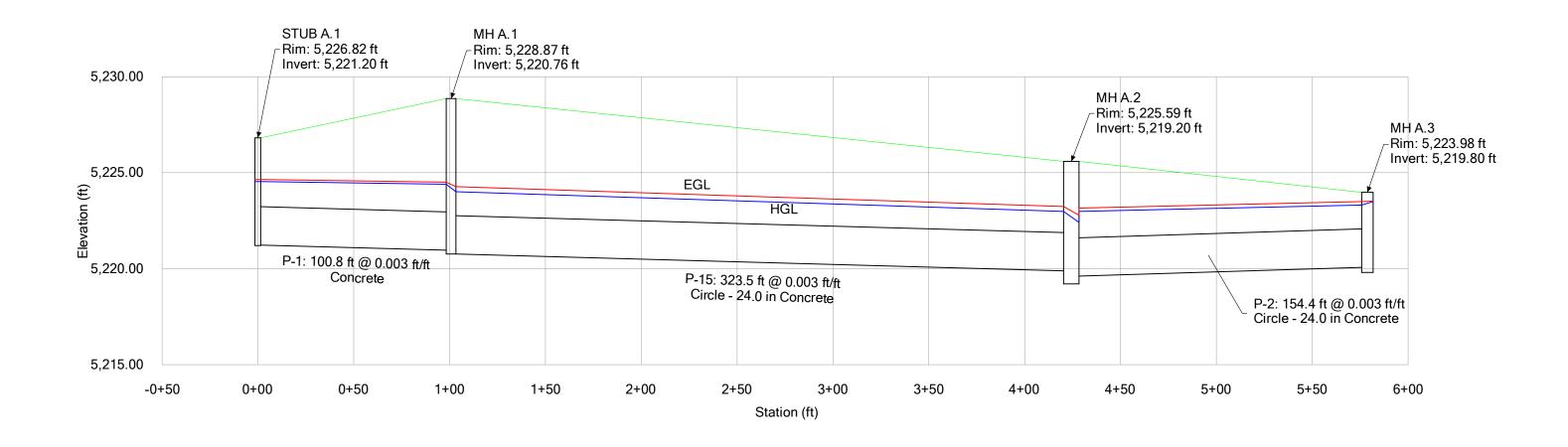
Outfall Table - Time: 0.00 hours

Label	Notes	Elevation (Invert) (ft)	Flow (Total Out) (cfs)	Boundary Condition Type
OUTFALL TO POND	Dummy Null Structure for LandXML purposes	5,215.91	53.34	Free Outfall

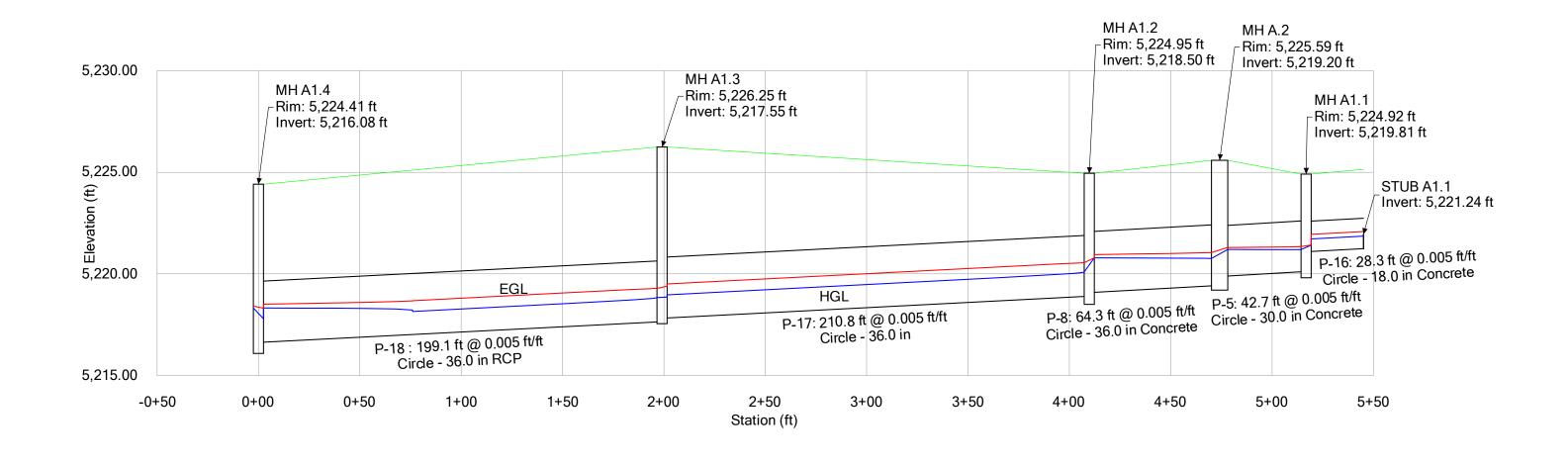
Profile Report Engineering Profile - 1 - STUB A.1-MH A.3 (Reunion Center StormCAD Model ACJ.stsw)



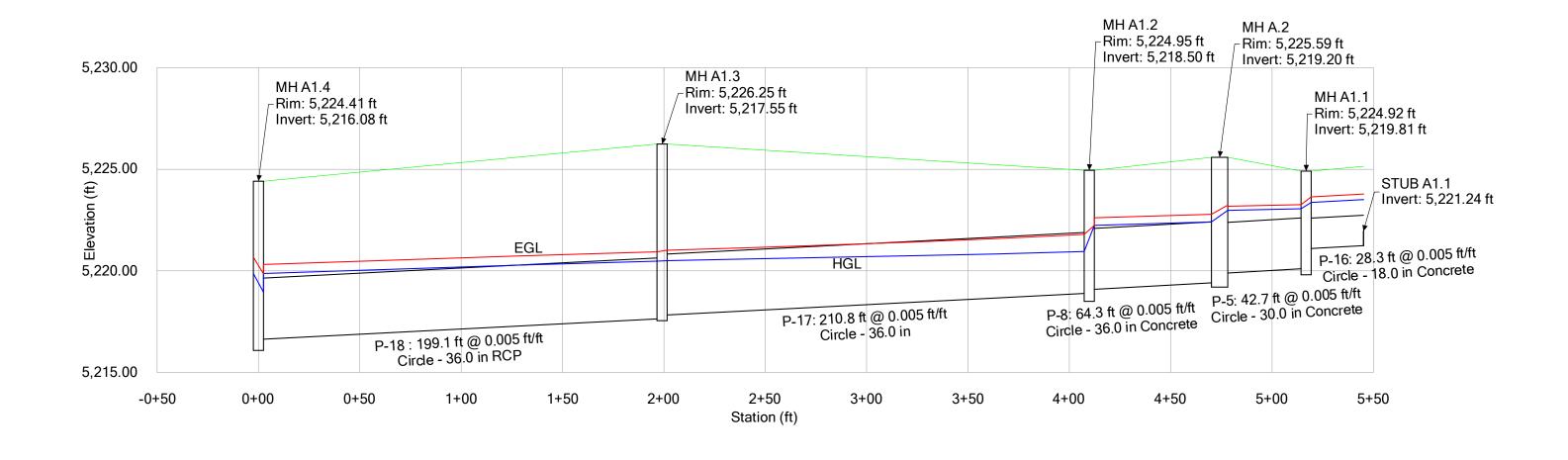
Profile Report Engineering Profile - 1 - STUB A.1-MH A.3 (Reunion Center StormCAD Model ACJ.stsw)



Profile Report Engineering Profile - 3 - STUB A1.1-MH A1.4 (Reunion Center StormCAD Model ACJ.stsw)

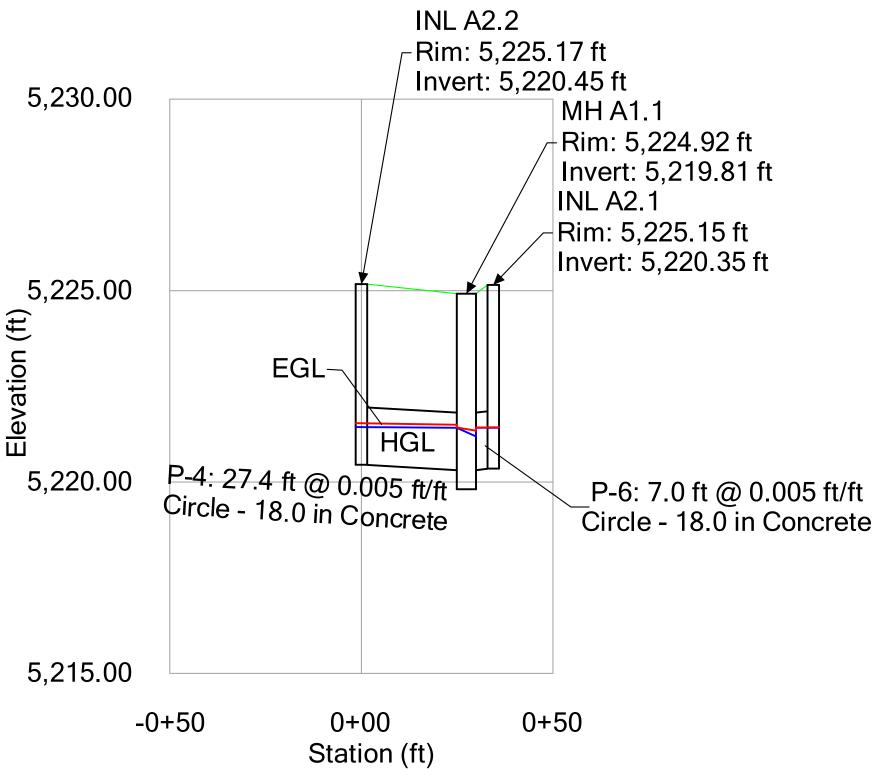


Profile Report Engineering Profile - 3 - STUB A1.1-MH A1.4 (Reunion Center StormCAD Model ACJ.stsw)



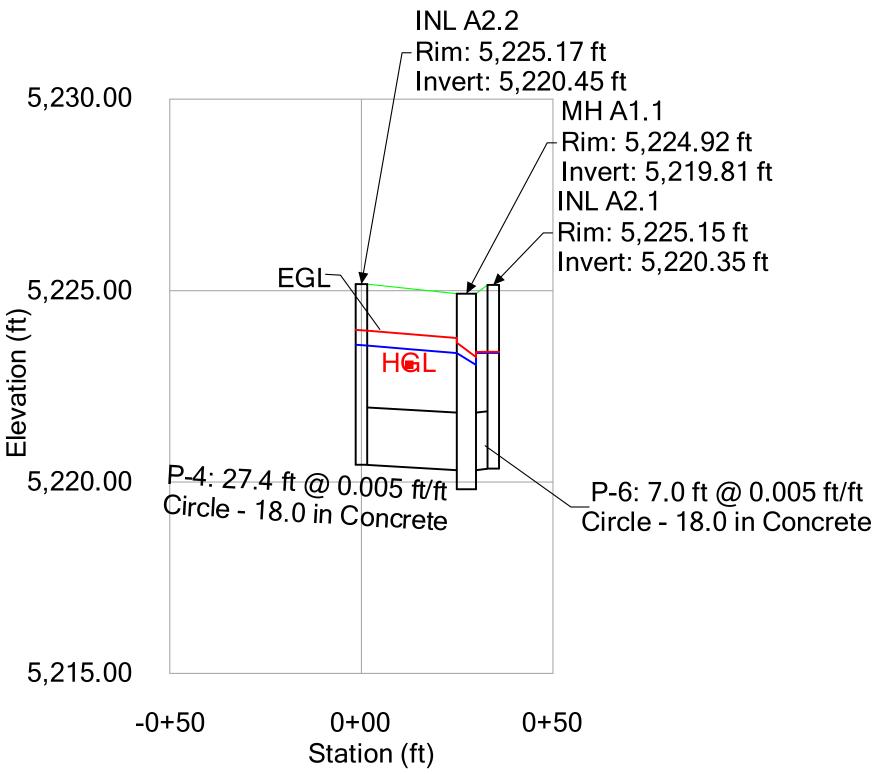
Profile Report

Engineering Profile - 4 - INL A2.2-INL A2.1 (Reunion Center StormCAD Model ACJ.stsw)



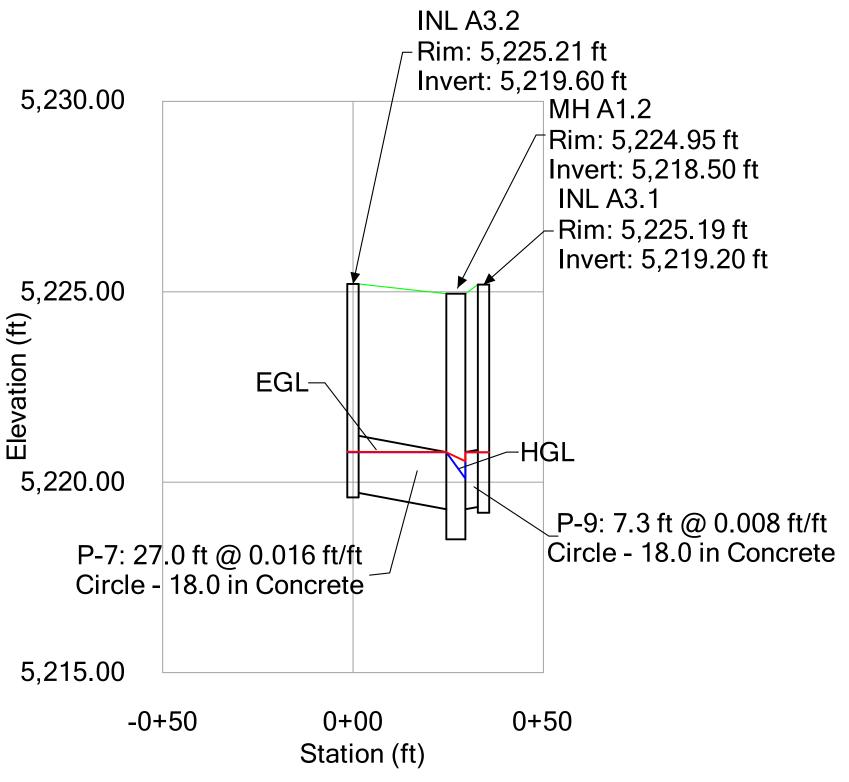
Profile Report

Engineering Profile - 4 - INL A2.2-INL A2.1 (Reunion Center StormCAD Model ACJ.stsw)



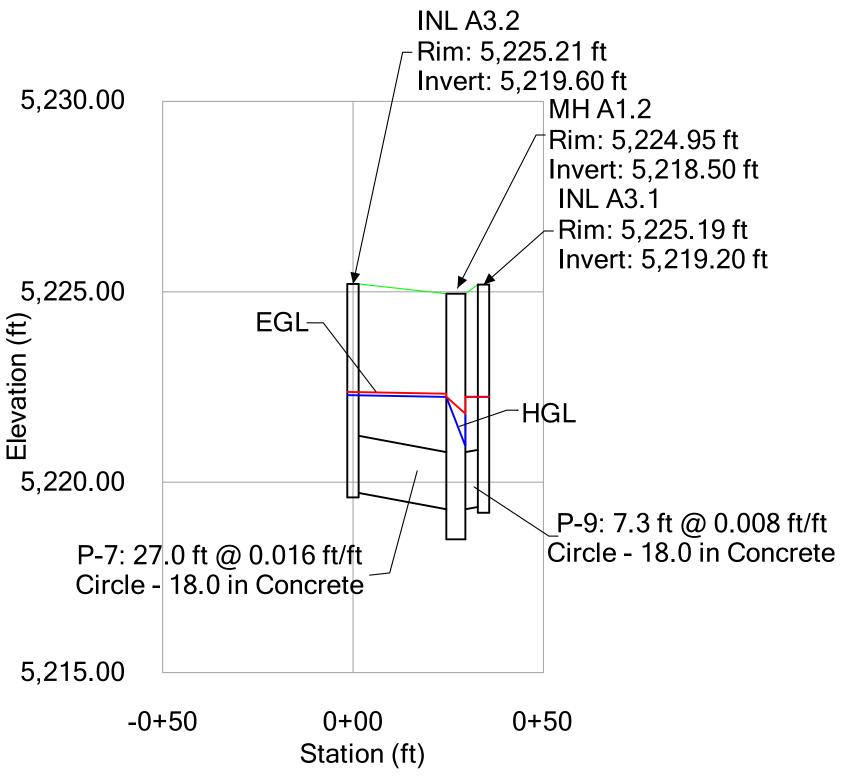
Profile Report

Engineering Profile - 5 - INL A3.2-INL A3.1 (Reunion Center StormCAD Model ACJ.stsw)



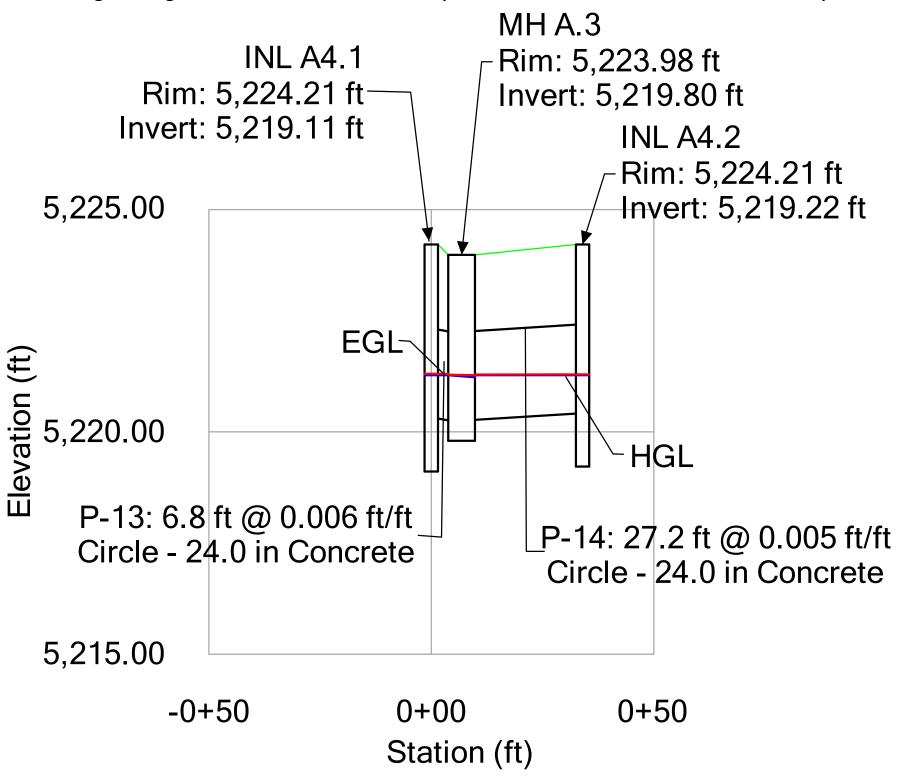
Profile Report

Engineering Profile - 5 - INL A3.2-INL A3.1 (Reunion Center StormCAD Model ACJ.stsw)



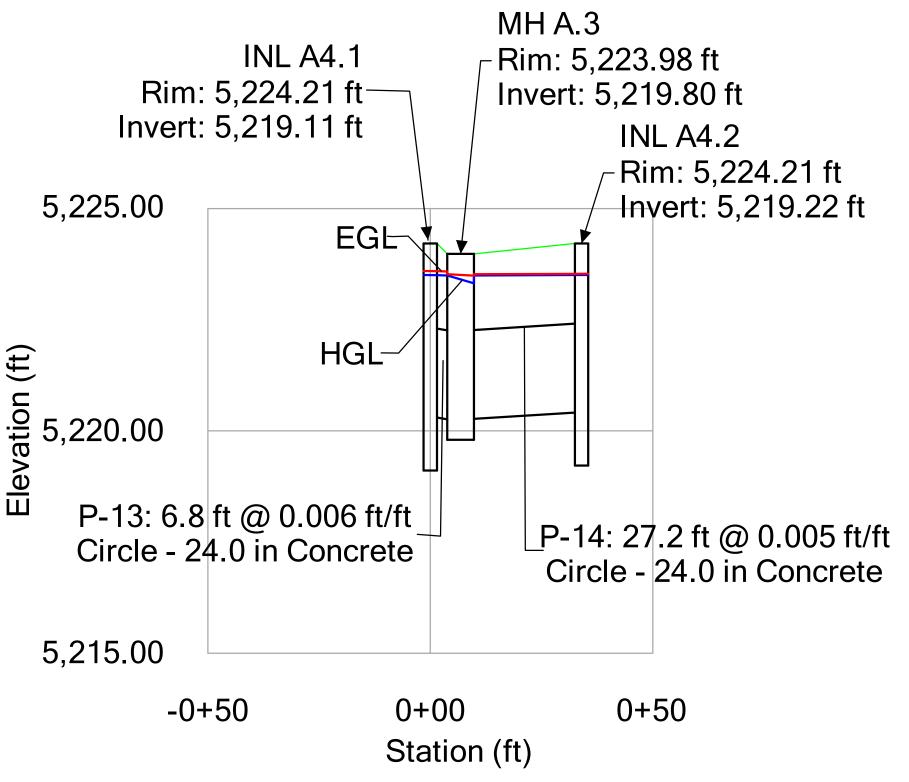
Profile Report

Engineering Profile - 6 - INL A4.1-INL A4.2 (Reunion Center StormCAD Model ACJ.stsw)

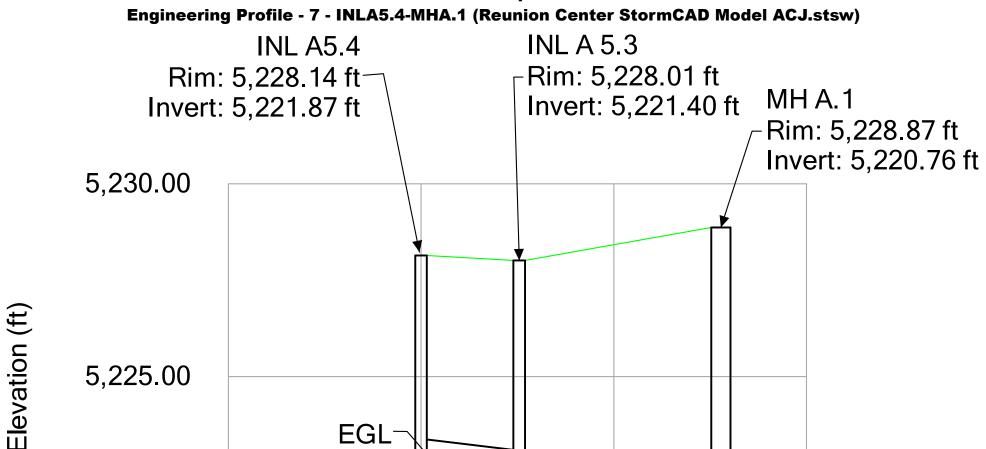


Profile Report

Engineering Profile - 6 - INL A4.1-INL A4.2 (Reunion Center StormCAD Model ACJ.stsw)



Profile Report



EGL-

0+00

P-86: 25.5 ft @ 0.011 ft/ft Circle - 18.0 in

5,220.00

-0+50



P-87: 52.3 ft @ 0.010 ft/ft Circle - 18.0 in

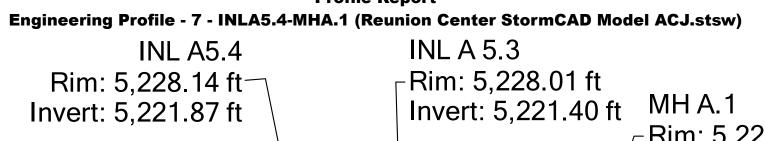
0+50

[10.03.04.53] Page 1 of 1

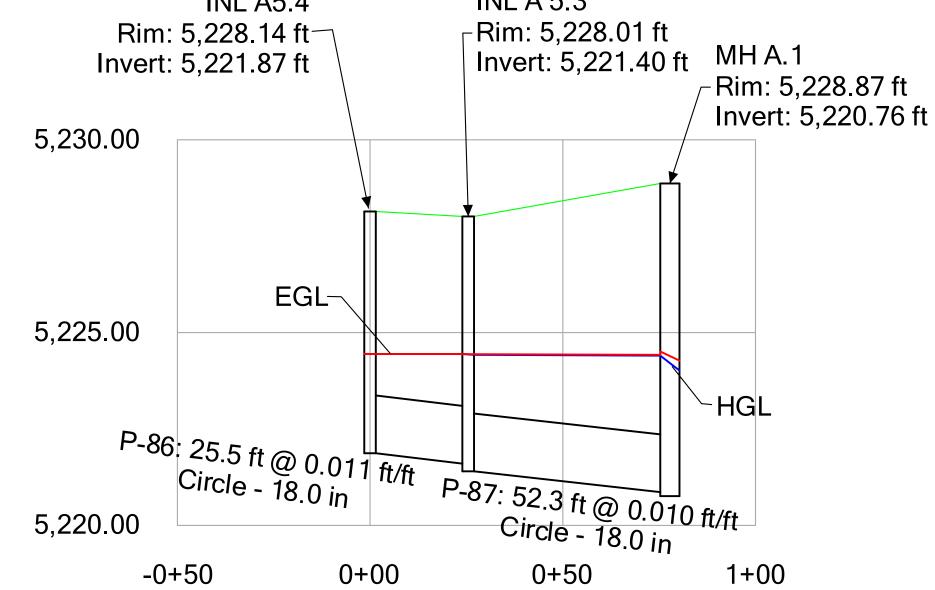
HGL

1+00

Profile Report



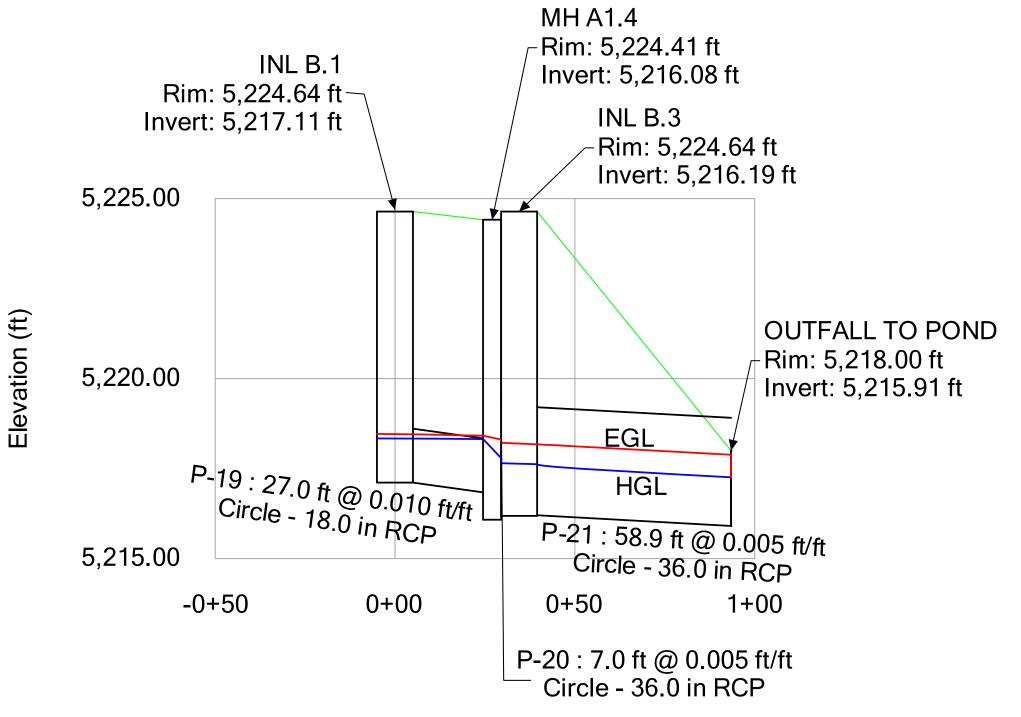




Station (ft)

Profile Report

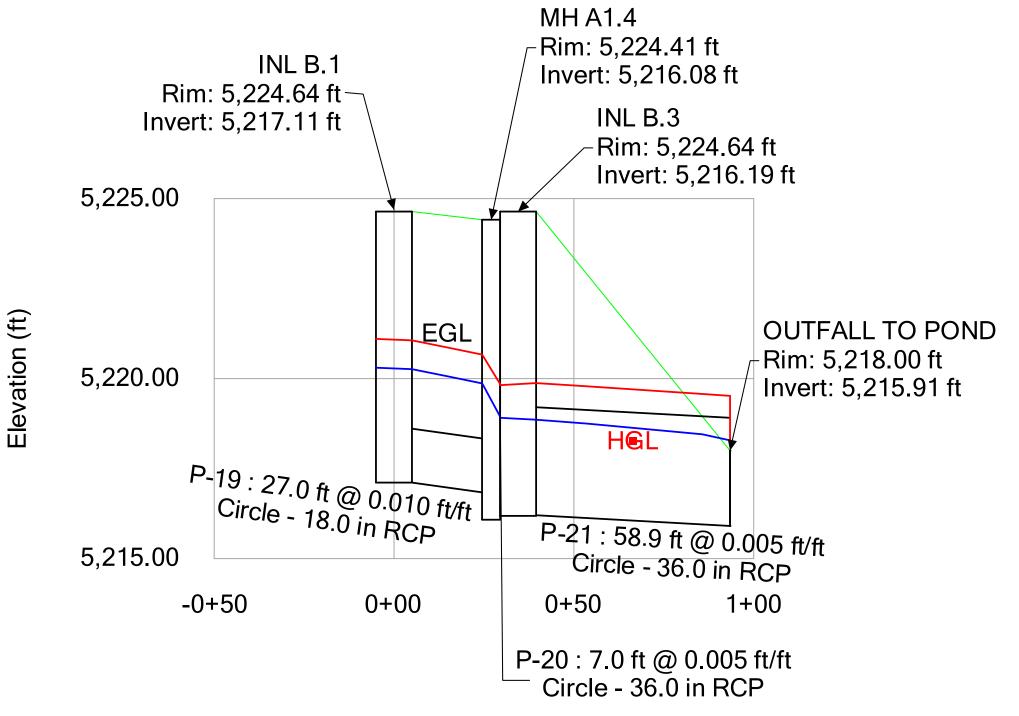




Station (ft)

Profile Report





Station (ft)

APPENDIX C REFERENCE EXCERPTS

AMENDMENT #2 TO PRELIMINARY DRAINAGE REPORT FOR REUNION CENTER - VILLAGE 1

November 6, 2023

Prepared For: **Reunion Metropolitan District**17910 East Parkside Drive North
Commerce City, Colorado 80022
Contact: Matt Urkoski

Prepared By: JR ENGINEERING, LLC 7200 S Alton Way, Suite C400 Centennial, Colorado 80112 (303) 740-9393 Contact: Aaron Clutter, PE

Project No. 14421.49

DRAINAGE REPORT FOR REUNION CENTER - VILLAGE 1, JR ENGINEERING, NOVEMBER 6, 2023

FROM: AMENDMENT #2 TO PRELIMINARY

JR ENGINEERING, N



NOAA Atlas 14, Volume 8, Version 2 Location name: Commerce City, Colorado, USA* Latitude: 39.8942°, Longitude: -104.7702° Elevation: 5209.73 ft**

source: ESRI Maps
** source: USGS

POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

PF tabular

PDS-	based po	int precip	itation fre	quency e	stimates v	vith 90% (confiden	ce interva	als (in inc	ches) ¹
Duration				Average	recurrence	interval (ye	ars)			
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	0.227 (0.178-0.290)	0.278 (0.218-0.355)	0.373 (0.292-0.478)	0.462 (0.359-0.594)	0.600 (0.458-0.817)	0.718 (0.533-0.985)	0.847 (0.607-1.19)	0.989 (0.680-1.42)	1.19 (0.789-1.76)	1.36 (0.871-2.02
10-min	0.333 (0.261-0.424)	0.407 (0.320-0.520)	0.546 (0.427-0.699)	0.676 (0.526-0.870)	0.878 (0.671-1.20)	1.05 (0.781-1.44)	1.24 (0.889-1.74)	1.45 (0.996-2.09)	1.75 (1.16-2.58)	1.99 (1.28-2.95)
15-min	0.406 (0.319-0.517)	0.497 (0.390-0.635)	0.666 (0.521-0.853)	0.825 (0.642-1.06)	1.07 (0.818-1.46)	1.28 (0.952-1.76)	1.51 (1.09-2.12)	1.77 (1.22-2.54)	2.13 (1.41-3.15)	2.43 (1.56-3.60)
30-min	0.562 (0.442-0.718)	0.685 (0.538-0.875	0.914 MINOR STOR	1.13 M 878-1.45)	1.46 (1.12-1.99)	1.75 (1.30-2.40 M	2.06 AJOR STOR	2.40 8M _{65-3.46)}	2.90 (1.92-4.28)	3.30 (2.12-4.90)
60-min	0.692 (0.544-0.884)	0.843 (0.661-1.08)	1.12 (0.878-1.44)	1.39 (1.08-1.78)	1.79 (1.37-2.44)	2.15 (1.59-2.94)	2.53 (1.81-3.55)	2.95 (2.03-4.25)	3.56 (2.36-5.26)	4.06 (2.60-6.02)
2-hr	0.823 (0.651-1.04)	1.00 (0.791-1.27)	1.33 (1.05-1.69)	1.64 (1.29-2.09)	2.13 (1.64-2.87)	2.54 (1.91-3.46)	3.00 (2.17-4.17)	3.50 (2.43-4.99)	4.22 (2.82-6.17)	4.82 (3.11-7.06)
3-hr	0.892 (0.710-1.12)	1.08 (0.860-1.36)	1.44 (1.14-1.81)	1.77 (1.39-2.24)	2.28 (1.77-3.07)	2.73 (2.05-3.69)	3.22 (2.34-4.44)	3.75 (2.62-5.31)	4.52 (3.04-6.57)	5.16 (3.35-7.51)
6-hr	1.06 (0.850-1.32)	1.27 (1.02-1.59)	1.66 (1.33-2.08)	2.03 (1.61-2.54)	2.59 (2.02-3.44)	3.08 (2.34-4.12)	3.61 (2.65-4.93)	4.19 (2.95-5.88)	5.04 (3.41-7.23)	5.72 (3.76-8.25)
12-hr	1.31 (1.06-1.62)	1.54 (1.25-1.91)	1.98 (1.59-2.45)	2.38 (1.90-2.96)	2.99 (2.35-3.92)	3.52 (2.69-4.64)	4.08 (3.02-5.51)	4.70 (3.34-6.50)	5.59 (3.82-7.92)	6.31 (4.18-8.99)
24-hr	1.57 (1.28-1.93)	1.87 (1.52-2.29)	2.38 (1.93-2.92)	2.83 (2.29-3.50)	3.51 (2.76-4.51)	4.06 (3.13-5.28)	4.65 (3.46-6.18)	5.28 (3.78-7.20)	6.17 (4.25-8.61)	6.87 (4.60-9.68)
2-day	1.81 (1.49-2.20)	2.18 (1.79-2.65)	2.79 (2.29-3.40)	3.32 (2.70-4.05)	4.06 (3.20-5.12)	4.64 (3.59-5.93)	5.24 (3.92-6.85)	5.86 (4.22-7.86)	6.71 (4.65-9.22)	7.36 (4.98-10.3)
3-day	1.98 (1.63-2.39)	2.35 (1.94-2.83)	2.97 (2.44-3.59)	3.50 (2.86-4.25)	4.25 (3.37-5.33)	4.84 (3.76-6.15)	5.45 (4.10-7.09)	6.09 (4.41-8.11)	6.96 (4.85-9.50)	7.63 (5.19-10.6)
4-day	2.11 (1.75-2.53)	2.47 (2.05-2.97)	3.09 (2.55-3.72)	3.62 (2.97-4.38)	4.37 (3.49-5.48)	4.98 (3.88-6.30)	5.60 (4.23-7.25)	6.25 (4.54-8.29)	7.14 (5.00-9.71)	7.84 (5.35-10.8)
7-day	2.40 (2.00-2.86)	2.78 (2.32-3.32)	3.43 (2.85-4.11)	3.99 (3.30-4.79)	4.78 (3.84-5.92)	5.40 (4.24-6.78)	6.04 (4.60-7.75)	6.71 (4.92-8.82)	7.62 (5.38-10.3)	8.33 (5.74-11.4)
10-day	2.65 (2.22-3.15)	3.06 (2.57-3.64)	3.75 (3.13-4.47)	4.33 (3.60-5.18)	5.15 (4.15-6.34)	5.79 (4.57-7.22)	6.45 (4.93-8.22)	7.13 (5.24-9.30)	8.04 (5.71-10.8)	8.75 (6.06-11.9)
20-day	3.39 (2.87-3.99)	3.87 (3.27-4.56)	4.65 (3.92-5.49)	5.30 (4.45-6.28)	6.20 (5.04-7.54)	6.90 (5.49-8.49)	7.60 (5.86-9.55)	8.31 (6.17-10.7)	9.25 (6.62-12.2)	9.97 (6.97-13.3)
30-day	3.99 (3.39-4.67)	4.54 (3.85-5.31)	5.42 (4.59-6.36)	6.15 (5.18-7.24)	7.14 (5.83-8.61)	7.90 (6.31-9.65)	8.65 (6.70-10.8)	9.41 (7.02-12.0)	10.4 (7.48-13.6)	11.1 (7.84-14.8)
45-day	4.71 (4.02-5.47)	5.36 (4.58-6.24)	6.42 (5.46-7.49)	7.27 (6.16-8.51)	8.42 (6.89-10.1)	9.28 (7.45-11.2)	10.1 (7.88-12.5)	11.0 (8.21-13.9)	12.0 (8.70-15.6)	12.8 (9.07-16.9)
60-day	5.29 (4.54-6.13)	6.06 (5.19-7.02)	7.28 (6.22-8.46)	8.27 (7.03-9.64)	9.57 (7.86-11.4)	10.5 (8.49-12.7)	11.5 (8.96-14.1)	12.4 (9.32-15.6)	13.6 (9.84-17.5)	14.4 (10.2-18.9)

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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EX & PROP CONDITIONS T-88 OUTFALL DRAINAGE MAP

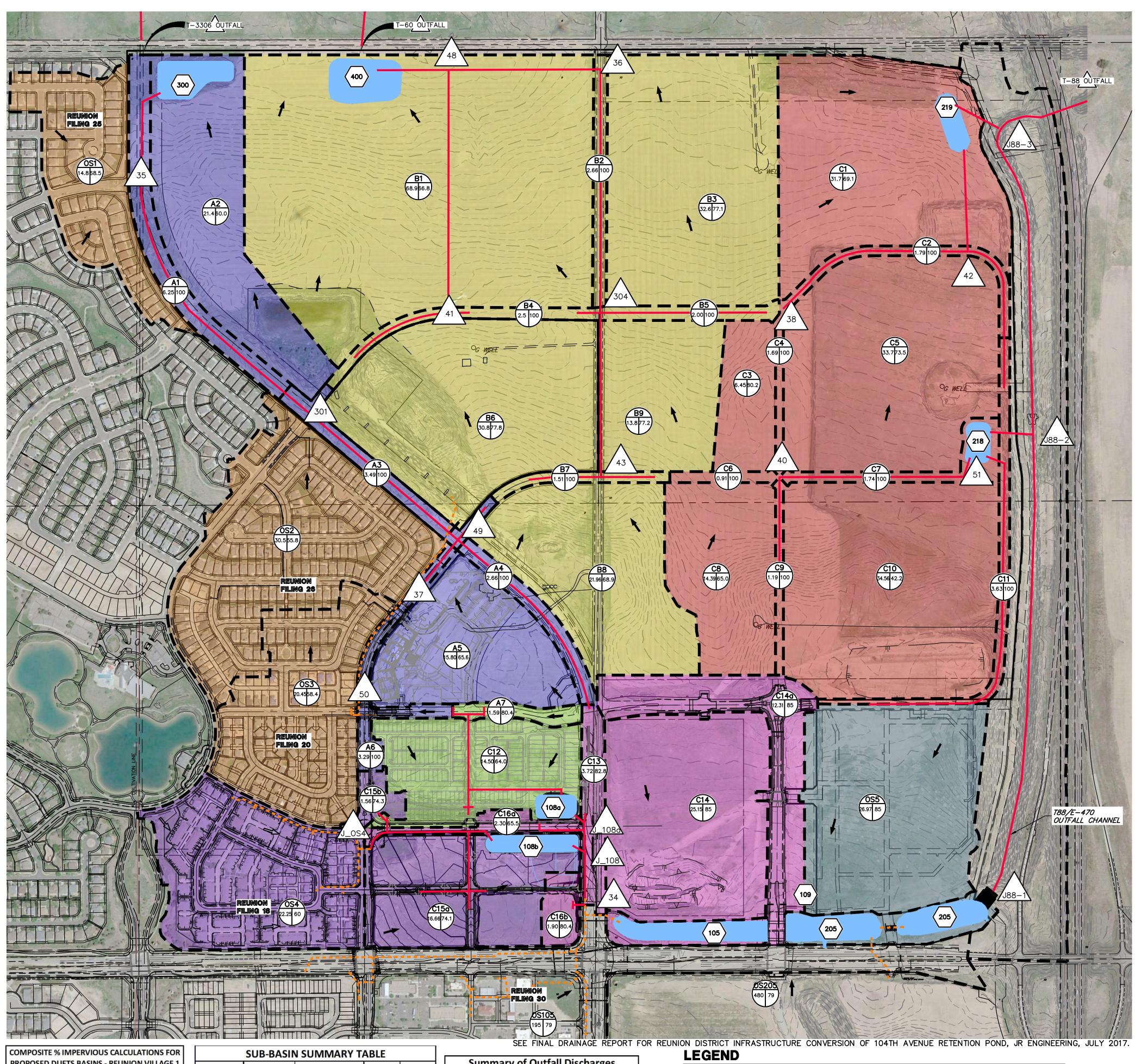
REUNION VILLAGE 1 PDR - AMENDMENT 2

112TH AVENUE

X:/1440000.all/1442149\Drawings\Sheet Dwgs\Drainage\Drain

REUNION VILLAGE 1

PRELIMINARY DRAINAGE REPORT - AMENDMENT #2 **OVERALL DRAINAGE PLAN**



	PUK AIVIE	NDMENT 2	
Overall Sub- Basin ID ¹	Duets Sub- Basin ID ²	Total Area (acres) ²	Basins Total Weighted % Imp.
	B1	0.67	79.1%
	B2	0.55	82.4%
A7	B5	0.15	81.3%
	B6	0.22	78.7%
	TOTAL	1.59	80.4%
	B3	0.31	65.0%
	B4	0.64	69.1%
C12	B8	12.44	67.2%
	108a	1.11	25.0%
	TOTAL	14.50	64.0%
	D1-F	0.51	60.6%
	D2-F	0.41	100.0%
121212	D3-F	0.30	96.6%
C13	D4-F	0.45	67.7%
	D8-F	1.17	82.5%
	D9-F	0.88	91.1%
	TOTAL	3.72	82.8%
	C7	1.40	72.5%
	C8	1.95	80.0%
	C9	0.98	80.0%
	C10	0.98	80.0%
	C11	1.27	80.0%
	C12	0.43	76.8%
	C13	0.43	76.2%
	C15	0.40	80.6%
C15a	C17	0.41	79.7%
	C18	2.63	80.0%
	C19	0.83	80.0%
	C24	1.37	80.0%
	C25	0.27	66.4%
	C26	0.45	80.5%
	C27	0.61	80.0%
	C28	0.78	80.0% 25.0%
	108b TOTAL	1.48	74.1%
	C1	16.66 0.37	87.3%
	C2	0.68	68.2%
C15b	C4	0.32	73.7%
CIDD	C5	0.19	71.5%
	TOTAL	1.56	74.3%
	D5	0.52	54.7%
	D6	0.47	74.8%
C16a	D7	1.31	66.5%
	TOTAL	2.30	65.5%
	D10	0.40	81.9%
C16b	D11	1.50	80.0%
0100	TOTAL	1.90	80.4%

Overall Sub-Basin ID's from the Reunion Village 1 PDR - Amendment #2	
Overall Drainage Plan Map	
Sub-Basin ID's and Areas from the proposed Reunion Center Duets	
Orainage Calcs	

J.	50 B B/ 1511	A 20 MINIAKT 17		
Sub-Basin	Total Area (ac)	Composite Percent Impervious	Q ₅ * (cfs)	Q ₁₀₀ * (cfs)
A1	6.25	100.0%	5.32	13.42
A2	21.40	60.0%	12.22	43.47
А3	3.49	100.0%	2.25	5.82
A4	2.66	100.0%	2.50	6.24
A5	15.80	65.6%	16.01	51.23
A6	3.29	100.0%	2.78	7.01
A7	1.59	80.4%	1.48	4.12
B1	68.90	66.8%	62.62	196.84
B2	2.66	100.0%	2.20	5.55
В3	32.60	77.1%	35.24	100.08
B4	2.50	100.0%	2.52	6.22
B5	2.00	100.0%	3.30	7.84
В6	30.83	77.8%	38.44	108.50
В7	1.51	100.0%	1.67	4.08
В8	21.96	68.9%	21.00	65.44
В9	13.85	77.2%	16.20	46.33
C1	31.70	69.1%	31.94	96.28
C2	1.79	100.0%	2.06	5.02
C3	6.45	80.2%	6.87	19.22
C4	1.69	100.0%	1.88	4.60
C5	33.70	73.5%	36.80	108.99
C6	0.91	100.0%	0.89	2.20
C7	1.74	100.0%	1.27	3.24
C8	14.39	65.0%	10.96	35.49
С9	1.19	100.0%	0.84	2.15
C10	34.56	42.2%	15.67	72.65
C11	3.63	100.0%	2.52	6.49
C12	14.50	64.0%	10.90	34.54
C13	3.71	82.8%	2.80	7.81
C14	25.15	85.0%	30.95	82.44
C14a	12.31	85.0%	12.67	33.95
C15a	16.66	74.1%	17.81	52.70
C15b	1.56	74.3%	1.25	3.74
C16a	2.30	65.5%	1.02	3.51
C16b	1.90	80.4%	2.71	7.46
OS1	14.80	68.5%	16.01	48.47
OS2	30.50	55.8%	21.80	76.35
OS3	20.45	58.4%	18.37	64.85
OS4	22.25	60.0%	14.81	52.02
OS5	26.97	85.0%	36.08	96.17

SEE FINAL DRAINAGE REPORT I								
Summary of Outfall Discharges								
and Pond Discharges								
Hydrograph Routing ¹								
Outfall	Q_5	Q ₁₀₀	Max Q ₁₀₀ 2					

Outfall	Q_5	Q ₁₀₀	Max Q ₁₀₀ 2
	(cfs)	(cfs)	(cfs)
T-3306	1.74	63.30	63.31
T-60	7.42	85.27	87.62
Junction 108	27.62	48.91	
Junction 34	28.67	51.47	75.26

From previously approved studies, max allowable

Pond Release Ra	ate 1		
Pond	Q ₅	Q ₁₀₀	Max Q ₁₀₀ ²
	(cfs)	(cfs)	(cfs)
Pond 105	184.40	266.78	537.70
Pond 108a	5.15	8.12	Pond 108 Ma
Pond 108b	19.48	32.92	Q ₁₀₀ = 52.14
Pond OS 109	19.24	90.78	111.13
Pond 205	407.07	506.76	478.35
Pond 218	0.82	27.61	30.00
Pond 219	14.16	17.15	17.50
Pond 300	1.74	63.30	63.31
Pond 400	7.42	85.27	87.62

² From previously approved studies, max allowable

Maximum Release Rates (cfs)				
Over-Detention*				
478.35				
30.0				
17.5				
(47.5)				

* Over-Detention required for the T-88 North Basin per the Final Drainage Report for Reunion District Infrastructure Conversion of 104th Avenue Retention Pond by JR Engineering, July 31, 2017. Over-Detention in Pond 220 (release rate of 47.5 cfs) has been prorated among the two proposed Ponds 218 and 219.

LEGEND		

REUNION AREAS TRIBUTARY TO T-3306 OUTFALL.

REUNION AREAS TRIBUTARY TO T60 OUTFALL.

REUNION AREAS TRIBUTARY TO T88 OUTFALL. REUNION DISTRICT AREAS: TRIBUTARY TO WQ POND 105 DIRECT DISCHARGE: WQ IN POND 105; EURV/100-YR IN POND 205

REUNION DISTRICT AREAS: TRIBUTARY TO WQ POND 105 PEAK ATTENUATION PROVIDED IN DETENTION POND 108a: WQ IN POND 105; EURV/100-YR IN POND

REUNION DISTRICT AREAS: TRIBUTARY TO WQ POND 105

PEAK ATTENUATION PROVIDED IN DETENTION POND 108b: WQ IN POND 105; EURV/100-YR IN POND 205 REUNION DISTRICT AREAS: TRIBUTARY TO T88 OUTFALL

ONSITE WQ; EURV/100-YR DETAINED ONSITE (WITH OVER-DETENTION)

OFFSITE AREAS: TRIBUTARY TO T88 OUTFALL ROUTED THROUGH POND 105 AND/OR 205. SEE FINAL DRAINAGE REPORT REUNION DISTRICT INFRASTRUCTURE CONVERSION OF 104TH AVENUE RETENTION POND, JR ENGINEERING, JULY 2017.

REGIONAL WQ/EURV/100-YR

REUNION DISTRICT AREAS: TRIBUTARY TO T-3306 OUTFALL

REUNION DISTRICT AREAS (EXISTING FILINGS): TRIBUTARY TO T-3306 OUTFALL REGIONAL WQ/EURV/100-YR

REUNION DISTRICT AREAS: TRIBUTARY TO T60 OUTFALL SUB-REGIONAL WQ/EURV/100-YR

WQ POND / DETENTION POND / OVER-DETENTION POND DRAINAGE BASIN DESIGN POINT

DRAINAGE BASIN PROPOSED/FUTURE STORM SEWER EXISTING STORM SEWER DRAINAGE ARROW

150

THIS PROPOSED DRAINAGE/LAND USE MAP HAS BEEN PREPARED TO SUMMARIZE THE ASSUMED FULL BUILD-OUT CONDITIONS FOR THIS MASTER DRAINAGE REPORT AND SHOULD NOT BE CONSTRUED AS A PLANNING DOCUMENT. THE LAND USES SHOWN HEREIN ARE SUBJECT TO CHANGE.

NOTE:

THE FUTURE STORMWATER DETENTION FACILITIES IN THE T-88 BASIN SHALL BE HELD TO THE OVER-DETENTION RELEASE RATES ESTABLISHED IN THE FINAL DRAINAGE REPORT FOR REUNION DISTRICT INFRASTRUCTURE CONVERSION OF 104TH AVENUE RETENTION POND (JR ENGINEERING, JULY 2017) (Q_{100, PEAK}: 50% OF HISTORIC DISCHARGE).



ORIGINAL SCALE: 1" = 300'

600

OVERALL DRAINAGE MAP **REUNION VILLAGE 1** PRELIMINARY DRAINAGE REPORT AMENDMENT #2 JOB NO. 14421.49 11/3/2023 SHEET 1 OF 1



J·R ENGINEERING A Westrian Company

Centennial 303-740-9393 • Colorado Springs 719-593-2593 Fort Collins 970-491-9888 • www.jrengineering.com

FROM: AMENDMENT #2 TO PRELIMINARY DRAINAGE REPORT FOR REUNION **CENTER - VILLAGE 1,** JR ENGINEERING, NOVEMBER 6, 2023

Subdivision: Reunion

Reunion Village 1 PDR - Amendment 2 Project Name:

Project No.: 14421.49 Calculated By: AHC Date: 11/1/2023

> The WQCV is relatively constant across the metropolitan Denver area, and is set at 0.60 inches. For SWMM Routing, assume the WQCV total precipitation depth occurs over a period of one hour per UDFCD Vol 3. $WQCV = (0.911^3 - 1.191^2 + 0.78)$

Water Quality Capture Volume Calculation - Pond 105

	Docin	Acrongo	Dorcont	WQCV	WQCV	
	Basin	Acreage	Percent			
		(ac)	Impervious	(in)	(ac-ft)	
	1	22.93	75.0%	0.300	0.572	
	2	24.26	54.5%	0.219	0.443	
	3a	21.55	60.6%	0.238	0.428	
	4a	22.80	73.8%	0.293	0.557	
ea	4b	16.52	65.7%	0.257	0.354	
Ā	4c	17.93	66.2%	0.259	0.387	
tan)	4d	7.97	65.9%	0.258	0.171	
pnl	5a	25.15	2.0%	0.015	0.032	
Έ	5c	12.31	96.0%	0.457	0.469	
Pond 105 Tributary Area	A1	3.76	100.0%	0.500	0.157	
Pu	A2	5.91	100.0%	0.500	0.246	
Pol	B1	4.50	100.0%	0.500	0.188	
	B2	4.05	100.0%	0.500	0.169	
	В3	6.67	100.0%	0.500	0.278	
	105	3.12	100.0%	0.500	0.130	
	TOTAL	199.43	64.50%	0.276	4.580	Total WQCV in Pond 105 (ac-ft) based on Amend
Pond 105 Origin	al Design	195.67	79.36%	0.324	5.289	From Final Drainage Report for Reunion District of 104th Avenue Retention Pond; July 31 2017

Total WQCV in Pond 105 (ac-ft) based on Amendment 2 land use and drainage patterns. From Final Drainage Report for Reunion District Infrastructure - Conversion

Legend:

Direct Discharge: WQCV in Pond 105

Onsite Detention for Peak Attenuation Only: WQCV provided in Pond 105

Pond 105 As-Built WQCV: 5.92 ac-ft Remaining WQCV: 1.340 ac-ft Based on the Spillway Elev from Approved Pond 105 Pond Certification Letter; December 6, 2018. Field Surveyed June 19, 2018

AS-BUILT POND 105 VOLUME CALCULATIONS

Project Name: Reunion Village 1 PDR - Amendment 2 Subdivision: Reunion

Project No.: 14421.49 Location: Commerce City

By: AHC

Volume=1/3 x Depth x (A+B+(A*B)^0.5)

A - Upper Surface

Checked By:

B - Lower Surface

Date: 11/1/23

As-Built Pond 105 - Volume Check

Stage	Stage Elevation	Stage Surface Area (square feet)	Stage Volume (cubic feet)	Cumulative Volume (cubic feet)	Cumulative Volume (acre feet)
		(square reet)	(cubic reet)	(cubic reet)	(acre reet)
0.00	5205.10	187	0	0	0.00
0.90	5206.00	2,790	1,110	1,110	0.03
1.90	5207.00	10,101	6,067	7,177	0.16
2.90	5208.00	21,002	15,223	22,400	0.51
3.90	5209.00	33,725	27,114	49,514	1.14
4.90	5210.00	43,172	38,351	87,865	2.02
5.90	5211.00	52,978	47,991	135,856	3.12
6.90	5212.00	62,903	57,870	193,726	4.45
7.65	5212.75	110,443	64,174	257,900	5.92

As-Built Spillway Elevation = 5212.75

	Volume (acre feet)	Water Surface Elevation	Stage (ft)	
Original Design Water Quality	5.289	5212.43	7.33	(from Final Drainage Report for Reunion District Infrastructure - Conversion of 104th Avenue Retention Pond; July 31
As-Built Water Quality	5.92	5212.76	7.66	(based on the Spillway Elev from Approved Pond 105 Pond Certification Letter; December 6, 2018. Field Surveyed Jun
Amendment 2 Design Water Quality	4.58	5212.07	6.97	(based on the Amendment 2 drainage basin updates contributing flows to WQ Pond 105. Amend. 2 Design WQCV = 4.



KEY CONTACTS

OWNER
REUNION METROPOLITAN DISTRICT
17910 E. PARKSIDE DRIVE NORTH
COMMERCE CITY, CO 80022 ATTN: DENISE DENSLOW 303-288-5431 CITY CITY OF COMMERCE CITY, ENGINEERING 8602 ROSEMARY STREET COMMERCE CITY, CO 80022-5053 ATTN: MARIA D'ANDREA, PE 303-289-8156 TRENGINEERING
7200 SOUTH ALTON WAY, SUITE C400
CENTENNIAL, CO 80112
ATTN: AARON CLUTTER, PE 303-740-9393 ELECTRIC UTILITY
UNITED POWER, INC.
500 COOPERATIVE WAY
BRIGHTON, CO 80603
ATTN: RANDY REESE 303-659-0551 GAS UTILITIES XCEL ENERGY GAS DISTRIBUTION 1123 WEST 3RD AVENUE DENVER, CO 80223 ATTN: TAMMY WRAY

SANITARY SEWER & WATER AUTHORITIES

SOUTH ADAMS COUNTY WATER & SANITATION DISTRICT 10200 E 102ND. AVENUE HENDERSON, CO 80640 ATTN: ABEL MORENO 720-206-0590

TELECOMMUNICATION UTILITIES

CENTURY LINK 5325 ZUNI STREET, #728 DENVER, CO 80221 ATTN: MARK IVERSON

303-458-2048

303-425-3994

8490 NORTH UMATILLA STREET FEDERAL HEIGHTS, CO 80260 ATTN: GLEN NELSON

303-603-6745

FIRE DISTRICT
SOUTH ADAMS FIRE PROTECTION DISTRICT 6550 EAST 72ND AVENUE COMMERCE CITY, CO 80022-2006 ATTN: KEVIN VINCEL

303-288-4179

GEOTECHNICAL ENGINEER
CTL THOMPSON MATERIALS ENGINEERS INC.
22 LIPAN STREET
DENVER, CO 80223

ATTN: ZACHORIAH BALLARD 303-825-0777

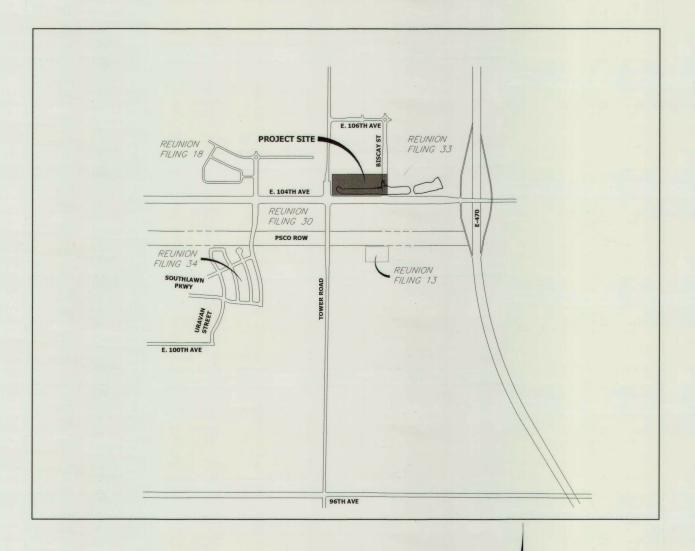
BENCHMARK & HORIZONTAL DATUM

PROJECT COORDINATES ARE MODIFIED COLORADO STATE PLANE, NORTH ZONE NAD83 (2011) COORDINATES. THE COMBINED ELEVATION/SCALE FACTOR USED TO MODIFY THE COORDINATES FROM STATE PLANE TO THE PROJECT COORDINATES IS 1.000273080. THE RESULTING PROJECT COORDINATES ARE TRUNCATED BY 1,000,000 IN THE NORTHING AND 3,000,000 IN THE EASTING. PROJECT COORDINATE NORTHING US SURVEY FEET = (STATE PLANE NORTHING * 1.000273080) * (3937/1200) - 1,000,000)
PROJECT COORDINATE EASTING US SURVEY FEET = (STATE PLANE EASTING * 1.000273080) * (3937/1200) - 3,000,000)
PROJECT COORDINATE EASTING US SURVEY FEET = (STATE PLANE EASTING * 1.000273080) * (3937/1200) - 3,000,000)
PROJECT ELEVATIONS ARE BASED ON NGS MONUMENT DVXJ WITH A NAVD88 ELEVATION OF 5425.25 FT.

E. 104TH AVENUE WATER QUALITY POND

E-470 & E. 104TH AVENUE REGIONAL DETENTION POND CITY OF COMMERCE CITY, COUNTY OF ADAMS, STATE OF COLORADO **PUBLIC IMPROVEMENT CONSTRUCTION PLANS**

REUNION METROPOLITAN DISTRICT



PROJECT LOCATION MAP



FROM: AMENDMENT #2 TO PRELIMINARY DRAINAGE REPORT FOR REUNION CENTER - VILLAGE 1, JR ENGINEERING, NOVEMBER 6, 2023

SHEET INDEX

COVER SHEET
GENERAL NOTES
LEGEND
OVERALL EARTHWORK PLAN
DEMOLITION PLAN
WAITER QUALITY POND PLAN (AB)
POND SECTIONS
STORM SEWER PLAN AND PROFILE (AB)
OUTLET STRUCTURE DETAILS (AB)
FOREBAY AND IMPACT BASIN DETAILS (AB)
GESC PLANS



(AB) - INDICATES AS BUILT CONDITION AS CONSTRUCTED 11/2018

CERTIFICATION STATEMENT

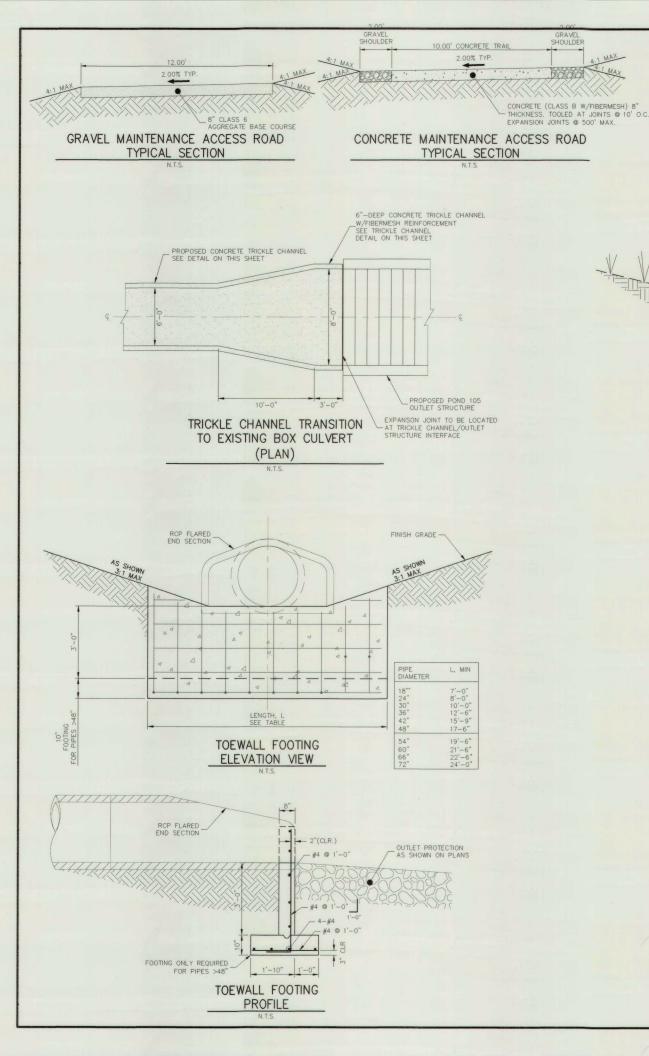
I HEREBY CERTIFY THAT THE PUBLIC IMPROVEMENTS FOR E. 104TH AVENUE WATER QUALITY POND HAVE BEEN CONSTRUCTED IN SUBSTANTIAL COMPLIANCE WITH THE CONSTRUCTION PLANS APPROVED BY THE CITY OF COMMERCE



COVER SHEET E. 104TH AVENUE WATER QUALITY POND JOB NO. 14421.32 SHEET 1 OF 33



7200 S. Alton Way, Suite C100, • Centennial, CO 80112 303-740-9393 • Fax: 303-721-9019 • www.jrengineering.com



POND GRADING NOTES:

FIBER MESH REINFORCEMENT. PROVIDE TOOLED JOINTS @ 10' O.C. WITH DOWELS. EXPANSION JOINTS AT STRUCTURE/TRICKLE CHANNEL INTERFACES.

WELDED WIRE MESH (6×6-W2.9×W2.9)

4' CONCRETE TRICKLE CHANNEL

APPROVED FILL MATERIAL MUCK REMOVED

6' CONCRETE TRICKLE CHANNEL

TYPICAL SECTION

TYPICAL SECTION

TYPE M RIPRAP (d₅₀=12"), 24" DEPTH

- STABILIZED COMPACTED SUBGRADE

3.00% 1 WELDED WIRE MESH (6×6-W2.9×W2.9)

(AB) - INDICATES AS BUILT CONDITION

AS CONSTRUCTED

11/2018

SLOPE AS SHOWN ON PLANS 4:1 H: V MAXIMUM 3.00% TYPICAL

FIBER MESH REINFORCEMENT.
PROVIDE TOOLED JOINTS @ 10' O.C. WITH
DOWELS. EXPANSION JOINTS AT
STRUCTURE/TRICKLE CHANNEL INTERFACES.

TYPE M RIPRAP (d₅₀=12"), 24" DEPTH

- STABILIZED SUBGRADE MATERIAL

SLOPE AS SHOWN ON PLANS 4:1 H: V MAXIMUM 3.00% TYPICAL

- THE EXISTING E. 104TH AVENUE RETENTION POND IS AN ACTIVE REGIONAL DRAINAGE FACILITY WITH STORMWATER RUNOFF FROM ADJACENT DEVELOPMENT ENTERING THE
- POND.

 2. CONTRACTOR SHALL ANTICIPATE STORMWATER INFLOWS TO THE EXISTING POND DURING CONSTRUCTION AND PROVIDE A MEANS OF CONVEYANCE/REMOVAL OF ANY CONTINUOUS INFLOWS TO THE POND.

 3. DEWATERING.

 3. O. THE EXISTING RETENTION POND IS CURRENTLY IMPOUNDING WATER. DEWATERING OF THE EXISTING RETENTION POND SHALL OCCUR IN ADVANCE OF CONSTRUCTION ACTIVITIES.

- . THE EXISTING RETENTION POND IS CURRENTLY IMPOUNDING WATER. DEWATERING OF THE EXISTING RETENTION POND SHALL OCCUR IN ADVANCE OF CONSTRUCTION ACTIVITES.

 CONTRACTOR TO PHASE T88 OUTFALL CONSTRUCTION IN A MANNER TO FACILITATE CONSTRUCTION DEWATERING AND PROVIDE A MEANS OF REMOVAL OF CURRENTLY IMPOUNDED WATER. THE ESTIMATED QUANTITY OF DEWATERING FROM THE EXISTING RETENTION POND IS 30 ACRE-FEET.

 THE CONTRACTOR SHALL OBTAIN A CONSTRUCTION DEWATERING (CDW) PERMIT FROM CDPHE ANYTIME GROUNDWATER, INCLUDING GROUNDWATER THAT IS COMMINGLED WITH STORMWATER OR SURFACE WATER, IS ENCOUNTERED DURING CONSTRUCTION ACTIVITIES AND THE GROUNDWATER OR COMMINGLED WATER NEEDS TO BE DISCHARGED TO SURFACE WATER.

 WATER FROM DEWATERING OPERATIONS SHALL NOT BE DIRECTLY DISCHARGED INTO ANY STATE WATERS, UNLESS ALLOWED BY A PERMIT.

 THE SWMP DESCRIBES AND LOCATES THE PRACTICES TO BE USED THAT WILL ENSURE THAT NO GROUNDWATER FROM CONSTRUCTION DEWATERING IS DISCHARGED FROM THE PROJECT BOUNDARY AS SURFACE WHOFF OR TO SURFACE WATERS OR STORM SEWERS.

 GROUNDWATER IS NOT ANTICIPATED WITH THIS PROJECT. HOWEVER, THE CONTRACTOR SHALL BE PREPARED TO PROVIDE CONSTRUCTION DEWATERING FOR GROUNDWATER.

- CONTRACTOR SHALL BE PREPARED TO PROVIDE CONSTRUCTION DEWATERING FOR GROUNDWATER.

 4. MUCK EXCAVATION.

 4.0. THE EXISTING POND BOTTOM IS ASSUMED TO BE UNSUITABLE MATERIAL. CONTRACTOR SHALL REMOVE ORGANIC MUCK MATERIAL FROM THE EXISTING POND BOTTOM TO THE DEPTH AS DETERMINED BY THE ENGINEER AND REPLACE THE EXCAVATED VOLUME WITH SUITABLE APPROVED FILL MATERIAL PRIOR TO CONSTRUCTION OF THE PROPOSED POND STRUCTURAL IMPROVEMENTS.

 4.b. MUCK EXCAVATION PAY ITEM SHALL CONSIST OF THE REMOVAL AND DISPOSAL OF MIXTURES OF SOILS AND ORGANIC MATERIAL NOT SUITABLE FOR FOUNDATION OR EMBANKMENT MATERIAL.

 5. FILL MATERIAL SHALL BE APPROVED BY THE GEOTECHNICAL ENGINEER. ALL UNSUITABLE MATERIAL SHALL BE DISPOSED OF AS DIRECTED.

 6. THE MAXIMUM SLOPE FOR EXCAVATION AND PLACEMENT OF FILL IS 4:1 HORIZONTAL VERTICAL UNLESS OTHERWISE SHOWN IN THE PLANS.

 7. ALL EMBANKMENT FILL MATERIAL SHALL BE MOISTURE CONDITIONED PRIOR TO COMPACTION, FILL MATERIAL SHALL BE MOISTURE CONDITIONED PRIOR TO COMPACTION, FILL MATERIAL SHALL BE MOISTURE CONDITIONED TO WITHIN THE FOLLOWING OF OPTIMUM:

 7.0. BENEATH STRUCTURAL AREAS:

 1 TO +3% (COHESIVE);

 7.b. BENEATH NON—STRUCTURAL AREAS:

 3 TO 1-3% (NON—COHESIVE)

 8. THE FILL SHALL BE PLACED IN THIN, LOOSE LIFTS OF 8 INCHES OR LESS. FILL IS TO BE

- THE FILL SHALL BE PLACED IN THIN, LOOSE LIFTS OF 8 INCHES OR LESS. FILL IS TO BE COMPACTED TO A MINIMUM OF:
 8.0. BENEATH STRUCTURAL AREAS: 95 PERCENT OF MAXIMUM DRY DENSITY AND PER ASTM D 698 (COHESIVE SOILS) OR ASTM D 1557 (GRANULAR SOILS).

 AND PER ASTM D 698 (COHESIVE SOILS) OR ASTM D 1557 (GRANULAR SOILS).

 A COLORADO DEPARTMENT OF PUBLIC HEALTH AND ENVIRONMENT (COPHE) WATER OUALITY DIVISION STORMWATER DISCHARGE PERMIT SHALL BE OBTAINED AND A COPY SHALL BE SUBMITTED TO THE CITY OF COMMERCE CITY DEPARTMENT OF PUBLIC WORKS.

FIBER MESH NOTES:

FIBROUS CONCRETE REINFORCEMENT SHALL CONSIST OF:
100% VIRGIN POLYPROPYLENE FIBRILLATED FIBERS SPECIFICALLY
MANUFACTURED FOR USE AS CONCRETE REINFORCEMENT,
CONTAINING NO REPROCESSED OLEFIN MATERIALS. FIBROUS
CONCRETE REINFORCEMENT SHALL BE AS MANUFACTURED BY
FIBERMESH COMPANY, BUCKEYE ULTRA FIBER 500, OR APPROVED
FOLIAL

EXPANSION JOINT NOTES:

EXPANSION JOINTS SHALL BE LOCATED AT ABUTTING JUNCTIONS OF CONCRETE APRONS, CONCRETE TRICKLE CHANNELS @ 400' O.C., OUTLET STRUCTURES, GROUTED BOULDER STRUCTURES, ETC. EXPANSION JOINTS SHALL BE FILLED WITH ½ INCH THICK FULL DEPTH, PREFORMED EXPANSION JOINT FILLER. THE MEMBRANE SHALL BE FLASHED UP TO THE TOP OF THE JOINT AND SECURED WITH PRIMER.

EXPANSION JOINTS IN THE COMPLETED WORK SHALL BE LEFT CAREFULLY TOOLED AND FREE OF ALL MORTAR AND CONCRETE. THE JOINT FILLER SHALL BE LEFT EXPOSED FOR ITS FULL LENGTH WITH CLEAN AND TRUE EDGES.

BENCHMARK & HORIZONTAL DATUM

PROJECT COORDINATES ARE MODIFIED COLORADO STATE PLANE, NORTH ZONE NAD83 (2011) COORDINATES. THE COMBINED ELEVATION/SCALE FACTOR USED TO MODIFY THE COORDINATES FROM STATE PLANE TO THE PROJECT COORDINATES IS 1,000273080. THE RESULTING PROJECT COORDINATES ARE TRUNCATED BY 1,000,000 IN THE NORTHING AND 3,000,000 IN THE EASTING. PROJECT COORDINATE NORTHING US SURVEY FEET = (STATE PLANE NORTHING * 1.000273080) * (3937/1200) - 1,000,000)
PROJECT COORDINATE EASTING US SURVEY FEET = (STATE PLANE EASTING * 1.000273080) * (3937/1200) - 3,000,000)
PROJECT COORDINATE EASTING US SURVEY FEET = (STATE PLANE EASTING * 1.000273080) * (3937/1200) - 3,000,000)
PROJECT ELEVATIONS ARE BASED ON NGS MONUMENT DVXJ WITH A NAVD88 ELEVATION OF 5425.25 FT.

Know what's below. Call before you dig.

INFORMATION ONLY

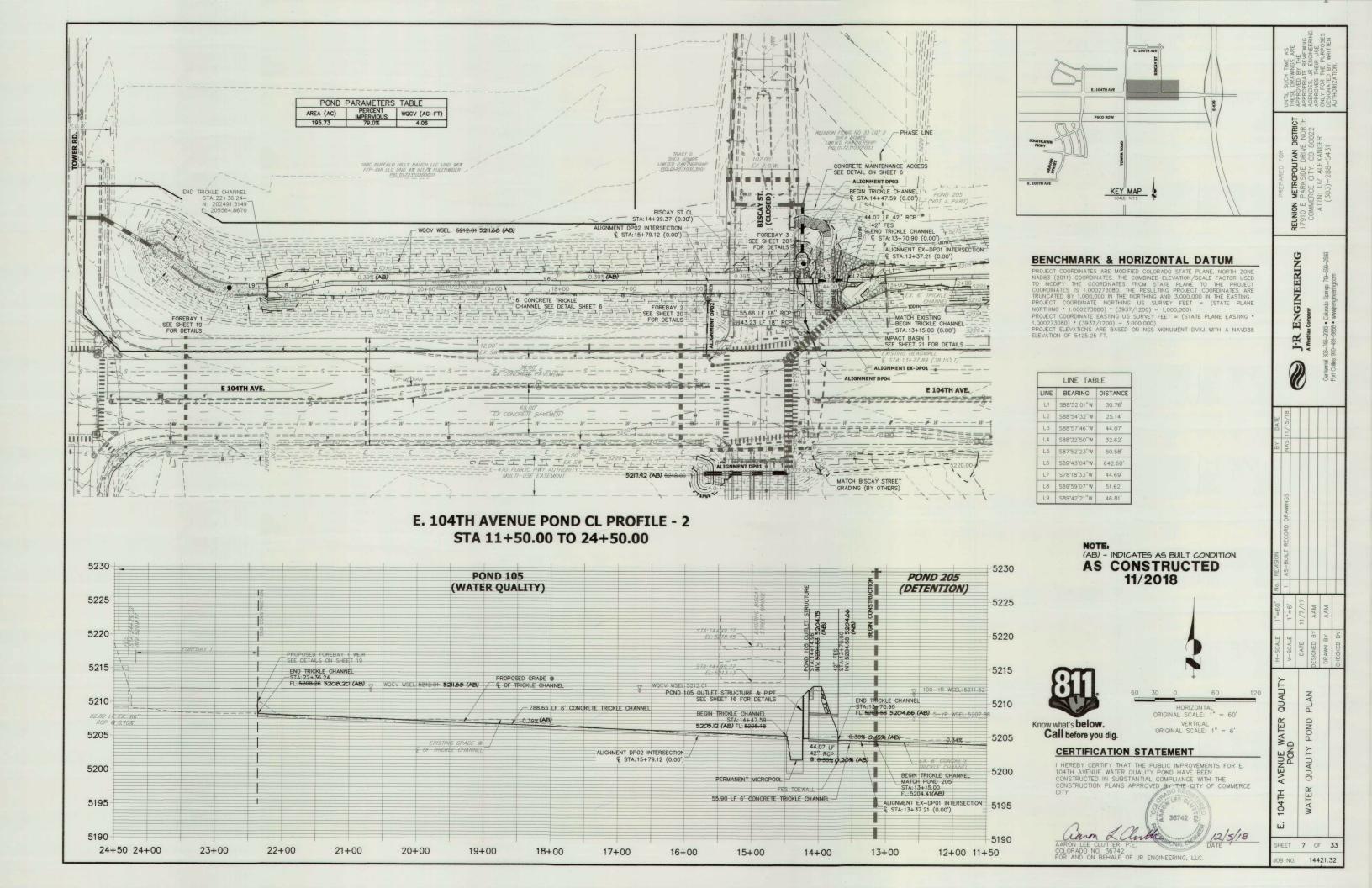
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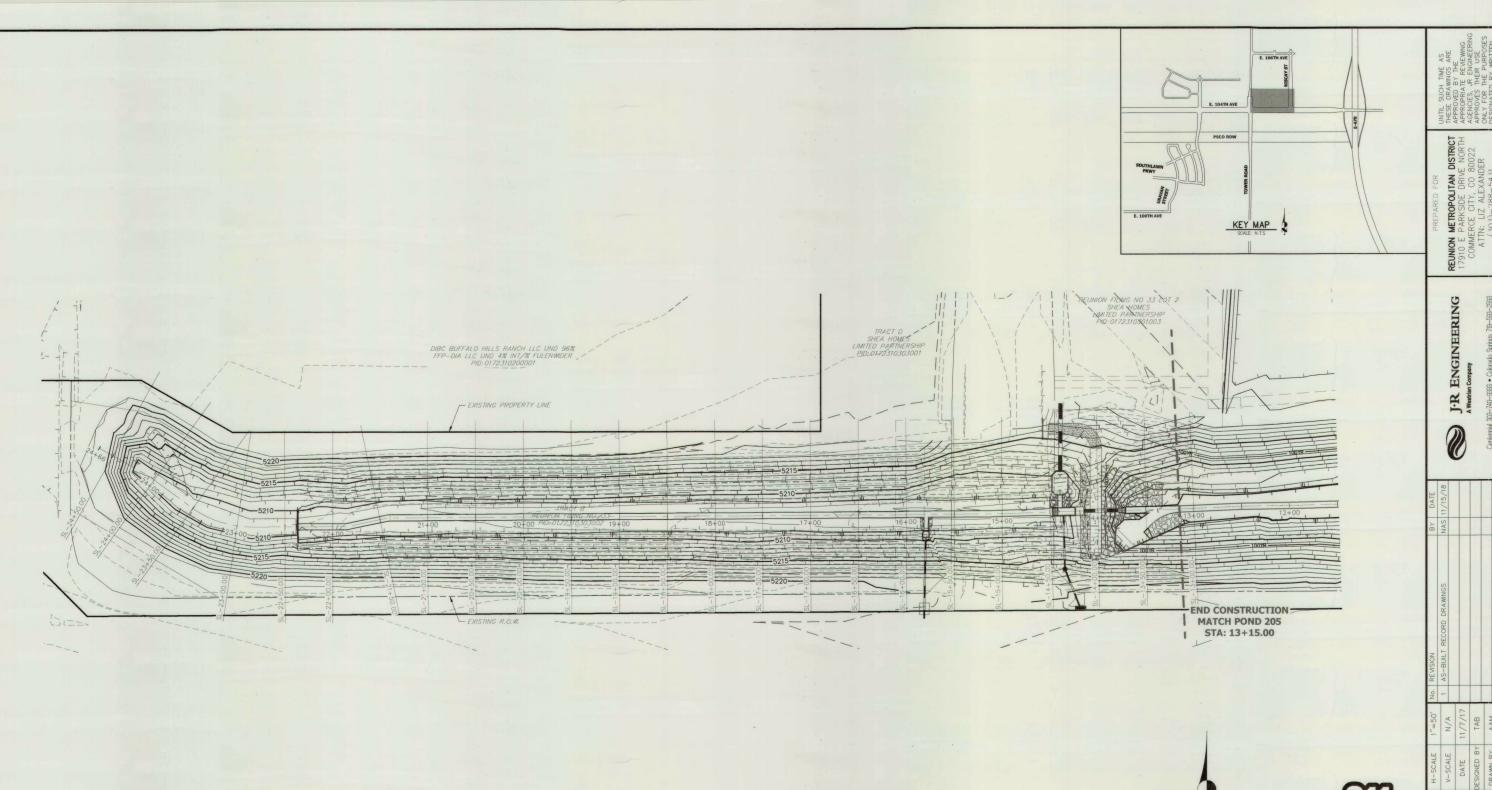
DRIVE NORTH
CO 80022
XANDER
-5431 TROPOLITAN ME

ENGINEERING



QUALI PLAN AVENUE WATER (POND QUALITY WATER 104TH نیا SHEET 6 OF 33







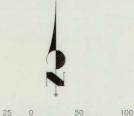
- EXISTING INTERMEDIATE CONTOUR - EXISTING INDEX CONTOUR

AS-BUILT INTERMEDIATE CONTOUR - AS-BUILT INDEX CONTOUR

NOTE.
(AB) - INDICATES AS BUILT CONDITION
AS CONSTRUCTED
11/2018

NOTES:

1. SEE SHEETS 9 & 10 FOR POND SECTIONS



ORIGINAL SCALE: 1" = 50'



Know what's **below**.

Call before you dig.

CERTIFICATION STATEMENT

HEREBY CERTIFY THAT THE PUBLIC IMPROVEMENTS FOR E.

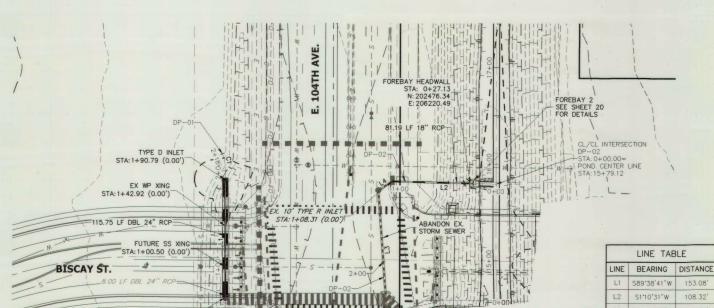
104TH AVENUE WATER QUALITY POND HAVE BEEN
CONSTRUCTED IN SUBSTANTIAL COMPLIANCE WITH THE
CONSTRUCTION PLANS APPROVED BY THE CITY OF COMMERCE
CITY.

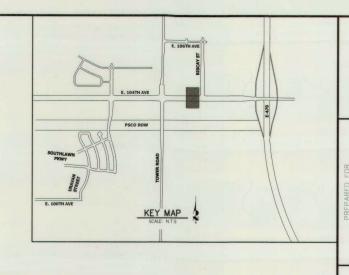


SHEET 8 OF 33

14421.32

AVENUE WATER QUALITY POND





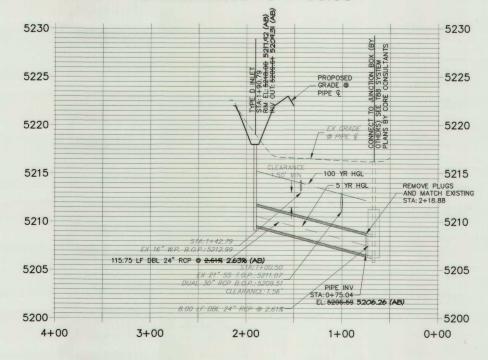
	CURVE	TABLE	
CURVE	DELTA	RADIUS	LENGTH
C1	17*56'01"	47.52'	14.87'

L3 N85'31'33"E 124.35' L4 S32*27'01"E 17.33'

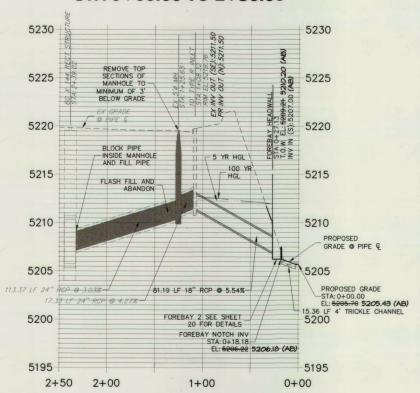
DP-01 PROFILE STA 0+00.00 TO 4+00.00

CONNECT TO JUNCTION BOX (BY OTHERS)
SEE T88 SYSTEM
PLANS BY CORE CONSULTANTS

STA: 0+68.50 (0.00')



DP-02 PROFILE STA 0+00.00 TO 2+50.00



STORM SEWER NOTES

- ALL STATIONING IS PIPE CENTERLINE UNLESS OTHERWISE NOTED.
 PIPE LENGTHS ARE FROM INSIDE INLET WALL TO INSIDE INLET WALL, FROM
 CENTER OF MANHOLE TO INSIDE INLET WALL, OR FROM CENTER OF
 MANHOLE TO CENTER OF MANHOLE. PIPE LENGTHS INCLUDE FES OR

- MANHOLE TO CENTER OF MANHOLE. PIPE LENGTHS INCLUDE FES OR HEADWALL.

 3. ALL ON-GRADE INLETS ARE TO MATCH TBC ELEVATIONS AT EACH END, FOLLOWING STREET GRADES.

 4. ALL PIPES SHALL BE CLASS III RCP UNLESS OTHERWISE NOTED.

 5. ALL MANHOLES SHALL BE 5' Ø UNLESS OTHERWISE NOTED.

 6. PIPE BEDDING SHALL CONFORM TO THE CITY OF COMMERCE CITY CONSTRUCTION STANDARDS AND SPECIFICATIONS, BEDDING FOR RCP PIPE SHALL BE AG7122 NO. 57/67 CRUSHED ROCK, SQUEEGEE OR MIXTURES CONTAINING SQUEEGEE SHALL NOT BE USED. BEDDING SHALL BE SIX TO EIGHT INCHES DEEP UNDER THE PIPE AND BACKFILLED TO THE SPRING LINE.

 7. INLET STATIONING IS TO CENTER OF INLET.

 8. PIPES SHALL HAVE JOINT RESTRAINTS ON LAST 3 JOINTS AT PIPE OUTFALL.

BENCHMARK & HORIZONTAL DATUM

PROJECT COORDINATES ARE MODIFIED COLORADO STATE PLANE, NORTH ZONE NAD83 (2011) COORDINATES. THE COMBINED ELEVATION/SCALE FACTOR USED TO MODIFY THE COORDINATES FROM STATE PLANE TO THE PROJECT COORDINATES IS 1.000273080. THE RESULTING PROJECT COORDINATES ARE TRUNCATED BY 1,000,000 IN THE NORTHING AND 3,000,000 IN THE EASTING. PROJECT COORDINATE NORTHING US SURVEY FEET = (STATE PLANE NORTHING * 1.000273080) * (3937/1200) - 1,000,000) PROJECT COORDINATE EASTING SURVEY FEET = (STATE PLANE EASTING * 1.000273080) * (3937/1200) - 3,000,000)

1.000273080) * (3937/1200) - 3,000,000) PROJECT ELEVATIONS ARE BASED ON NGS MONUMENT DVXJ WITH A NAVD88 ELEVATION OF 5425.25 FT.



(AB) - INDICATES AS BUILT CONDITION AS CONSTRUCTED 11/2018





CERTIFICATION STATEMENT

I HEREBY CERTIFY THAT THE PUBLIC IMPROVEMENTS FOR E. 104TH AVENUE WATER QUALITY POND HAVE BEEN
CONSTRUCTED IN SUBSTANTIAL COMPLIANCE WITH THE
CONSTRUCTION PLANS APPROVED BY THE CITY OF COMMERCE



SHEET 11 OF 33

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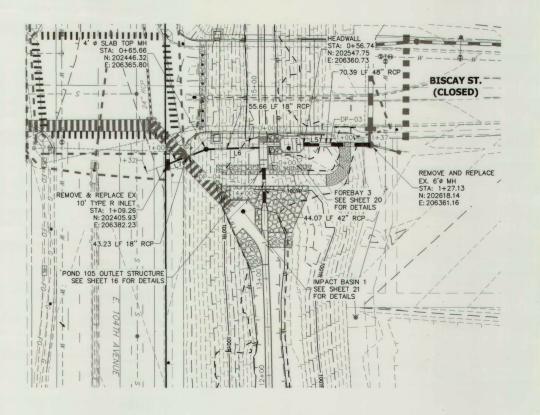
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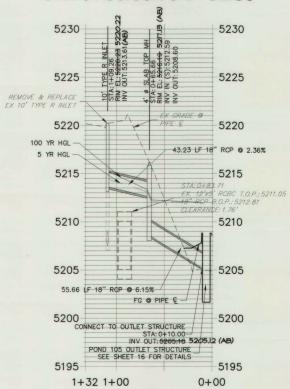
QUALITY AND AVENUE WATER POND PLAN

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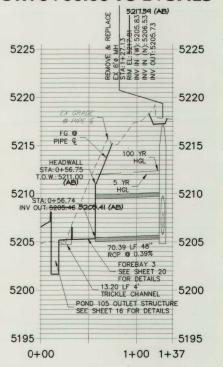


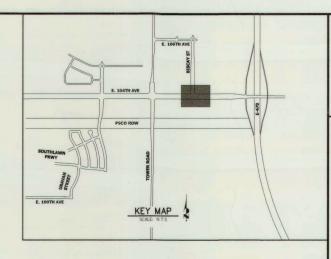
LINE TABLE						
LINE	BEARING	DISTANCE				
L5	N0*20'40"E	137.13'				
L6	S1*37'10"E	65.66'				
L7	S20*54'25"E	66.64				

DP-04 PROFILE STA 0+00.00 TO 1+32.30



DP-03 PROFILE STA 0+00.00 TO 1+37.13





STORM SEWER NOTES

- ALL STATIONING IS PIPE CENTERLINE UNLESS OTHERWISE NOTED.
 PIPE LENGTHS ARE FROM INSIDE INLET WALL, FROM CENTER OF MANHOLE TO INSIDE INLET WALL, OR FROM CENTER OF MANHOLE TO CENTER OF MANHOLE. PIPE LENGTHS INCLUDE FES OR

- MANHOLE TO CENTER OF MANHOLE. PIPE LÉNGTHS INCLUDE FES OR HEADWALL.

 3. ALL ON-GRADE INLETS ARE TO MATCH TBC ELEVATIONS AT EACH END, FOLLOWING STREET GRADES.

 4. ALL PIPES SHALL BE CLASS III RCP UNLESS OTHERWISE NOTED.

 5. ALL MANHOLES SHALL BE 5' Ø UNLESS OTHERWISE NOTED.

 6. PIPE BEDDING SHALL CONFORM TO THE CITY OF COMMERCE CITY CONSTRUCTION STANDARDS AND SPECIFICATIONS, BEDDING FOR RCP PIPE SHALL BE AG7122 NO. 57/67 CRUSHED ROCK. SQUEEGEE OR MIXTURES CONTAINING SQUEEGEE SHALL NOT BE USED. BEDDING SHALL BE SIX TO EIGHT INCHES DEEP UNDER THE PIPE AND BACKFILLED TO THE SPRING LINE.

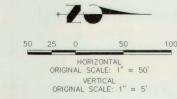
 7. INLET STATIONING IS TO CENTER OF INLET.

 8. PIPES SHALL HAVE JOINT RESTRAINTS ON LAST 3 JOINTS AT PIPE OUTFALL.

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(AB) - INDICATES AS BUILT CONDITION AS CONSTRUCTED 11/2018



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now what's below.

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COLORADO NO. 36742
FOR AND ON BEHALF OF JR ENGINEERING, LLC.

UNTIL THESE APPRO APPRO APPRO ONLY ONLY

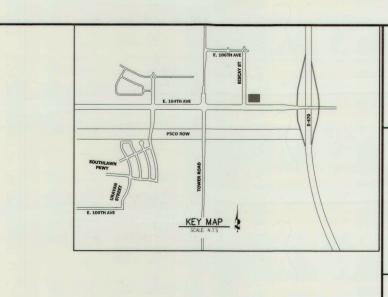
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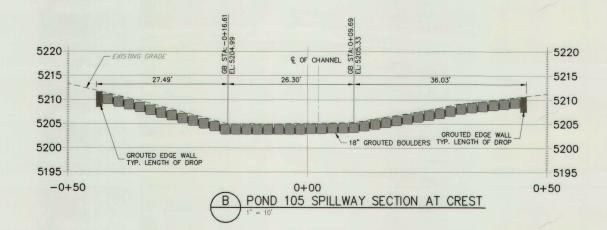
QUALITY PROFILE . WATER ND AND PLAN SEWER 104TH STORM نیا

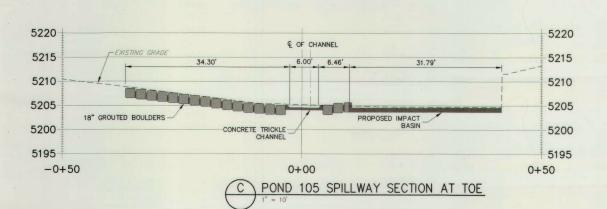
SHEET 12 OF 33

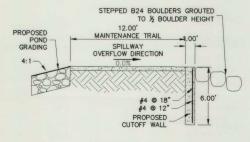


5220 5220 8" CONCRETE _ MAINTANENCE ACCESS 5215 5215 & OF CHANNEL 5210 5210 PROPOSED CONCRETE CUTOFF WALL 5205 5205 EXISTING GRADE 5200 5200 5195 5195 5190 5190 -0+500+00 0+50 A POND 105 SPILLWAY SECTION AT CUTOFF WALL

NOTE.
(AB) - INDICATES AS BUILT CONDITION
AS CONSTRUCTED
11/2018







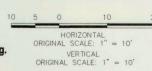
PROPOSED CUTOFF
WALL DETAIL

SCALE: 1"=5'

NOTES:

1. SEE SHEET 14 FOR SECTION LOCATIONS





FOR INFORMATION ONLY

E: 1" = 10,

AVENUE WATER QUALITY
POND

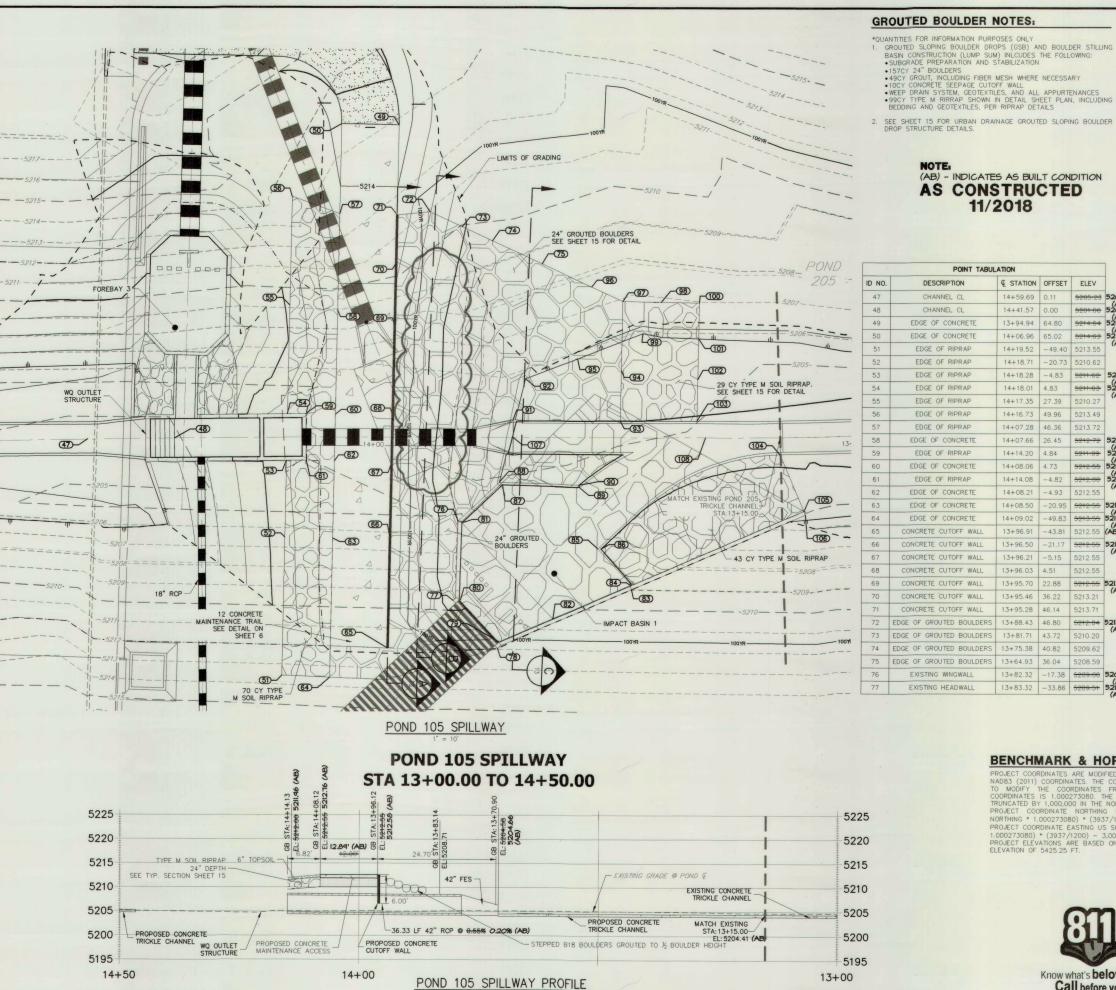
SHEET 13 OF 33
JOB NO. 14421.32

PROFILE

AND

SPILLWAY PLAN

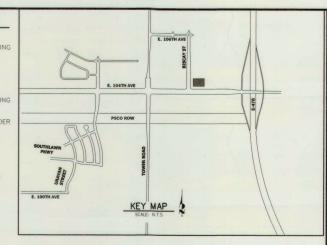
J-R ENGINEERING



GROUTED BOULDER NOTES:

- SEE SHEET 15 FOR URBAN DRAINAGE GROUTED SLOPING BOULDER DROP STRUCTURE DETAILS.

(AB) - INDICATES AS BUILT CONDITION AS CONSTRUCTED 11/2018



	ELEV	OFFSET	& STATION	DESCRIPTION	ID NO.
5205.	5205:23	0.11	14+59.69	CHANNEL CL	47
(AB)	5201.66	0.00	14+41.57	CHANNEL CL	48
(AB)	5214.64	64.80	13+94.94	EDGE OF CONCRETE	49
(AB)	5214.63	65.02	14+06.96	EDGE OF CONCRETE	50
(AB)	5213.55	-49.40	14+19.52	EDGE OF RIPRAP	51
2	5210.62	-20.73	14+18.71	EDGE OF RIPRAP	52
5211.5	5211.62	-4.83	14+18.28	EDGE OF RIPRAP	53
	5211.63	4.83	14+18.01	EDGE OF RIPRAP	54
(AB)	5210.27	27.39	14+17.35	EDGE OF RIPRAP	55
9	5213.49	49.96	14+16.73	EDGE OF RIPRAP	56
2	5213.72	46.36	14+07.28	EDGE OF RIPRAP	57
5212.8	5212.72	26.45	14+07.66	EDGE OF CONCRETE	58
(AB)	5211.99	4.84	14+14.20	EDGE OF RIPRAP	59
	5212.55	4.73	14+08.06	EDGE OF CONCRETE	60
	5212.00	-4.82	14+14.08	EDGE OF RIPRAP	61
(AB)	5212.55	-4.93	14+08.21	EDGE OF CONCRETE	62
	5212.55	-20.95	14+08.50	EDGE OF CONCRETE	63
	5213.55	-49.83	14+09.02	EDGE OF CONCRETE	64
(AB)	5212.55	-43.81	13+96.91	CONCRETE CUTOFF WALL	65
	5212.55	-21.17	13+96.50	CONCRETE CUTOFF WALL	66
(AB)	5212.55	-5.15	13+96.21	CONCRETE CUTOFF WALL	67
	5212.55	4.51	13+96.03	CONCRETE CUTOFF WALL	68
	5212.55	22.88	13+95.70	CONCRETE CUTOFF WALL	69
(AB)	5213.21	36.22	13+95.46	CONCRETE CUTOFF WALL	70
	5213.71	46.14	13+95.28	CONCRETE CUTOFF WALL	71
	5212.04	46.80	13+88.43	EDGE OF GROUTED BOULDERS	72
(AB)	5210.20	43.72	13+81.71	EDGE OF GROUTED BOULDERS	73
2	5209.62	40.82	13+75.38	EDGE OF GROUTED BOULDERS	74
9	5208.59	36.04	13+64.93	EDGE OF GROUTED BOULDERS	75
	5209.00	-17.38	13+82.32	EXISTING WINGWALL	76
52II.60	5209.51	-33.86	13+83.32	EXISTING HEADWALL	77

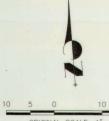
	POINT TABUL	ATION			
ID NO.	DESCRIPTION	€ STATION	OFFSET	ELEV	
78	EXISTING HEADWALL	13+73.96	-43.81	5211.97	
79	EDGE OF CONCRETE	13+73.75	-42.39	5204.60	
80	EDGE OF CONCRETE	13+81.75	-33.72	5204.60	
81	EDGE OF CONCRETE	13+81.50	-17.75	5204.60	5204.58 (AB)
82	EDGE OF CONCRETE	13+62.49	-37.69	5208.70	(AD)
83	EXISTING WINGWALL	13+46.07	-31.54	5209.00	
84	EDGE OF CONCRETE	13+46.35	-30.62	5204.83	5204.88
85	EDGE OF CONCRETE	13+53.10	-23.10	5204.52	(AB)
86	EDGE OF RIPRAP	13+52.40	-23.11	5205.03	(AB)
87	EDGE OF CONCRETE	13+73.04	-9.94	5204.57	5204.61
88	TOE	13+73.73	-9.24	5205.88	5205.86
89	EDGE OF CONCRETE	13+56.95	-10.35	5204.52	5204.46
90	NULL STRUCTURE	13+57.13	-9.85	5205.01	5205.00
91	EDGE OF GROUTED BOULDERS	13+70.90	3.75	5205.86	5205.TT
92	TOE	13+68.37	12.16	5205.67	(AB)
93	EDGE OF GROUTED BOULDERS	13+48.53	3.47	5205.01	5205.21
94	EDGE OF GROUTED BOULDERS	13+48.31	13.96	5205.41	(AB)
95	TOE	13+57.47	16.36	5205.67	
96	EDGE OF GROUTED BOULDERS	13+54.57	31.27	5207.57	5201.30
97	EDGE OF GROUTED BOULDERS	13+48.04	28.27	5206.92	5206.94
98	EDGE OF RIPRAP	13+40.02	28.11	5206.86	(AB)
99	TOE	13+43.82	21.60	5205.62	
100	EDGE OF RIPRAP	13+32.04	27.96	5206.96	
101	TOE	13+32.19	20.52	5205.50	
102	EDGE OF RIPRAP	13+32.36	12.05	5205.24	
103	EDGE OF RIPRAP	13+32.53	3.43	5204.97	
104	EDGE OF RIPRAP	13+15.06	-3.51	5204.91	5204.96
105	EDGE OF RIPRAP	13+10.40	-15.36	5205.59	(AB) 5205.05
106	EXISTING WINGWALL	13+10.09	-16.13	5205.65	(AB)
107	CHANNEL CL	13+70.90	0.00	5204.60	5204.66
108	CHANNEL CL	13+30.71	0.00	5204.46	(AB) 5204.53

BENCHMARK & HORIZONTAL DATUM

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Know what's below.

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ORIGINAL SCALE: 1" = 10"

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36742 Claron 2 Cluth

AARON LEE CLUTTER, P.E. COLORADO NO. 36742 FOR AND ON BEHALF OF JR ENGINEERING, LLC.

SHEET 14 OF 33

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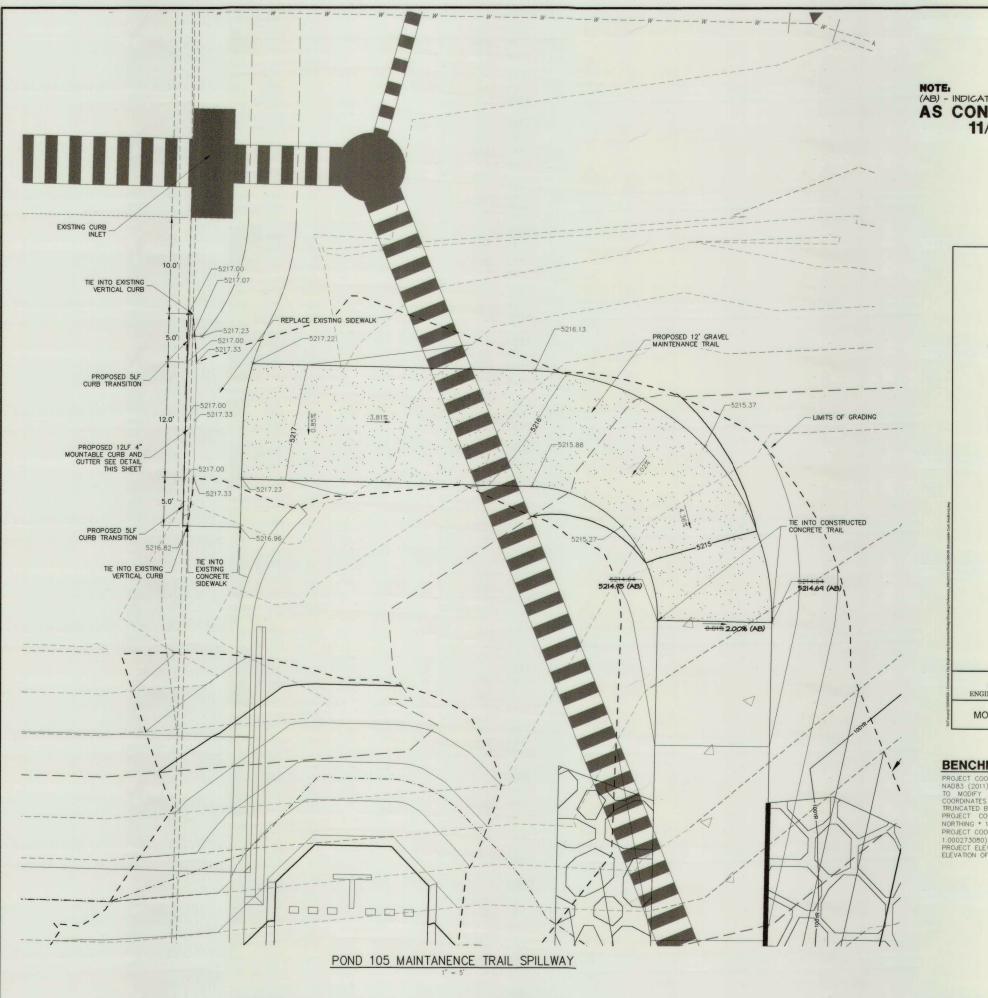
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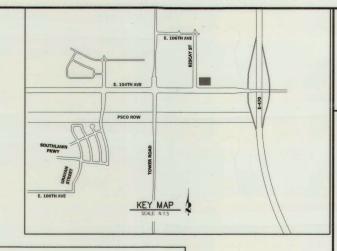
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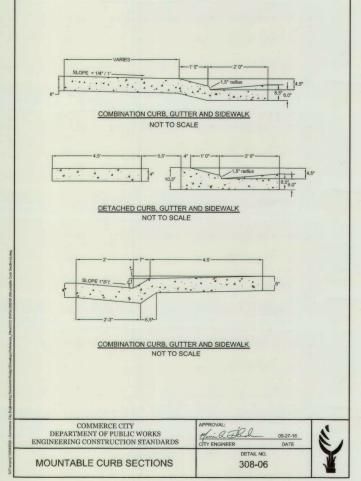
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NOTE:
(AB) - INDICATES AS BUILT CONDITION
AS CONSTRUCTED
11/2018

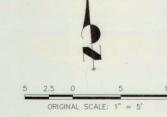




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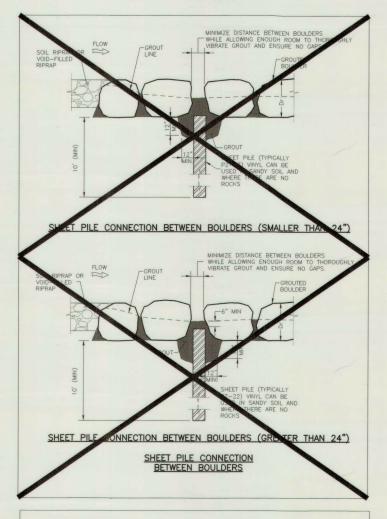
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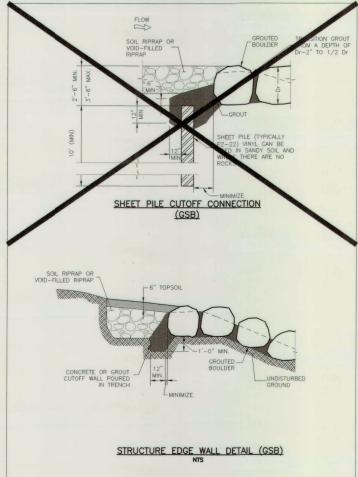
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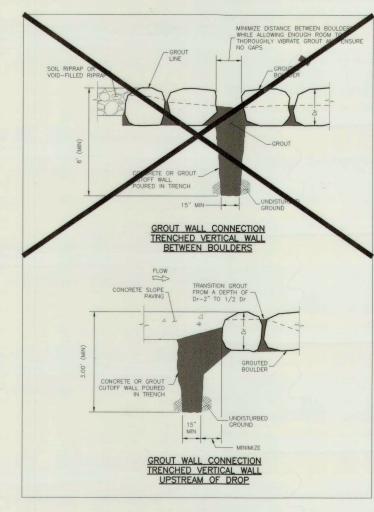
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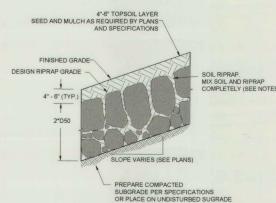
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QUALITY AVENUE WATER (AND PLAN نیا









TYPICAL SECTION -SOIL RIPRAP WITH MULCH

RIPRAP NOTES:

1. SOIL RIPRAP DETAILS ARE APPLICABLE TO AREAS. SLOPED REFER TO THE SITE PLAN ACTUAL LOCATION AND LIMITS.
2. MIX UNIFORMLY 65% RIPRAP BY WITH 35% OF APPROVED SOIL VOLUME BY VOLUME PRIOR TO PLACEMENT.
3. PLACE STONE—SOIL MIX TO RESULT IN SECURELY INTERLOCKED ROCK AT THE DESIGN THICKNESS AND GRADE. COMPACT AND ALL LEVEL TO ELIMINATE VOIDS AND ROCKS PROJECTING DESIGN ABOVE RIPRAP TOP GRADE.
4. CRIMP OR TACKIFY MULCH OR USE APPROVED HYDROMULCH AS CALLED FOR IN THE PLANS AND SPECIFICATIONS.

TY	PF	L	RIP	RAP	

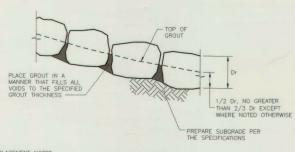
TYPE L RIPI	RAP
INTERMEDIATE	PERCENT
ROCK DIMENSION	PASSING
(IN.)	(%)
15	70-100
12	50-70
9	35-50
3	2-10

TYPE L RIPRAP D50=9"

TYPE M RIPRAP

INTERMEDIATE	PERCENT
ROCK DIMENSION	PASSING
(IN.)	(%)
21	70-100
18	50-70
12	35-50
4	2-10

TYPE M RIPRAP D50=12".



BOULDER PLACEMENT NOTES:

1. PLACE BOULDERS WITH THE REQUIRED BOULDER HEIGHT VERTICAL. PLACE BOULDERS AS TIGHTLY TOGETHER AS POSSIBLE (WITHOUT TOUCHING) WHILE PROVIDING ENOUGH ROOM BETWEEN THEM TO THOROUGHLY MERATE THE GROUT AND TO ENSURE NO GAPS IN THE GROUT. THE SMALL DIMENSION OF A 2X4 CAN BE USED AS A GUIDE TO CHECK MINIMUM SPACING.

2. BEFORE GROUTING, CLEAN ALL DIRT AND MATERIAL FROM ROCK THAT COULD PREVENT THE GROUT FROM BINDING TO THE ROCK. KEEP BOULDERS FROM TOUCHING, AVOID SLIDING BOULDERS AGAINST SUBGRADE TO PROPERLY POSITION.

MATERIAL SPECIFICATIONS:

1. ALL GROUT SHALL HAVE A MINIMUM 28—DAY COMPRESSIVE STRENGTH EQUAL TO 3200 PSI.

2. ONE CUBIC YARD OF GROUT SHALL HAVE A MINIMUM OF SIX (6) SACKS OF TYPE II PORTLAND CEMENT.

3. A MAXIMUM OF 25% TYPE F FLY ASH MAY BE SUBSTITUTED FOR THE PORTLAND CEMENT.

4. THE AGGREGATE SHALL BE COMPRISED OF 70% NATURAL SAND (FINES) AND 30% %—INCH ROCK

(COARSE).

5. THE GROUT SLUMP SHALL BE BETWEEN 4-INCHES TO 6-INCHES.

6. AIR ENTRAINMENT SHALL BE BETWEEN 5.5% AND 7.5%.

7. TO CONTROL SHRINKAGE AND CRACKING, 1.5 POUNDS OF FIBERMESH, OR EQUIVALENT, SHALL BE USED PER CUBIC YARD OF GROUT.

8. COLOR ADDITIVE IN REQUIRED AMOUNTS SHALL BE USED WHEN SO SPECIFIED BY CONTRACT.

GROUT PLACEMENT SPECIFICATIONS:

1. SPECIAL PROCEDURES SHALL BE REQUIRED FOR GROUT PLACEMENT WHEN THE AIR TEMPERATURES ARE LESS THAN 40F OR GREATER THAN 90F. CONTRACTOR SHALL OBTAIN PRIOR APPROVAL FROM THE DESIGN ENGINEER OF THE PROCEDURES TO BE USED FOR PROTECTING THE GROUT.

2. GROUT SHALL BE DELIVERED BY MEANS OF A LOW PRESSURE (LESS THAN 10 PSI) GROUT PUMP USING A 2—INCH DIAMPETER (MAXIMUM) NOZZUE.

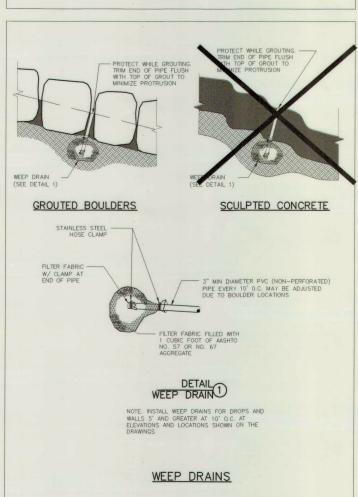
3. FULL DEPTH PENETRATION OF THE GROUT INTO THE BOULDER VOIDS SHALL BE ACHIEVED BY INJECTING GROUT STATING WITH THE NOZZUE NEAR THE BOTTOM AND RAISING IT AS THE GROUT FILLS, WHILE VIBRATING GROUT INTO PLACE USING A PENCIL VIBRATOR.

4. ALL GROUT BETWEEN BOULDERS SHALL BE TREATED WITH A BROOM FINISH.

5. AFTER GROUT PLACEMENT, EXPOSED BOULDER FACES SHALL BE CLEANED AND FREE OF GROUT.

6. ALL FINISHED GROUT SURFACES SHALL BE SPRAYED WITH A CLEAR LIQUID MEMBRANE CURING COMPOUND AS SPECIFIED IN ASTM C309.

GROUTED BOULDER PLACEMENT DETAIL



GROUTED BOULDER NOTES:

- BOULDERS USED FOR GROUTING SHOULD MEET ALL THE PROPERTIES OF ROCK FOR ORDINARY RIPRAP, AND ROCK OF UNIFORM SIZE SHOULD BE USED.
- ROCK SHALL BE HARD, DURABLE, AND FREE FROM CRACKS, OVERBURDEN, SHALE, AND ORGANIC MATTER.
- 3. GROUTED BOULDERS SHALL BE PLACED DIRECTLY ON STABILIZED, COMPACTED SUBGRADE WITHOUT GRANULAR BEDDING. 4. THE TOP ONE-HALF OF THE BOULDERS SHALL BE LEFT UNGROUTED AND EXPOSED.
- 5. ROCK HAVING A MINIMUM SPECIFIC GRAVITY OF 2.65 IS PREFERRED; HOWEVER, IN NO CASE SHALL ROCK HAVE A SPECIFIC GRAVITY LESS THAN 2.50.
- 6. WEEP HOLES SHALL BE PROVIDED AT THE TOE OF CHANNEL SLOPES AND CHANNEL DROPS TO REDUCE UPLIFT FORCES ON THE GROUTED CHANNEL LINING.
- 7. GROUTED BOULDERS ON THE BANKS SHALL BE BURIED AND VEGETATED WITH DRY-LAND GRASSES AND SHRUBS. COVER GROUTED BOULDERS WITH SLIGHTLY COMPACTED TOPSOIL, FILLING DEPRESSIONS AND COVERING THE TOP OF THE TALLEST ROCKS TO A HEIGHT OF NO LESS THAN 4-INCHES (6-INCHES OF MORE PREFERRED) TO ESTABLISH DRY-LAND VEGETATION.
- 8. PLACEMENT AND GROUTING OF BOULDERS SHALL GENERALLY CONFORM TO THE SPECIFICATIONS AND DETAILS FOR GROUTED BOULDER DROPS. SEE DETAILS AND NOTES FOR GROUTED BOULDER DROPS ON THIS SHEET.

(AB) - INDICATES AS BUILT CONDITION AS CONSTRUCTED 11/2018



INFORMATION ONLY

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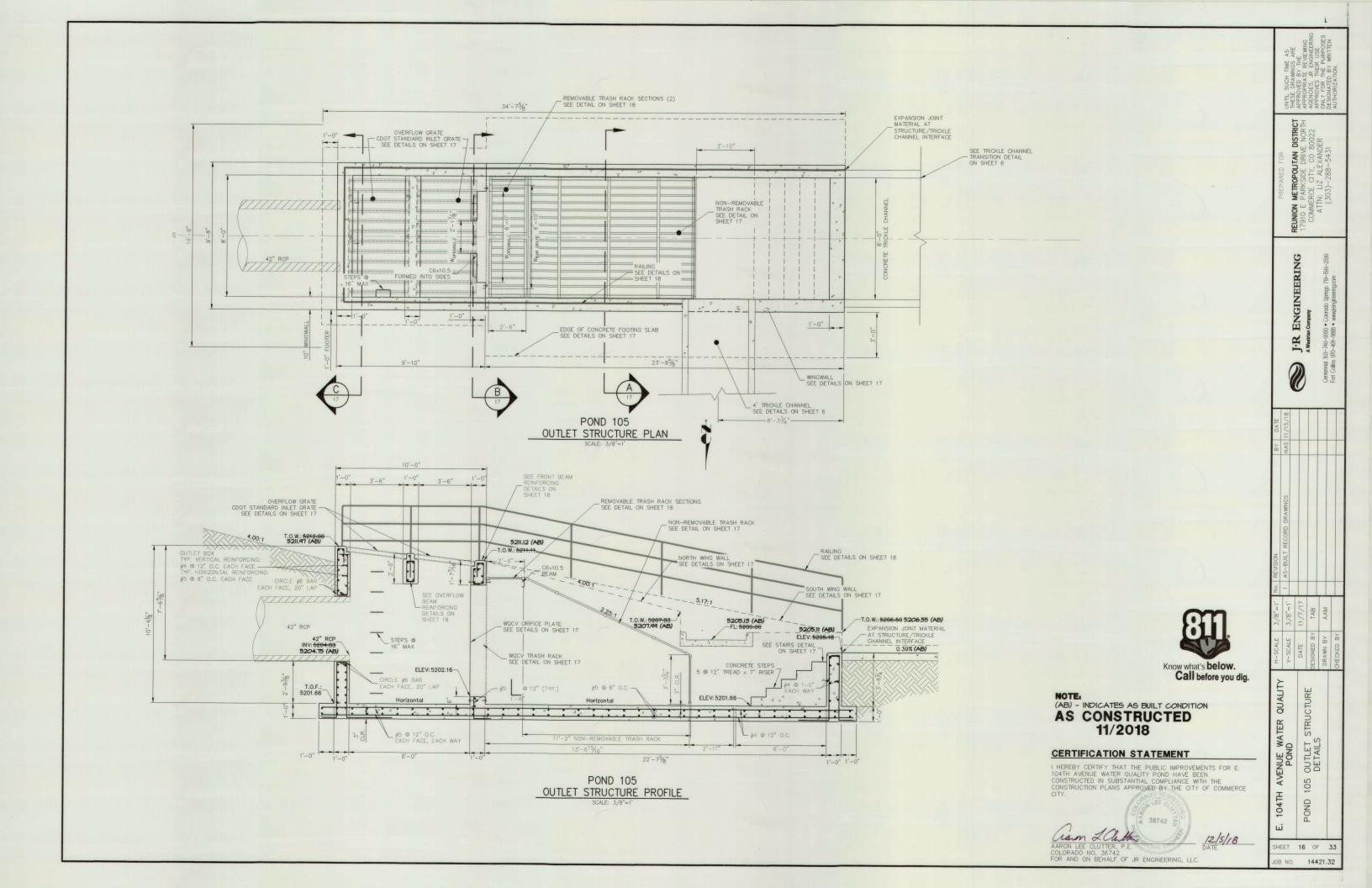
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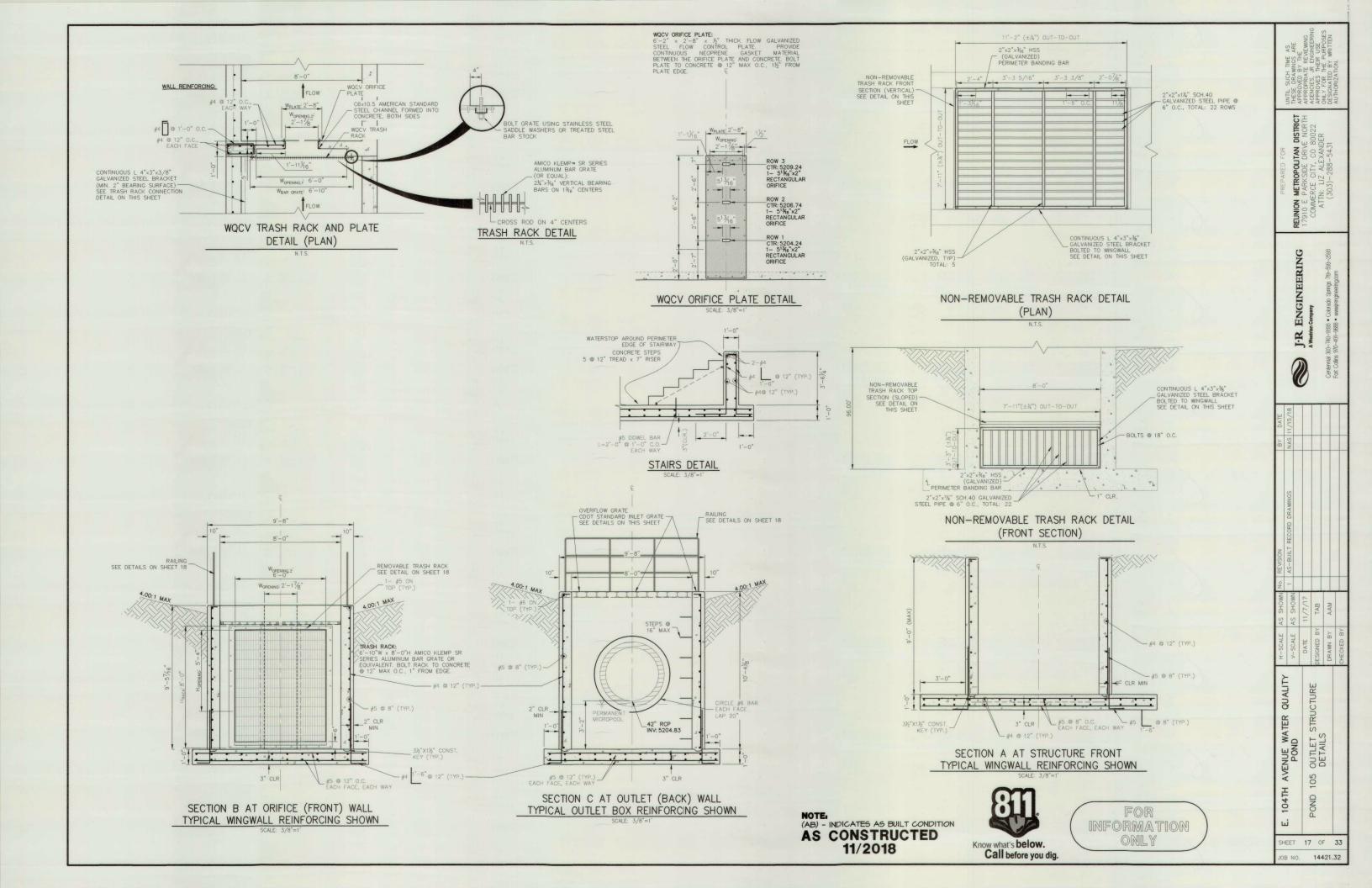


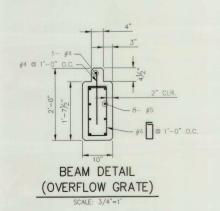
QUALITY PROFILE

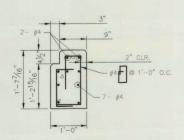
AVENUE WATER (AND PLAN 104TH نیا

SHEET 15 OF 33

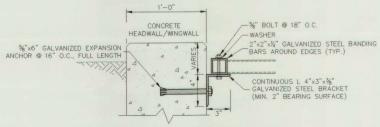




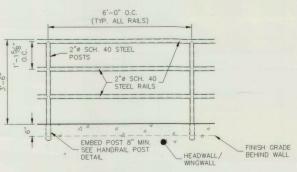




BEAM DETAIL (FRONT OF BEAM)



TRASH RACK CONNECTION TO WALLS



PEDESTRIAN RAILING DETAIL

PEDESTRIAN RAILING NOTES:

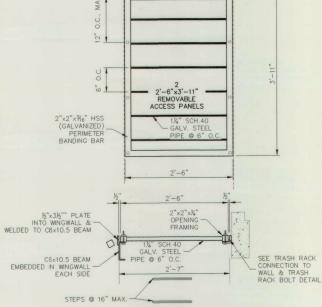
- GRIND ALL WELDS SMOOTH.

 2. HANDRAIL PAINT SHALL CONFORM TO CDOT STANDARD SPECIFICATION 509.24. ALL STEEL RAILING SHALL BE PAINTED USING A TWO-COAT SYSTEM WITH INDRCANIC ZINC-RICH PRIMER (SHOP COAT) AND HIGH-BIULD URETHANE TOP COAT. THE SHOP COAT SHALL HAVE A DRY FILM THICKNESS OF 3.0 MILS. THE TOP COAT SHALL HAVE A THICKNESS OF 3.0 MILS. COLOR: BLACK.

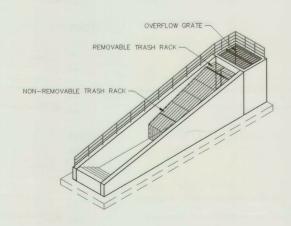
 3. RAILING POSTS SHALL BE SET NORMAL TO GRADE RAILS SHALL RUN PARALLEL TO THE SLOPES OF TOPS OF THE WALLS.

 4. HANDRAIL SHALL BE REQUIRED AT ALL WALLS GREATER THAN 2"-6" IN HEIGHT AND AT ALL LOCATIONS SHOWN ON THE PLANS.

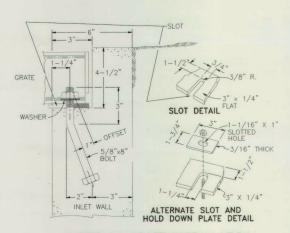
 5. CONTRACTOR SHALL SUBMIT HANDRAIL SHOP DERAWINGS TO ENGINEER OF RECORD FOR APPROVAL PRIOR TO FABRICATION.



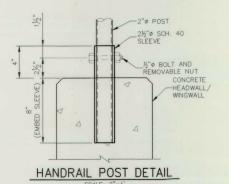
REMOVABLE TRASH RACK DETAIL



POND 105 OUTLET STRUCTURE ISOMETRIC VIEW



OVERFLOW GRATE INSTALLATION DETAIL



NOTE: (AB) - INDICATES AS BUILT CONDITION AS CONSTRUCTED 11/2018

FOR INFORMATION ONLY

OUTLET STRUCTURE STRUCTURAL NOTES:

ALL CONCRETE SHALL BE CLASS D IN ACCORDANCE WITH CDOT STANDARD SPECIFICATIONS FOR ROAD AND BRIDGE CONSTRUCTION.

CONSTRUCTION.

STRUCTURE EXCAVATION AND BACKFILL SHALL BE IN ACCORDANCE WITH CDOT STD. M-206-1.
DO NOT BACKFILL UNTIL CONCRETE HAS REACHED DESIGN STRENGTH, F'c.
GRADE 60 REINFORCING STEEL AND EPOXY COATED ARE REQUIRED.
THE MINIMUM LAP SPLICE LENGTH FOR EPOXY COATED REINFORCING BARS SHALL BE:

BAR SIZE: #4 #5 #6 #7 #8 #9 #10 #11 SPLICE LENGTH: 1'-3" 1'-6" 1'-10" 2'-2" 3'-8" 4'-8" 5'-11" 7'-3"

THE MINIMUM	LAP	SPLICE	LENGTH	FOR	BLACK	REINFOR	CING	BARS	SHAL	. 1
F 0.10 017F		11.4	ur	110	1 117	T #0 T	110	114	0 1	174.4

10. REINFORCING BARS SHALL BE DEFORMED AND SHALL HAVE A MINIMUM OF 2" CLEARANCE.

11. ALL EXPOSED CONCRETE CORNERS SHALL BE CHAMFERED 3".

12. STEPS SHALL BE PROVIDED WHEN STRUCTURE INTERIOR HEIGHT EXCEEDS 3"-6" AND SHALL BE IN ACCORDANCE WITH ASSHTO M 199.

13. IT SHALL BE THE CONTRACTOR'S RESPONSIBILITY TO VERIFY THE LOCATIONS OF EXISTING STRUCTURES AND EXISTING UTILITIES, PRIOR TO CONSTRUCTION OF THE CAST—IN—PLACE STRUCTURES. FIELD MODIFICATIONS OF PRECAST UNITS TO ACCOMMODATE CAST—IN—PLACE STRUCTURES WILL ONLY BE ACCEPTABLE WITH THE ENGINEER'S APPROVAL.

14. CONTRACTOR SHALL SUBMIT STEEL REINFORCING SHOP DRAWNGS FOR ALL CAST—IN—PLACE STRUCTURES FOR ENGINEER'S APPROVAL PRIOR TO CONSTRUCTION.

OUTLET STRUCTURE PLATE AND GRATING NOTES:

ORIFICE PLATE AND RESTRICTOR PLATE:

1. PROVIDE GASKET MATERIAL BETWEEN THE ORIFICE PLATE AND CONCRETE AND BETWEEN THE

RESTRICTOR PLATE AND CONCRETE.
BOLT PLATE TO CONCRETE 12" MAX. ON CENTER.

RESTRICTOR PLATE AND CONCRETE.

2. BOLT PLATE TO CONCRETE IZ* MAX. ON CENTER.

FUREY AND WOCV TRASH RACKS.

3. BAR GRATE TRASH RACKS.

3. BAR GRATE TRASH RACKS.

4. TRASH RACKS.

4. TRASH RACKS SHALL BE 1½" SCH.40 STEEL PIPE, GALVANIZED,

6 6" CENTERS. SUPPORT BARS SHALL BE ½"x2" STEEL RECTANGULAR BARS, GALVANIZED,

6 6" CENTERS. SUPPORT BARS SHALL BE ½"x2" STEEL RECTANGULAR BARS, GALVANIZED,

6 6" CENTERS. SUPPORT BARS SHALL BE HOT DIP GALVANIZED AND PROVIDED WITH BOLTABLE ACCESS PANELS.

5. STEEL TRASH RACKS SHALL BE HOT DIP GALVANIZED AND MAY BE HOT POWDER COATED AFTER GALVANIZING.

6. STRUCTURAL STEEL FOR GRATES, ORIFICE PLATES, AND BARS SHALL BE GALVANIZED AND SHALL BE IN ACCORDANCE WITH COOT STANDARD SPECIFICATIONS, SUBSECTION 712.06.

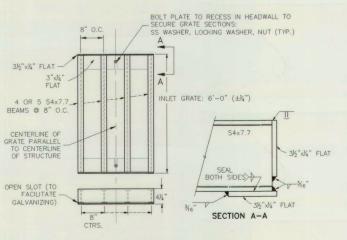
7. ALL HARDWARE, BOLTS, AND FASTENERS SHALL BE STAINLESS STEEL.

8. CONTRACTOR SHALLS SUBMIT SHOP DRAWNINGS FOR ALL PLATES AND GRATING FOR ENGINEER'S APPROVAL PRIOR TO CONSTRUCTION.

OVERFLOW GRATE:

9. ALL OVERFLOW GRATES SHALL BE MOUNTED USING STAINLESS STEEL HARDWARE AND PROVIDED WITH HINGED & LOCKABLE OR BOLTABLE ACCESS PANELS AS SHOWN ON THE PLANS.

10. OVERFLOW GRATES SHALL BE HOT DIP GALVANIZED STEEL AND MAY BE HOT POWDER COATED



OVERFLOW GRATE DETAILS



Know what's below. Call before you dig.

THESE APPRO APPRO AGENCI APPRO ONLY DESIGN

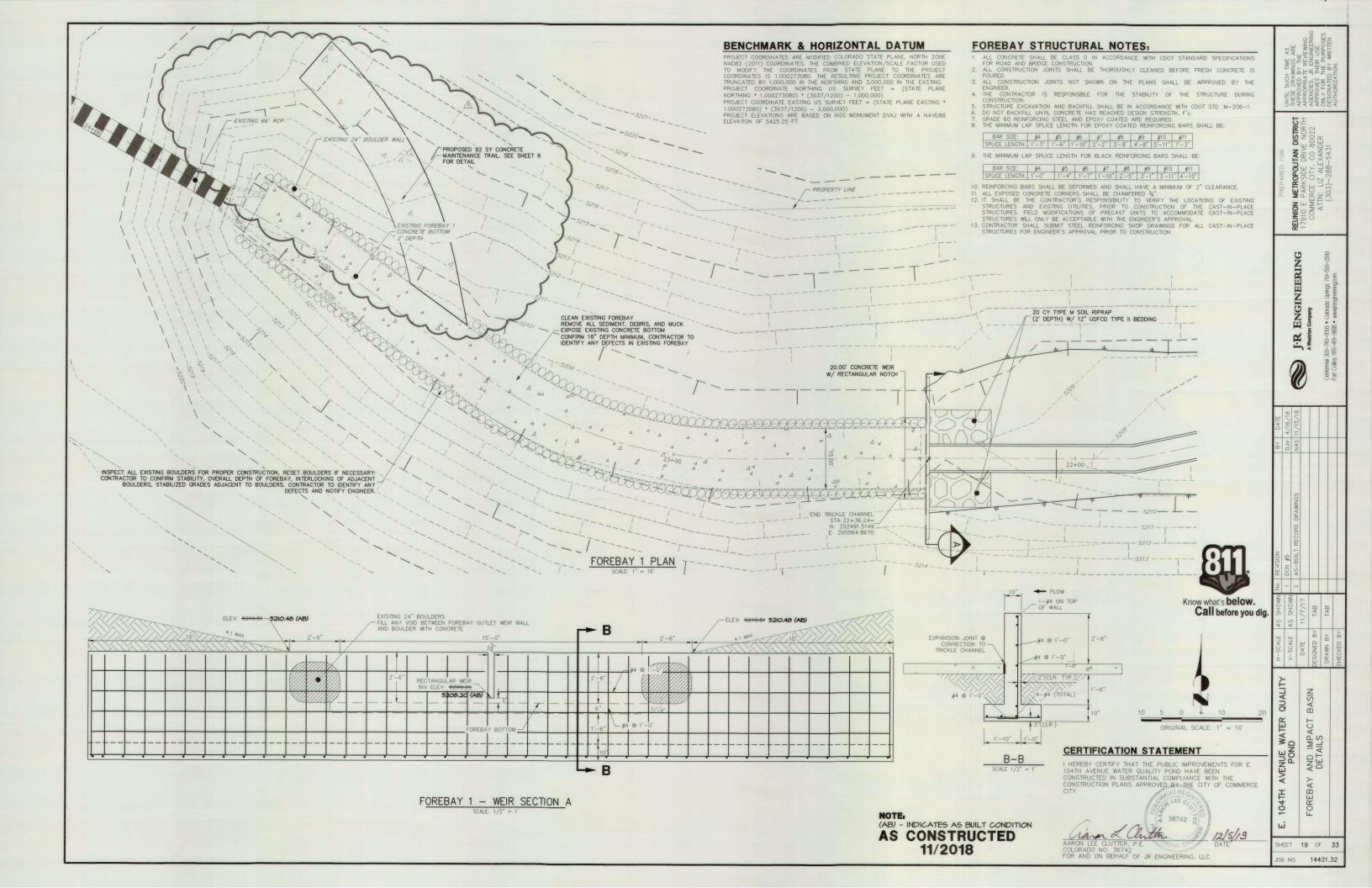
WETROPOLIAN DISTRICT
E PARKSIDE DRIVE NORTH
WERCE CITY, CO 80022
TIN: LIZ ALEXANDER
(303)-288-5431

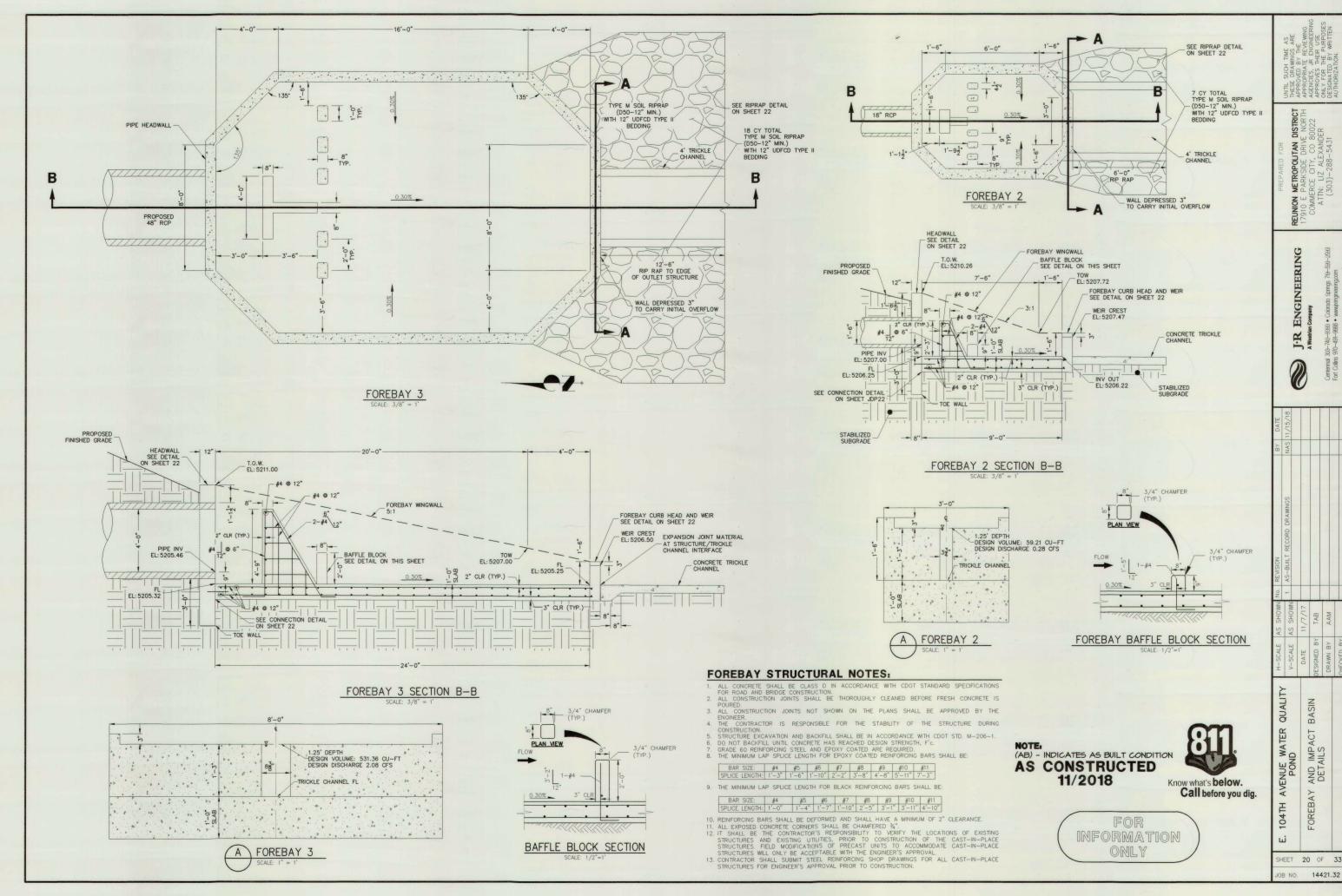
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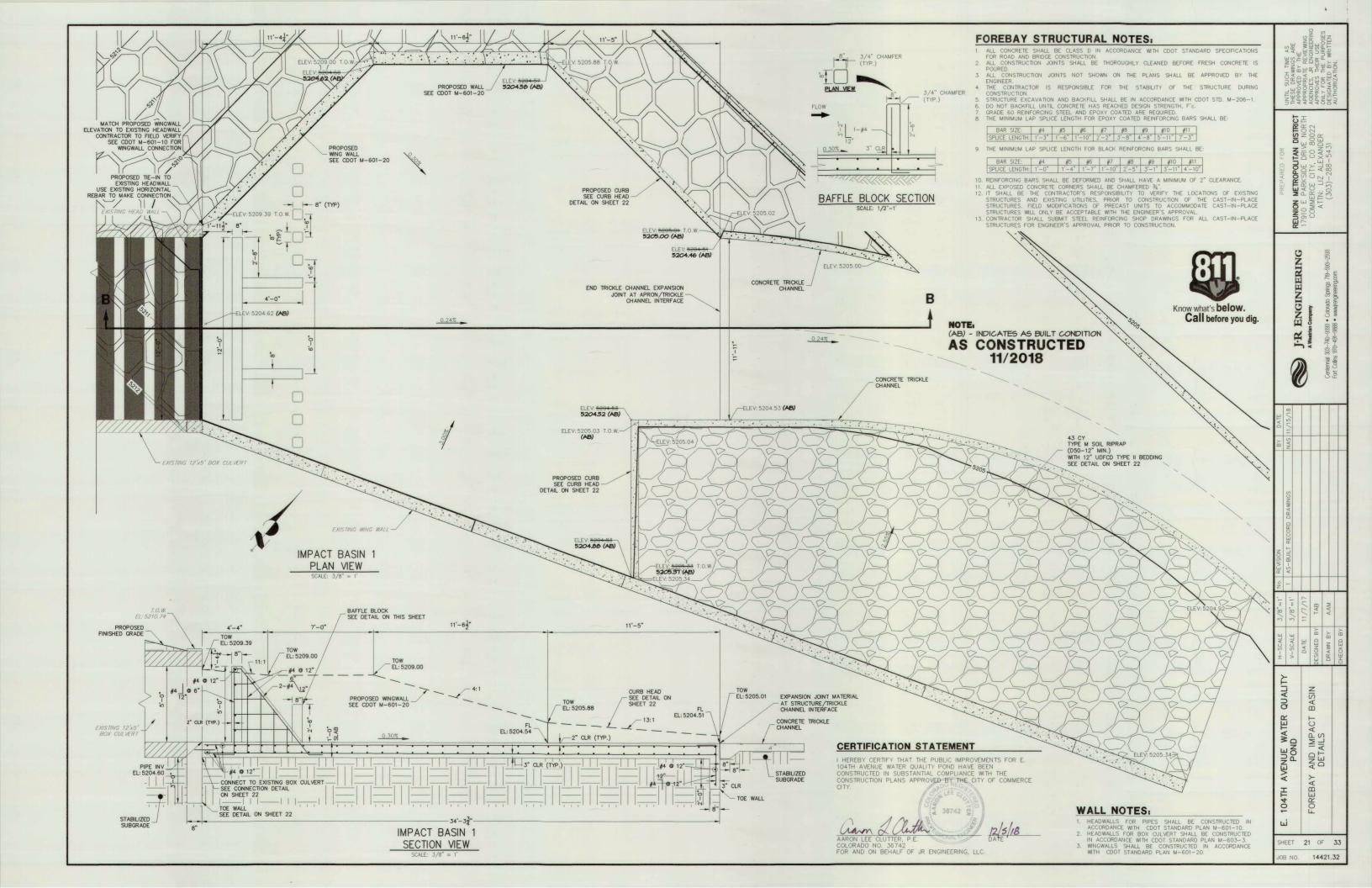
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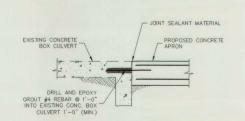
DETAILS AVENUE WATER (STRUCTURE OUTLET 104TH نیا

SHEET 18 OF 33 14421.32

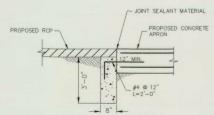




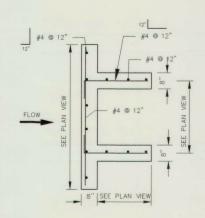




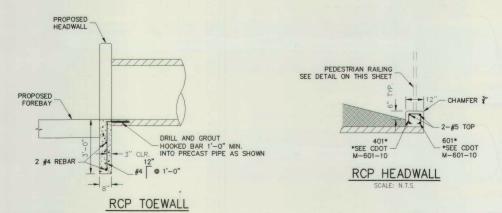
CONNECTION TO EXISTING BOX CULVERT

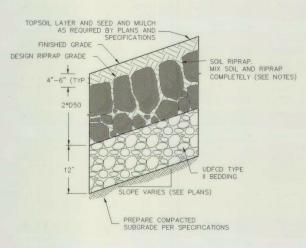


CONNECTION TO PROPOSED RCP TOEWALL

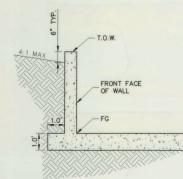


IMPACT BASIN 1 BAFFLE BLOCK PLAN





SOIL RIPRAP EMBANKMENT PROTECTION WITH BEDDING TYP. SECTION

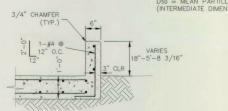


FOREBAY WALL SECTION/LEGEND

TYPE M RIPRAP

INTERMEDIATE	PERCENT
ROCK DIMENSION	PASSING
(IN.)	(%)
21	70-100
18	50-70
12	35-50
4	2-10

*TYPE M RIPRAP D50=12". D50 = MEAN PARTICLE SIZE (INTERMEDIATE DIMENSION) BY WEIGHT.



FOREBAY CURB HEAD AND WEIR/WINGWALL REINFORCING DETAIL

RIPRAP NOTES:

1.	SOIL RIPRAP	DETAILS A	RE APPLIC	ABLE TO	SLOPED	AREAS.	REFER	ТО	THE	SITE
	PLAN ACTUA	L LOCATION	AND LIMI	TS.						
2	MIY LINIEODA	HV 659 DI	DDAD DV	WOLLIME	WITLE	ZEST OF	ADDDOM	ED	COIL	DV

PLAN ACTUAL LOCATION AND LIMITS.

2 MIX UNIFORMLY 65% RIPRAP BY VOLUME WITH 35% OF APPROVED SOIL BY VOLUME PRIOR TO PLACEMENT.

3 PLACE STONE-SOIL MIX TO RESULT IN SECURELY INTERLOCKED ROCK AT THE DESIGN THICKNESS AND GRADE. COMPACT AND LEVEL TO ELIMINATE ALL VOIDS AND ROCKS PROJECTING ABOVE DESIGN RIPRAP TOP GRADE.

4. CRIMP OR TACKIFY MULCH OR USE APPROVED HYDROMULCH AS CALLED FOR IN THE PLANS AND SPECIFICATIONS.

5. ROCK SHAUL BE HARD, DURABLE, ANGULAR IN SHAPE, AND FREE FROM CRACKS, OVERSURDEN, SHALE, AND ORGANIC MATTER.

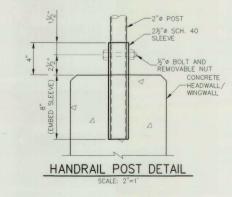
6. NEITHER BREADTH NOR THICKNESS OF A SINGLE STONE SHOULD BE LESS THAN ONE—THIRD ITS LENGTH, AND ROUNDED STONE SHOULD BE AVOIDED.

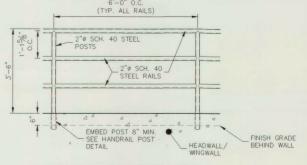
7. THE ROCK SHOULD SUSTAIN A LOSS OF NOT MORE THAN 40% AFTER 50. REVOLUTIONS IN AN ABRASION TEST (LOS ANGELES MACHINE ASTM C—5355—69) AND SHOULD SUSTAIN A LOSS OF NOT MORE THAN 10% AFTER 12 CYCLES OF FREEZING AND THAWING (AASHTO TEST 103 FOR LEDGE ROCK PROCEDURE A).

8. ROCK HAWING A MINIMUM SPECIFIC GRAVITY OF 2.65 IS PREFERRED; HOWEVER, IN NO CASE SHOULD ROCK HAVE A SPECIFIC GRAVITY LESS THAN 2.50.

WALL NOTES:

- HEADWALLS FOR PIPES SHALL BE CONSTRUCTED IN ACCORDANCE WITH CODT STANDARD PLAN M-601-10.
 HEADWALLS FOR BOX CULVERT SHALL BE CONSTRUCTED IN ACCORDANCE WITH CODT STANDARD PLAN M-603-3.
 WINGWALLS SHALL BE CONSTRUCTED IN ACCORDANCE WITH CDDT STANDARD PLAN M-601-20.





PEDESTRIAN RAILING DETAIL

NOTE:
(AB) - INDICATES AS BUILT CONDITION
AS CONSTRUCTED 11/2018



FOR INFORMATION ONLY

UNTIL THESE APPRO APPRO APPRO ONLY DESIGN

DRIVE NORTH
CO 80022
EXANDER
-5431 METROPOLITAN

ENGINEERING J-R.

QUALITY

FOREBAY & IMPACT BASIN STANDARD DETAILS AVENUE WATER POND 104TH نیا

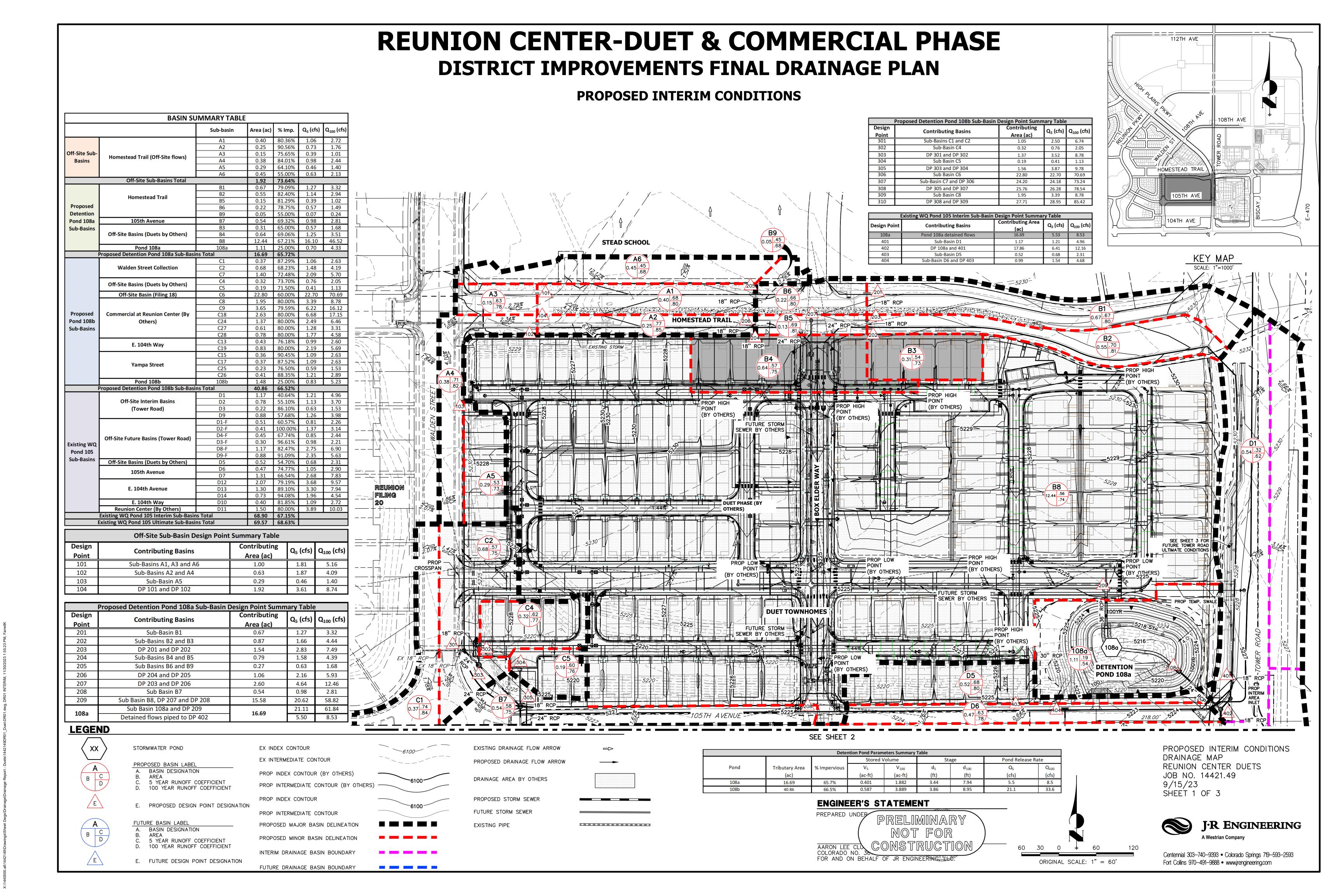
SHEET 22 OF 33

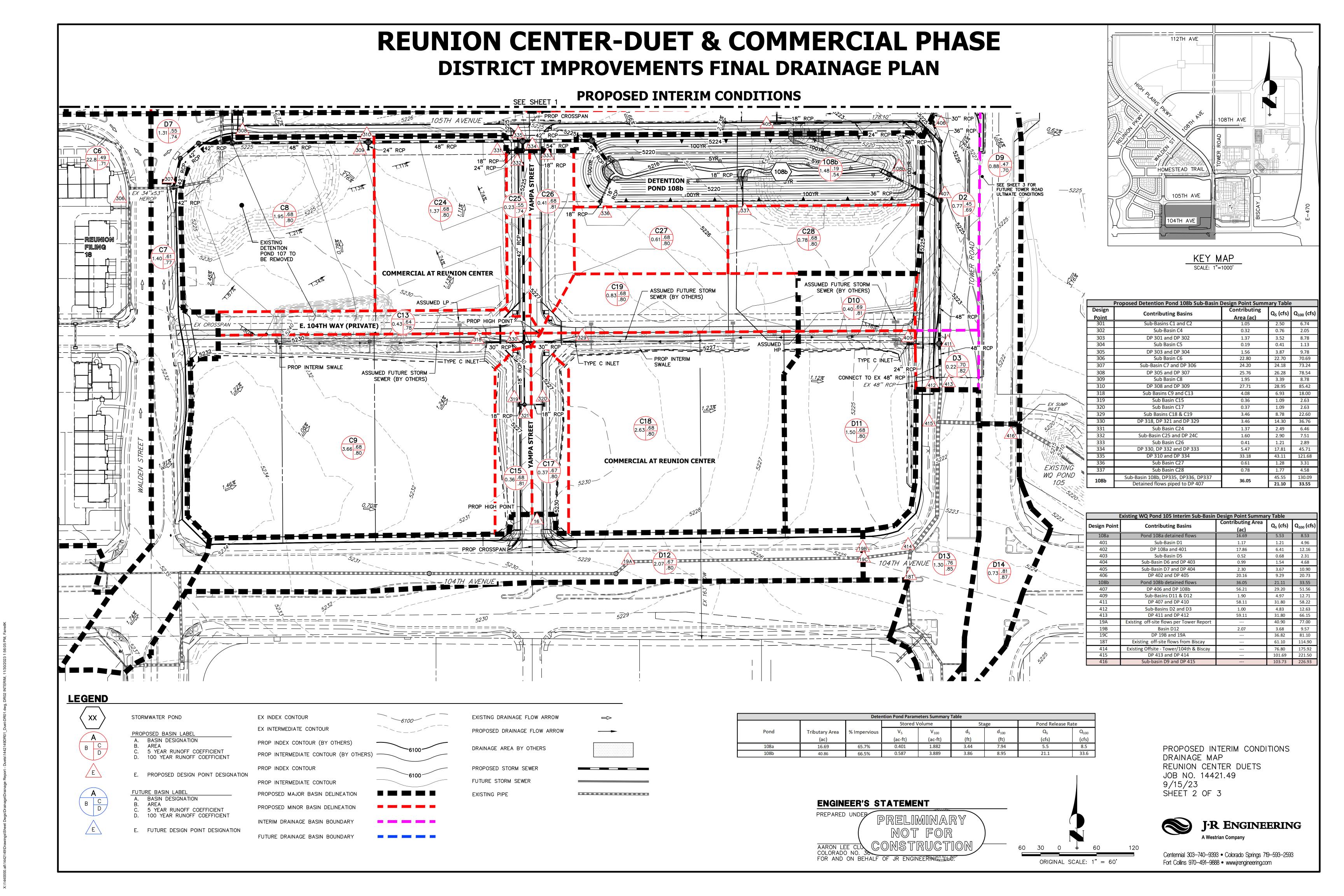
FINAL DRAINAGE REPORT FOR REUNION CENTER – DUET & COMMERCIAL PHASE DISTRICT INFRASTRUCTURE

November 30, 2023

Prepared For: **Reunion Metropolitan District**17910 East Parkside Drive North
Commerce City, Colorado 80022
Contact: Matt Urkoski

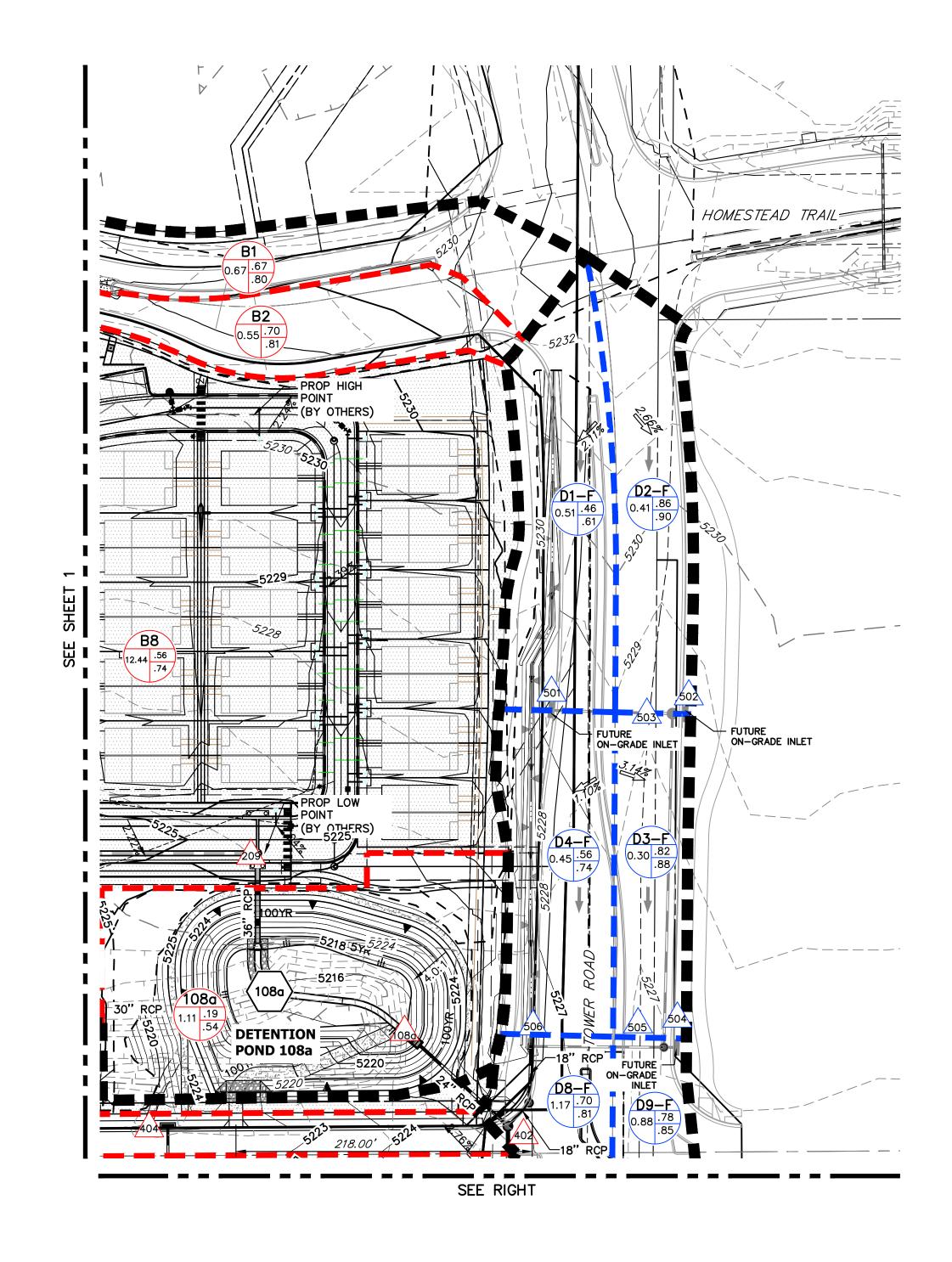
Prepared By: JR ENGINEERING, LLC 7200 S Alton Way, Suite C400 Centennial, Colorado 80112 (303) 740-9393 Contact: Aaron Clutter, PE

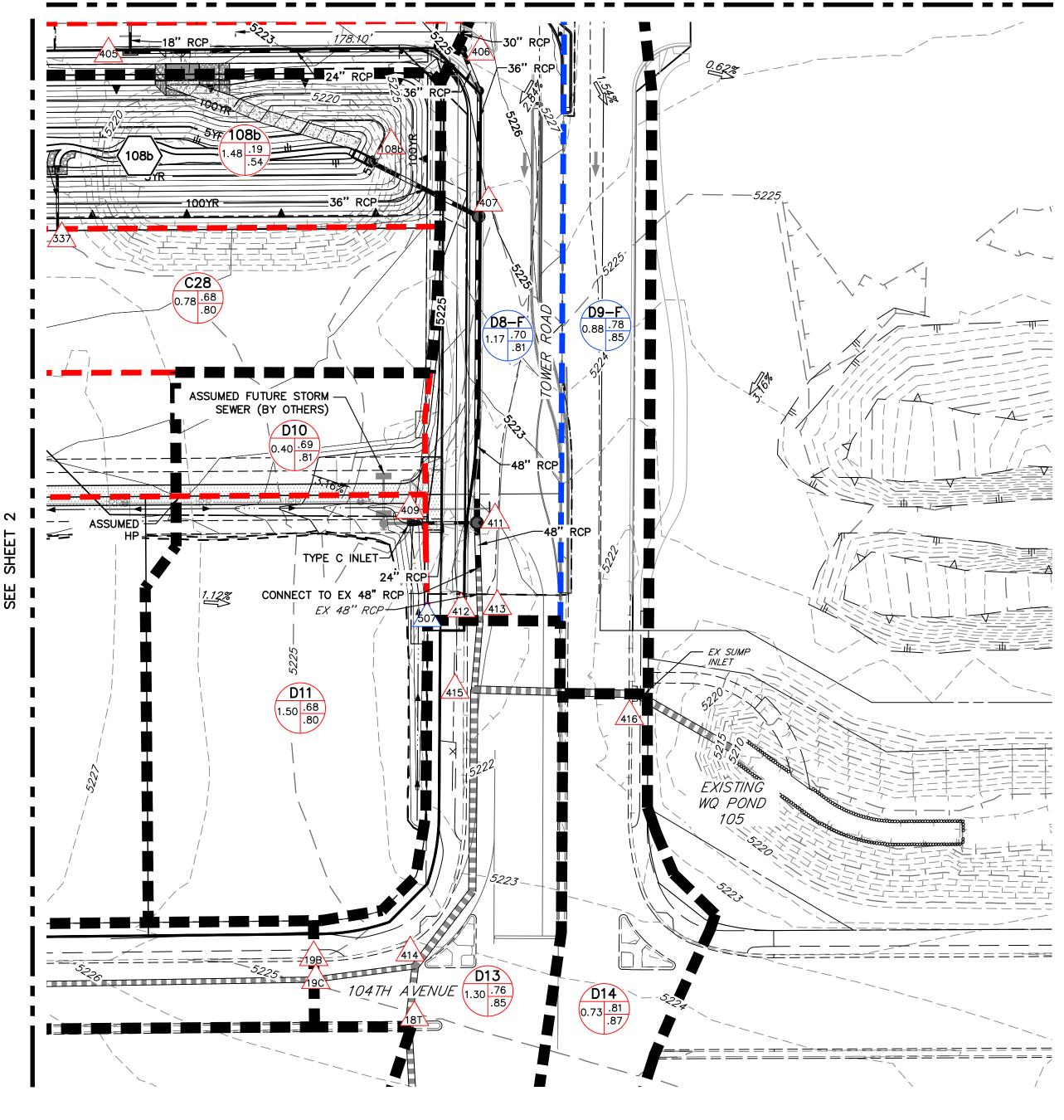


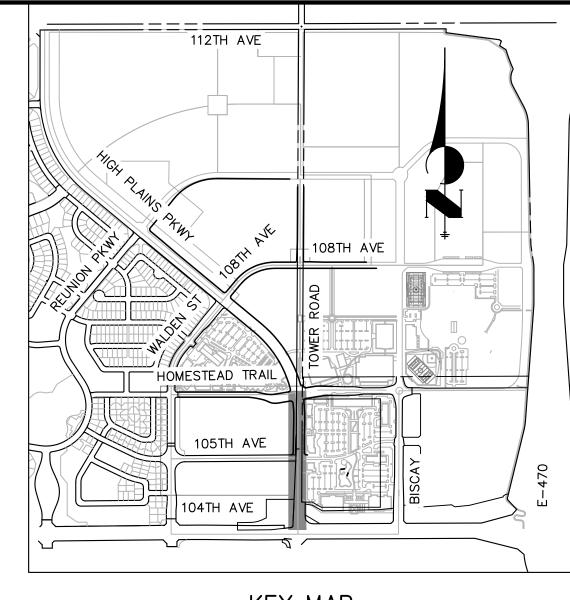


REUNION CENTER-DUET & COMMERCIAL PHASE DISTRICT IMPROVEMENTS FINAL DRAINAGE PLAN

FUTURE CONDITIONS



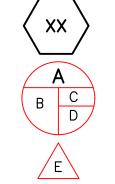




Design Point Contributing Basins Contributing Area (ac) Q ₅ (cfs) Q ₁₀₀ (cfs) 501 Sub-Basin D1-F 0.51 0.81 2.26 502 Sub-Basin D2-F 0.41 1.37 3.14 503 DP 501 and DP 502 0.92 1.98 4.96 504 Sub-Basin D3-F 0.30 0.98 2.21 505 DP 503 and DP 504 1.22 2.82 6.85 506 Sub-Basin D4-F and DP 505 1.67 0.00 0.00 402 DP 506 and DP 108a 18.36 6.41 12.16 403 Sub-Basin D5 0.52 0.68 2.31 404 Sub-Basin D6 and DP 403 0.99 1.54 4.68 405 Sub-Basin D7 and DP JD5 2.30 3.67 10.90 406 DP 402 and DP 405 20.66 9.29 20.73 108b Pond 108b detained flows 36.05 0.00 0.00 407 DP 406 and DP 108b 56.71 29.20 51.56		Existing WQ Pond 105 Ultimate Sub-Basin Design Point Summary Table					
502 Sub-Basin D2-F 0.41 1.37 3.14 503 DP 501 and DP 502 0.92 1.98 4.96 504 Sub-Basin D3-F 0.30 0.98 2.21 505 DP 503 and DP 504 1.22 2.82 6.85 506 Sub-Basin D4-F and DP 505 1.67 3.66 9.26 108a Pond 108a detained flows 16.69 0.00 0.00 402 DP 506 and DP 108a 18.36 6.41 12.16 403 Sub-Basin D5 0.52 0.68 2.31 404 Sub-Basin D6 and DP 403 0.99 1.54 4.68 405 Sub-Basin D7 and DP JD5 2.30 3.67 10.90 406 DP 402 and DP 405 20.66 9.29 20.73 108b Pond 108b detained flows 36.05 0.00 0.00 407 DP 406 and DP 108b 56.71 29.20 51.56 409 Sub-Basin D10 & D11 1.90 4.97 12.71 411	_	Contributing Basins	_	Q ₅ (cfs)	Q ₁₀₀ (cfs)		
503 DP 501 and DP 502 0.92 1.98 4.96 504 Sub-Basin D3-F 0.30 0.98 2.21 505 DP 503 and DP 504 1.22 2.82 6.85 506 Sub-Basin D4-F and DP 505 1.67 3.66 9.26 108a Pond 108a detained flows 16.69 0.00 0.00 402 DP 506 and DP 108a 18.36 6.41 12.16 403 Sub-Basin D5 0.52 0.68 2.31 404 Sub-Basin D6 and DP 403 0.99 1.54 4.68 405 Sub-Basin D7 and DP JD5 2.30 3.67 10.90 406 DP 402 and DP 405 20.66 9.29 20.73 108b Pond 108b detained flows 36.05 0.00 0.00 407 DP 406 and DP 108b 56.71 29.20 51.56 409 Sub-Basin D10 & D11 1.90 4.97 12.71 411 DP 407 and DP 409 58.61 31.80 58.22 507	501	Sub-Basin D1-F	0.51	0.81	2.26		
504 Sub-Basin D3-F 0.30 0.98 2.21 505 DP 503 and DP 504 1.22 2.82 6.85 506 Sub-Basin D4-F and DP 505 1.67 3.66 9.26 108a Pond 108a detained flows 16.69 0.00 0.00 402 DP 506 and DP 108a 18.36 6.41 12.16 403 Sub-Basin D5 0.52 0.68 2.31 404 Sub-Basin D6 and DP 403 0.99 1.54 4.68 405 Sub-Basin D6 and DP JD5 2.30 3.67 10.90 406 DP 402 and DP 405 20.66 9.29 20.73 108b Pond 108b detained flows 36.05 0.00 0.00 407 DP 406 and DP 108b 56.71 29.20 51.56 409 Sub-Basin D10 & D11 1.90 4.97 12.71 411 DP 407 and DP 409 58.61 31.80 58.22 507 Sub-Basin D8-F 1.17 2.75 6.90 413 <td>502</td> <td>Sub-Basin D2-F</td> <td>0.41</td> <td>1.37</td> <td>3.14</td>	502	Sub-Basin D2-F	0.41	1.37	3.14		
505 DP 503 and DP 504 1.22 2.82 6.85 506 Sub-Basin D4-F and DP 505 1.67 3.66 9.26 108a Pond 108a detained flows 16.69 0.00 0.00 402 DP 506 and DP 108a 18.36 6.41 12.16 403 Sub-Basin D5 0.52 0.68 2.31 404 Sub-Basin D6 and DP 403 0.99 1.54 4.68 405 Sub-Basin D7 and DP JD5 2.30 3.67 10.90 406 DP 402 and DP 405 20.66 9.29 20.73 108b Pond 108b detained flows 36.05 0.00 0.00 407 DP 406 and DP 108b 56.71 29.20 51.56 409 Sub-Basin D10 & D11 1.90 4.97 12.71 411 DP 407 and DP 409 58.61 31.80 58.22 507 Sub-Basin D8-F 1.17 2.75 6.90 413 DP JD10 and DP 8DF 59.78 31.80 66.15 <td< td=""><td>503</td><td>DP 501 and DP 502</td><td>0.92</td><td>1.98</td><td>4.96</td></td<>	503	DP 501 and DP 502	0.92	1.98	4.96		
506 Sub-Basin D4-F and DP 505 1.67 3.66 9.26 108a Pond 108a detained flows 16.69 0.00 0.00 402 DP 506 and DP 108a 18.36 6.41 12.16 403 Sub-Basin D5 0.52 0.68 2.31 404 Sub-Basin D6 and DP 403 0.99 1.54 4.68 405 Sub-Basin D7 and DP JD5 2.30 3.67 10.90 406 DP 402 and DP 405 20.66 9.29 20.73 108b Pond 108b detained flows 36.05 0.00 0.00 407 DP 406 and DP 108b 56.71 29.20 51.56 409 Sub-Basin D10 & D11 1.90 4.97 12.71 411 DP 407 and DP 409 58.61 31.80 58.22 507 Sub-Basin D8-F 1.17 2.75 6.90 413 DP JD10 and DP 8DF 59.78 31.80 66.15 19A Existing off-site flows per Tower Report 40.90 77.00 </td <td>504</td> <td>Sub-Basin D3-F</td> <td>0.30</td> <td>0.98</td> <td>2.21</td>	504	Sub-Basin D3-F	0.30	0.98	2.21		
108a Pond 108a detained flows 16.69 0.00 0.00 402 DP 506 and DP 108a 18.36 6.41 12.16 403 Sub-Basin D5 0.52 0.68 2.31 404 Sub-Basin D6 and DP 403 0.99 1.54 4.68 405 Sub-Basin D7 and DP JD5 2.30 3.67 10.90 406 DP 402 and DP 405 20.66 9.29 20.73 108b Pond 108b detained flows 36.05 0.00 0.00 407 DP 406 and DP 108b 56.71 29.20 51.56 409 Sub-Basin D10 & D11 1.90 4.97 12.71 411 DP 407 and DP 409 58.61 31.80 58.22 507 Sub-Basin D8-F 1.17 2.75 6.90 413 DP JD10 and DP 8DF 59.78 31.80 66.15 19A Existing off-site flows per Tower Report 40.90 77.00 19B Basin D12 2.07 3.68 9.57	505	DP 503 and DP 504	1.22	2.82	6.85		
402 DP 506 and DP 108a 18.36 6.41 12.16 403 Sub-Basin D5 0.52 0.68 2.31 404 Sub-Basin D6 and DP 403 0.99 1.54 4.68 405 Sub-Basin D7 and DP JD5 2.30 3.67 10.90 406 DP 402 and DP 405 20.66 9.29 20.73 108b Pond 108b detained flows 36.05 0.00 0.00 407 DP 406 and DP 108b 56.71 29.20 51.56 409 Sub-Basin D10 & D11 1.90 4.97 12.71 411 DP 407 and DP 409 58.61 31.80 58.22 507 Sub-Basin D8-F 1.17 2.75 6.90 413 DP JD10 and DP 8DF 59.78 31.80 66.15 19A Existing off-site flows per Tower Report 40.90 77.00 19B Basin D12 2.07 3.68 9.57 19C DP 19B and 19A 36.82 81.10 18T Existing Off-site flows from Biscay 61.10 114.90	506	Sub-Basin D4-F and DP 505	1.67	3.66	9.26		
403 Sub-Basin D5 0.52 0.68 2.31 404 Sub-Basin D6 and DP 403 0.99 1.54 4.68 405 Sub-Basin D7 and DP JD5 2.30 3.67 10.90 406 DP 402 and DP 405 20.66 9.29 20.73 108b Pond 108b detained flows 36.05 0.00 0.00 407 DP 406 and DP 108b 56.71 29.20 51.56 409 Sub-Basin D10 & D11 1.90 4.97 12.71 411 DP 407 and DP 409 58.61 31.80 58.22 507 Sub-Basin D8-F 1.17 2.75 6.90 413 DP JD10 and DP 8DF 59.78 31.80 66.15 19A Existing off-site flows per Tower Report 40.90 77.00 19B Basin D12 2.07 3.68 9.57 19C DP 19B and 19A 36.82 81.10 18T Existing Off-site flows from Biscay 61.10 114.90 414 Existing Offsite Flows 76.80 175.92 <td>108a</td> <td>Pond 108a detained flows</td> <td>16.69</td> <td>0.00</td> <td>0.00</td>	108a	Pond 108a detained flows	16.69	0.00	0.00		
404 Sub-Basin D6 and DP 403 0.99 1.54 4.68 405 Sub-Basin D7 and DP JD5 2.30 3.67 10.90 406 DP 402 and DP 405 20.66 9.29 20.73 108b Pond 108b detained flows 36.05 0.00 0.00 407 DP 406 and DP 108b 56.71 29.20 51.56 409 Sub-Basin D10 & D11 1.90 4.97 12.71 411 DP 407 and DP 409 58.61 31.80 58.22 507 Sub-Basin D8-F 1.17 2.75 6.90 413 DP JD10 and DP 8DF 59.78 31.80 66.15 19A Existing off-site flows per Tower Report 40.90 77.00 19B Basin D12 2.07 3.68 9.57 19C DP 19B and 19A 36.82 81.10 18T Existing off-site flows from Biscay 61.10 114.90 414 Existing Offsite Flows 76.80 175.92	402	DP 506 and DP 108a	18.36	6.41	12.16		
405 Sub-Basin D7 and DP JD5 2.30 3.67 10.90 406 DP 402 and DP 405 20.66 9.29 20.73 108b Pond 108b detained flows 36.05 0.00 0.00 407 DP 406 and DP 108b 56.71 29.20 51.56 409 Sub-Basin D10 & D11 1.90 4.97 12.71 411 DP 407 and DP 409 58.61 31.80 58.22 507 Sub-Basin D8-F 1.17 2.75 6.90 413 DP JD10 and DP 8DF 59.78 31.80 66.15 19A Existing off-site flows per Tower Report 40.90 77.00 19B Basin D12 2.07 3.68 9.57 19C DP 19B and 19A 36.82 81.10 18T Existing off-site flows from Biscay 61.10 114.90 414 Existing Offsite Flows 76.80 175.92	403	Sub-Basin D5	0.52	0.68	2.31		
406 DP 402 and DP 405 20.66 9.29 20.73 108b Pond 108b detained flows 36.05 0.00 0.00 407 DP 406 and DP 108b 56.71 29.20 51.56 409 Sub-Basin D10 & D11 1.90 4.97 12.71 411 DP 407 and DP 409 58.61 31.80 58.22 507 Sub-Basin D8-F 1.17 2.75 6.90 413 DP JD10 and DP 8DF 59.78 31.80 66.15 19A Existing off-site flows per Tower Report 40.90 77.00 19B Basin D12 2.07 3.68 9.57 19C DP 19B and 19A 36.82 81.10 18T Existing off-site flows from Biscay 61.10 114.90 414 Existing Offsite Flows 76.80 175.92	404	Sub-Basin D6 and DP 403	0.99	1.54	4.68		
108b Pond 108b detained flows 36.05 0.00 0.00 407 DP 406 and DP 108b 56.71 29.20 51.56 409 Sub-Basin D10 & D11 1.90 4.97 12.71 411 DP 407 and DP 409 58.61 31.80 58.22 507 Sub-Basin D8-F 1.17 2.75 6.90 413 DP JD10 and DP 8DF 59.78 31.80 66.15 19A Existing off-site flows per Tower Report 40.90 77.00 19B Basin D12 2.07 3.68 9.57 19C DP 19B and 19A 36.82 81.10 18T Existing off-site flows from Biscay 61.10 114.90 414 Existing Offsite Flows 76.80 175.92	405	Sub-Basin D7 and DP JD5	2.30	3.67	10.90		
407 DP 406 and DP 108b 56.71 29.20 51.56 409 Sub-Basin D10 & D11 1.90 4.97 12.71 411 DP 407 and DP 409 58.61 31.80 58.22 507 Sub-Basin D8-F 1.17 2.75 6.90 413 DP JD10 and DP 8DF 59.78 31.80 66.15 19A Existing off-site flows per Tower Report 40.90 77.00 19B Basin D12 2.07 3.68 9.57 19C DP 19B and 19A 36.82 81.10 18T Existing off-site flows from Biscay 61.10 114.90 414 Existing Offsite Flows 76.80 175.92	406	DP 402 and DP 405	20.66	9.29	20.73		
409 Sub-Basin D10 & D11 1.90 4.97 12.71 411 DP 407 and DP 409 58.61 31.80 58.22 507 Sub-Basin D8-F 1.17 2.75 6.90 413 DP JD10 and DP 8DF 59.78 31.80 66.15 19A Existing off-site flows per Tower Report 40.90 77.00 19B Basin D12 2.07 3.68 9.57 19C DP 19B and 19A 36.82 81.10 18T Existing off-site flows from Biscay 61.10 114.90 414 Existing Offsite Flows 76.80 175.92	108b	Pond 108b detained flows	36.05	0.00	0.00		
411 DP 407 and DP 409 58.61 31.80 58.22 507 Sub-Basin D8-F 1.17 2.75 6.90 413 DP JD10 and DP 8DF 59.78 31.80 66.15 19A Existing off-site flows per Tower Report 40.90 77.00 19B Basin D12 2.07 3.68 9.57 19C DP 19B and 19A 36.82 81.10 18T Existing off-site flows from Biscay 61.10 114.90 414 Existing Offsite Flows 76.80 175.92	407	DP 406 and DP 108b	56.71	29.20	51.56		
507 Sub-Basin D8-F 1.17 2.75 6.90 413 DP JD10 and DP 8DF 59.78 31.80 66.15 19A Existing off-site flows per Tower Report 40.90 77.00 19B Basin D12 2.07 3.68 9.57 19C DP 19B and 19A 36.82 81.10 18T Existing off-site flows from Biscay 61.10 114.90 414 Existing Offsite Flows 76.80 175.92	409	Sub-Basin D10 & D11	1.90	4.97	12.71		
413 DP JD10 and DP 8DF 59.78 31.80 66.15 19A Existing off-site flows per Tower Report 40.90 77.00 19B Basin D12 2.07 3.68 9.57 19C DP 19B and 19A 36.82 81.10 18T Existing off-site flows from Biscay 61.10 114.90 414 Existing Offsite Flows 76.80 175.92	411	DP 407 and DP 409	58.61	31.80	58.22		
19A Existing off-site flows per Tower Report 40.90 77.00 19B Basin D12 2.07 3.68 9.57 19C DP 19B and 19A 36.82 81.10 18T Existing off-site flows from Biscay 61.10 114.90 414 Existing Offsite Flows 76.80 175.92	507	Sub-Basin D8-F	1.17	2.75	6.90		
19B Basin D12 2.07 3.68 9.57 19C DP 19B and 19A 36.82 81.10 18T Existing off-site flows from Biscay 61.10 114.90 414 Existing Offsite Flows 76.80 175.92	413	DP JD10 and DP 8DF	59.78	31.80	66.15		
19C DP 19B and 19A 36.82 81.10 18T Existing off-site flows from Biscay 61.10 114.90 414 Existing Offsite Flows 76.80 175.92	19A	Existing off-site flows per Tower Report		40.90	77.00		
18T Existing off-site flows from Biscay 61.10 114.90 414 Existing Offsite Flows 76.80 175.92	19B	Basin D12	2.07	3.68	9.57		
414 Existing Offsite Flows 76.80 175.92	19C	DP 19B and 19A		36.82	81.10		
· · · · · · · · · · · · · · · · · · ·	18T	Existing off-site flows from Biscay		61.10	114.90		
415 DP 413 and DP 414 101.69 221.50	414			76.80	175.92		
	415	DP 413 and DP 414		101.69	221.50		

Sub-Basin D9-F and DP 415





PROPOSED BASIN LABEL A. BASIN DESIGNATION

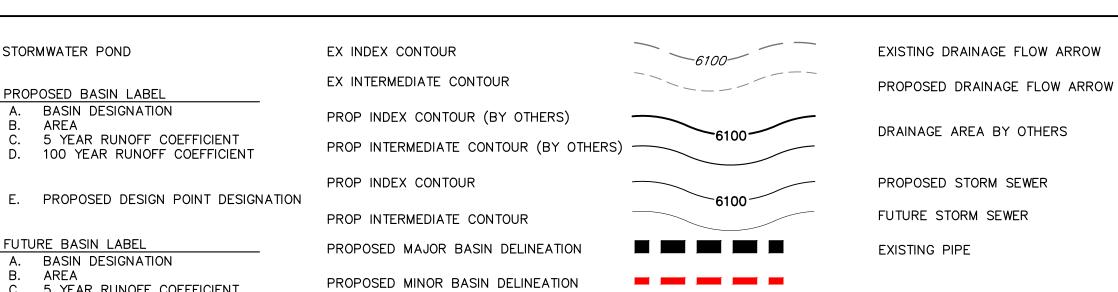
STORMWATER POND

D. 100 YEAR RUNOFF COEFFICIENT

C. 5 YEAR RUNOFF COEFFICIENT

FUTURE BASIN LABEL A. BASIN DESIGNATION C. 5 YEAR RUNOFF COEFFICIENT D. 100 YEAR RUNOFF COEFFICIENT

E. FUTURE DESIGN POINT DESIGNATION



INTERIM DRAINAGE BASIN BOUNDARY

FUTURE DRAINAGE BASIN BOUNDARY

Pond	Tributary Area (ac)	%
108a	16.69	
108b	40.86	

ENGINEER'S STATEMENT
PRELIMINARY NOT FOR
AARON LEE CLO CONSTRUCTION COLORADO NO. 30 FOR AND ON BEHALF OF JR ENGINEERING.

0.401 1.882

0.587 3.889

3.44

7.94



ORIGINAL SCALE: 1" = 60'

Pond Release Rate

5.5

FUTURE ULTIMATE CONDITIONS DRAINAGE MAP REUNION CENTER DUETS JOB NO. 14421.49 9/15/23 SHEET 3 OF 3

103.73 226.93



Centennial 303-740-9393 • Colorado Springs 719-593-2593 Fort Collins 970-491-9888 • www.jrengineering.com

Pond Tributary Areas

Subdivision: Reunion Center Commerce City Location:

Project Name: Reunion Duets

Project No.: 14421.49

By: WJL

Checked By: KAU Date: 11/28/23

Detention Pond 108a

Conceptual Pond Stage-Storage-Discharge from UD-Detention 4.06

Pond Imperviousness = 65.7%

Pond Acreage = 16.69

Detention Pond 108a Stage-Storage Table								
Elev	Stage	Area	Area	Cumulativ	/e Volume	Total Outflow		
Elev	(ft)	(sq ft)	(Acre)	(cubic ft)	(ac-ft)	(cfs)		
5214.58	0.00	0	0.000	0	0.000	0.00		
5214.75	0.17	53	0.001	4	0.000	0.11		
5215.00	0.42	213	0.005	37	0.001	0.59		
5216.00	1.42	3,848	0.088	2,084	0.048	3.42		
5217.00	2.42	8,328	0.191	8,187	0.188	4.59		
5218.00	3.42	10,010	0.230	17,361	0.399	5.52		
5-YR WSEL: 5218.02	3.44	10,051	0.231	17,562	0.403	5.53		
5219.00	4.42	11,786	0.271	28,265	0.649	6.31		
5220.00	5.42	13,662	0.314	40,995	0.941	7.01		
5221.00	6.42	15,649	0.359	55,657	1.278	7.65		
5222.00	7.42	17,735	0.407	72,356	1.661	8.24		
100-YR WSEL: 5222.52	7.94	19,218	0.441	81,966	1.882	8.53		
SPILLWAY CREST: 5223.00	8.42	20,578	0.472	91,517	2.101	8.79		
5224.00	9.42	21,876	0.502	112,746	2.588	9.31		
5225.00	10.42	24,187	0.555	135,786	3.117	9.80		

Detention Pond 108b
Conceptual Pond Stage-Storage-Discharge from UD-Detention 4.06

Pond Imperviousness= Pond Acreage= 66.5% 40.86

Detention Pond 108b Stage-Storage Table								
Elev	Stage	Area	Area	Cumulative Volume		Total Outflow		
Liev	[ft]	(sq ft)	(Acre)	(cubic ft)	(ac-ft)	Total Outflow		
5213.33	0.00	0	0.000	0	0.000	0.00		
5213.50	0.17	55	0.001	5	0.000	0.21		
5214.00	0.67	455	0.010	134	0.003	2.51		
5215.00	1.67	3,624	0.083	2,186	0.050	12.31		
5216.00	2.67	10,248	0.235	9,148	0.210	16.89		
5217.00	3.67	16,223	0.372	22,407	0.514	20.47		
5-YR WSEL: 5217.19	3.86	17,025	0.391	25,567	0.587	21.08		
5218.00	4.67	20,358	0.467	40,714	0.935	23.51		
5219.00	5.67	24,941	0.573	63,382	1.455	26.20		
5220.00	6.67	29,368	0.674	90,554	2.079	28.64		
5221.00	7.67	33,891	0.778	122,201	2.805	30.89		
5222.00	8.67	38,502	0.884	158,416	3.637	32.98		
100-YR WSEL: 5222.30	8.97	39,958	0.917	170,188	3.907	33.59		
SPILLWAY CREST: 5222.28	8.95	39,814	0.914	168,991	3.879	33.53		
5224.00	10.67	49,810	1.143	245,909	5.645	36.82		
5225.00	11.67	55,019	1.263	298,344	6.849	38.59		

Detention Pond Parameters Summary Table									
Stored Volume Stage Pond Release Rate							te		
Pond	Tributary Area	% Impervious	V_5	V ₁₀₀	d_5	d ₁₀₀	Q_5	Q ₁₀₀	
	(ac)		(ac-ft)	(ac-ft)	(ft)	(ft)	(cfs)	(cfs)	
108a	16.69	65.7%	0.401	1.882	3.44	7.94	5.5	8.5	
108b	40.86	66.5%	0.587	3.889	3.86	8.95	21.1	33.6	

Detention Pond Tributary Areas

Subdivision: Reunion Center
Location: Commerce City

Reunion Center
Project Name: Project No.: 14421.49
Calculated By: Checked By: Checked By: Date: 11728/23

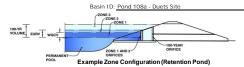
Basin	Area (ac)	% Imp.
Off-Site Sub-Basins Total	1.92	73.6%
Proposed Detention Pond 108a Sub-Basins Total	16.69	65.7%
Proposed Detention Pond 108b Sub-Basins Total	40.86	66.5%
Total	59.46	70.0%

WQCV Drain Time (hr):	40
Coefficient, a (Table 3-2):	1.0
WQCV (in):	0.28
Updated WQCV (ac-ft) per this report:	1.363
Per the Preliminary Drainage Report for Reunion Center – Village 1 WQCV (ac-ft):	1.431

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)

Project: Reunion Duets Developme



Watershed Information	Flood Control Only		
Selected BMP Type =	No BMP		
Watershed Area =	16.69	acres	
Watershed Length =	900	ft	
Watershed Length to Centroid =	350	ft	
Watershed Slope =	0.03	ft/ft	
Watershed Imperviousness =	65.7%	percent	
Percentage Hydrologic Soil Group A =	0.0%	percent	
Percentage Hydrologic Soil Group B =	100.0%	percent	

Percentage Hydrologic Soil Groups C/D = 100.0% percent
Target WCCV Drain Time = N/A hours

Location for 1-hr Rainfall Depths = Commerce City - Civic Center

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Uthan Hydroraph' Procedure.

the embedded Colorado Urban Hydro	igraph Procedu	re.
Water Quality Capture Volume (WQCV) =	0.357	acre-feet
Excess Urban Runoff Volume (EURV) =	1.199	acre-feet
2-yr Runoff Volume (P1 = 0.84 in.) =	0.666	acre-feet
5-yr Runoff Volume (P1 = 1.12 in.) =	0.941	acre-feet
10-yr Runoff Volume (P1 = 1.37 in.) =	1.240	acre-feet
25-yr Runoff Volume (P1 = 1.75 in.) =	1.787	acre-feet
50-yr Runoff Volume (P1 = 2.08 in.) =	2.227	acre-feet
100-yr Runoff Volume (P1 = 2.43 in.) =	2.741	acre-feet
500-yr Runoff Volume (P1 = 3.35 in.) =	4.011	acre-feet
Approximate 2-yr Detention Volume =	0.658	acre-feet
Approximate 5-yr Detention Volume =	0.931	acre-feet
Approximate 10-yr Detention Volume =	1.242	acre-feet
Approximate 25-yr Detention Volume =	1.495	acre-feet
Approximate 50-yr Detention Volume =	1.644	acre-feet
Approximate 100-yr Detention Volume =	1.851	acre-feet

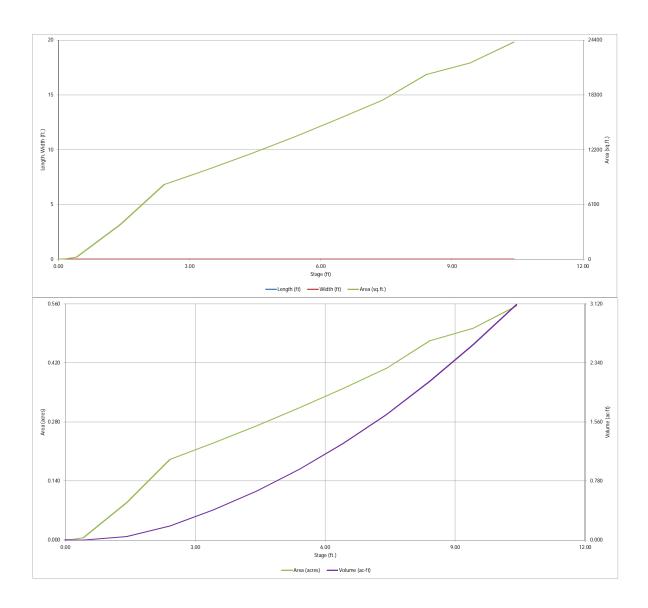
	Optional User Overrides							
et		acre-feet						
et		acre-feet						
et		inches						
et		inches						
et		inches						
et		inches						
et		inches						
et		inches						
et		inches						

Define Zones and Basin Geometry

Define Zones and Basin Geometry		
Zone 1 Volume (5-year) =	0.931	acre-fe
Zone 2 Volume (100-year - Zone 1) =	0.921	acre-fe
Select Zone 3 Storage Volume (Optional) =		acre-fe
Total Detention Basin Volume =	1.851	acre-fe
Initial Surcharge Volume (ISV) =	N/A	ft 3
Initial Surcharge Depth (ISD) =	N/A	ft
Total Available Detention Depth (H _{total}) =	user	ft
Depth of Trickle Channel (H _{TC}) =	user	ft
Slope of Trickle Channel (S _{TC}) =	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R _{L/W}) =	user	

Initial Surcharge Area (A _{ISV}) =	user	ft ²
Surcharge Volume Length (L _{ISV}) =	user	ft
Surcharge Volume Width (W _{ISV}) =	user	ft
Depth of Basin Floor (H_{FLOOR}) =	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor (A _{FLOOR}) =		ft ²
Volume of Basin Floor (V _{FLOOR}) =	user	ft ³
Depth of Main Basin (H _{MAIN}) =	user	ft
Length of Main Basin (L_{MAIN}) =	user	ft
Width of Main Basin (W _{MAIN}) =	user	ft
Area of Main Basin (A _{MAIN}) =		ft ²
Volume of Main Basin (V _{MAIN}) =	user	ft ³
Calculated Total Basin Volume (V_{total}) =	user	acre-feet

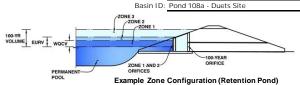
Depth Increment =	1.00	ft Optional		1	1	Optional		1	1
Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume
Description	(ft)	Stage (ft)	(ft)	(ft)	(ft 2)	Area (ft 2)	(acre)	(ft 3)	(ac-ft)
Media Surface		0.00				0	0.000		
5214.75		0.17				55	0.001	4	0.000
5215		0.42				217	0.005	37	0.001
5216		1.42				3,848	0.088	2,045	0.047
5217		2.42				8,328	0.191	8,103	0.186
5218 5219		3.42 4.42				10,010 11,786	0.230	17,261 28,147	0.396 0.646
5220		5.42				13,662	0.271	40,859	0.938
5220		6.42				15,649	0.359	55,501	1.274
5222		7.42				17,735	0.407	72,179	1.657
5223		8.42				20,578	0.472	91,517	2.101
5224		9.42				21,876	0.502	112,528	2.583
5225		10.42	-			24,187	0.555	135,544	3.112
									-
			-						
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			-						
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			-						



DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022,

Project: Reunion Duets Development



	Estimated	Estimated	
_	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (5-year)	5.39	0.931	Circular Orifice
Zone 2 (100-year)	7.88	0.921	Weir&Pipe (Restrict)
Zone 3			
•	Total (all zones)	1.851	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

ft (distance below the filtration media surface) Underdrain Orifice Invert Depth = N/A Underdrain Orifice Diameter = N/A

	Calculated Parameters for Underdrain			
Underdrain Orifice Area =	N/A	ft ²		
Underdrain Orifice Centroid =	N/A	feet		

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice = N/A ft (relative to basin bottom at Stage = 0 ft) Depth at top of Zone using Orifice Plate : N/A ft (relative to basin bottom at Stage = 0 ft) Orifice Plate: Orifice Vertical Spacing N/A inches Orifice Plate: Orifice Area per Row = N/A sq. inches

	Calculated Paramete	ers for Plate
WQ Orifice Area per Row =	N/A	ft ²
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft ²
•		

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (optional)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	N/A							
Orifice Area (sq. inches)	N/A							

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Orifice Area (sq. inches)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 1 Circular	Not Selected	
Invert of Vertical Orifice =	0.00		ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	5.60		ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	14.00		inches

	Calculated Parameters for Vertical Orifice					
	Zone 1 Circular	Not Selected				
Vertical Orifice Area =	1.07		ft ²			
Vertical Orifice Centroid =	0.58		feet			
•						

Calculated Parameters for Overflow Weir

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

	Zone 2 Weir	Not Selected		Zone 2 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	4.00		ft (relative to basin bottom at Stage = 0 ft) $\frac{1}{2}$ Height of Grate Upper Edge, $\frac{1}{2}$ Height of Grate Upper Edge, $\frac{1}{2}$	5.25		feet
Overflow Weir Front Edge Length =	5.00		feet Overflow Weir Slope Length =	5.15		feet
Overflow Weir Grate Slope =	4.00		H:V Grate Open Area / 100-yr Orifice Area =	28.22		
Horiz. Length of Weir Sides =	5.00		feet Overflow Grate Open Area w/o Debris =	17.94		ft ²
Overflow Grate Type =	Type C Grate		Overflow Grate Open Area w/ Debris =	8.97		ft ²
Debris Clogging % =	50%		%		•	

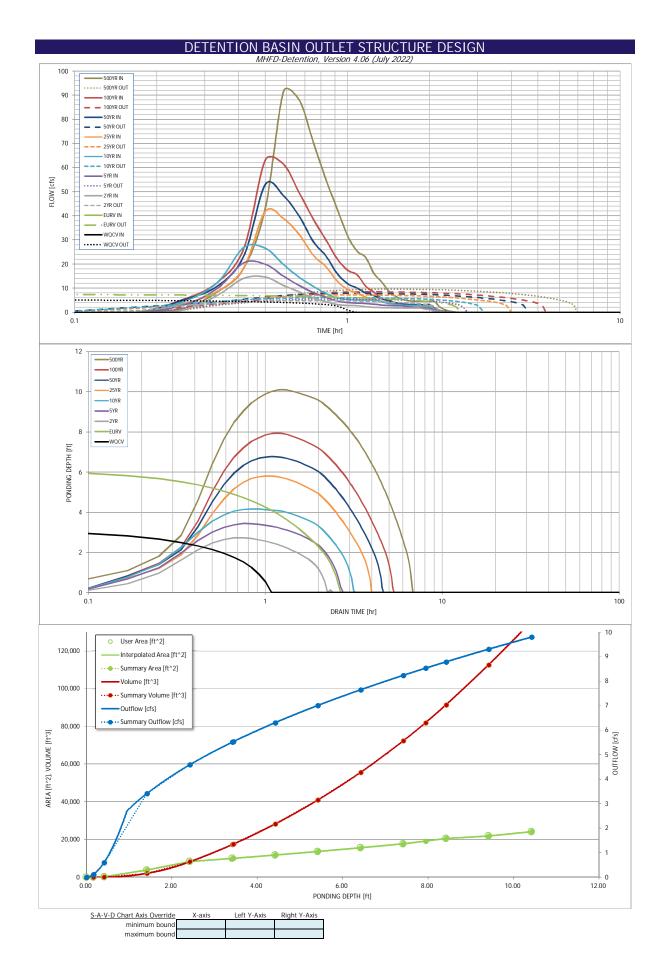
Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice) Calci					Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate				
	Zone 2 Restrictor	Not Selected			Zone 2 Restrictor	Not Selected			
Depth to Invert of Outlet Pipe =	0.17		ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	0.64		ft ²		
Outlet Pipe Diameter =	18.00		inches	Outlet Orifice Centroid =	0.34		feet		
Restrictor Plate Height Above Pipe Invert =	7.00		inches Half-Central Ang	gle of Restrictor Plate on Pipe =	1.35	N/A	radians		

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage=	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	feet
Spillway End Slopes =	H:V
Freeboard above Max Water Surface =	feet

	Calculated Paramete	ers for Spillway
Spillway Design Flow Depth=		feet
Stage at Top of Freeboard =		feet
Basin Area at Top of Freeboard =		acres
Basin Volume at Top of Freeboard =		acre-ft

Routed Hydrograph Results 500 Year Design Storm Return Period WOCV FURV 2 Year 10 Year 50 Yea 100 Yea One-Hour Rainfall Depth (in) N/A N/A 0.84 1.12 1.37 1.75 2.08 2.43 3.35 CUHP Runoff Volume (acre-ft) 0.357 1.199 0.666 1.787 2.227 2.741 4.011 Inflow Hydrograph Volume (acre-ft) N/A N/A 0.666 0.941 1.240 1.787 2.227 2.741 4.011 CUHP Predevelopment Peak Q (cfs) N/A N/A 0.2 0.5 4.7 14.9 21.3 29.2 47.1 OPTIONAL Override Predevelopment Peak Q (cfs) N/A N/A Predevelopment Unit Peak Flow, q (cfs/acre) N/A N/A 0.01 0.89 0.03 0.28 1.28 1.75 2.82 Peak Inflow Q (cfs) N/A N/A 14.6 20.6 41.9 91.7 Peak Outflow Q (cfs) 7.5 4.9 6.1 7.3 7.9 8.53 9.6 N/A 0.5 Ratio Peak Outflow to Predevelopment Q N/A N/A 10.5 0.4 0.3 0.2 Structure Controlling Flow Outlet Plate 1 Outlet Plate 1 Outlet Plate Outlet Plate 1 Outlet Plate 1 Outlet Plate Outlet Plate 1 Outlet Plate 1 Outlet Plate 1 Max Velocity through Grate 1 (fps) N/A -0.26 N/A N/A -0.2 -0.3 -0.3 -0.3 Max Velocity through Grate 2 (fps) N/A N/A N/A N/A N/A N/A N/A N/A N/A Time to Drain 97% of Inflow Volume (hours) 6 Time to Drain 99% of Inflow Volume (hours) Maximum Ponding Depth (ft) 3 24 6.20 2 74 3 44 4 17 5.80 6 77 7.94 10 11 Area at Maximum Ponding Depth (acres) 0.22 0.35 0.20 0.23 0.26 0.33 0.38 0.44 0.54 Maximum Volume Stored (acre-ft)



DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
	0:00:00									
5.00 min	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:15:00	0.00	0.00	0.00 1.02	0.00 2.98	0.00 4.41	0.00 3.49	0.00 5.08	0.00 5.34	1.67 8.46
	0:20:00	0.00	0.00	7.07	9.95	12.40	8.73	10.88	12.40	18.36
	0:25:00	0.00	0.00	14.13	20.59	26.89	18.49	23.35	26.49	43.39
	0:30:00	0.00	0.00	14.62	19.91	26.57	41.89	53.05	63.20	91.71
	0:35:00	0.00	0.00	11.11	14.98	19.76	38.85	48.30	61.39	87.92
	0:40:00	0.00	0.00	8.49	11.09	14.45	32.13	39.70	49.38	70.44
	0:45:00	0.00	0.00	5.98	8.21	10.79	23.67	29.25	38.62	55.19
	0:50:00	0.00	0.00	4.33	6.27	7.83	18.95	23.42	30.06	42.94
	0:55:00	0.00	0.00	3.30	4.67	6.02	12.95	16.09	22.24	31.88
	1:00:00	0.00	0.00	2.89	4.04	5.33	9.51	11.92	17.56	25.43
	1:10:00	0.00	0.00	2.75	3.80	5.13 5.06	7.97 6.36	10.09 7.97	15.62 10.86	22.76 16.14
	1:15:00	0.00	0.00	2.08	3.38	5.05	5.55	6.90	8.39	12.71
	1:20:00	0.00	0.00	1.95	3.04	4.46	4.48	5.55	5.84	8.77
	1:25:00	0.00	0.00	1.87	2.85	3.71	3.96	4.89	4.50	6.69
	1:30:00	0.00	0.00	1.83	2.75	3.28	3.30	4.01	3.68	5.43
	1:35:00	0.00	0.00	1.81	2.69	3.03	2.95	3.56	3.31	4.85
	1:40:00	0.00	0.00	1.81	2.27	2.89	2.77	3.32	3.18	4.63
	1:45:00	0.00	0.00	1.81	2.06	2.81	2.68	3.20	3.13	4.55
	1:50:00	0.00	0.00	1.81	1.93	2.80	2.65	3.15	3.13	4.55
	1:55:00	0.00	0.00	1.40	1.86	2.66	2.63	3.13	3.13	4.55
	2:05:00	0.00	0.00	1.18 0.64	0.93	1.27	2.63 1.43	3.13 1.70	3.13 1.70	4.55 2.47
	2:10:00	0.00	0.00	0.34	0.51	0.68	0.79	0.93	0.93	1.35
	2:15:00	0.00	0.00	0.16	0.26	0.34	0.40	0.47	0.47	0.68
	2:20:00	0.00	0.00	0.07	0.12	0.15	0.18	0.22	0.21	0.31
	2:25:00	0.00	0.00	0.02	0.03	0.04	0.05	0.06	0.06	0.08
	2:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00 3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00 4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00 4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00 5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00 5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00 5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)

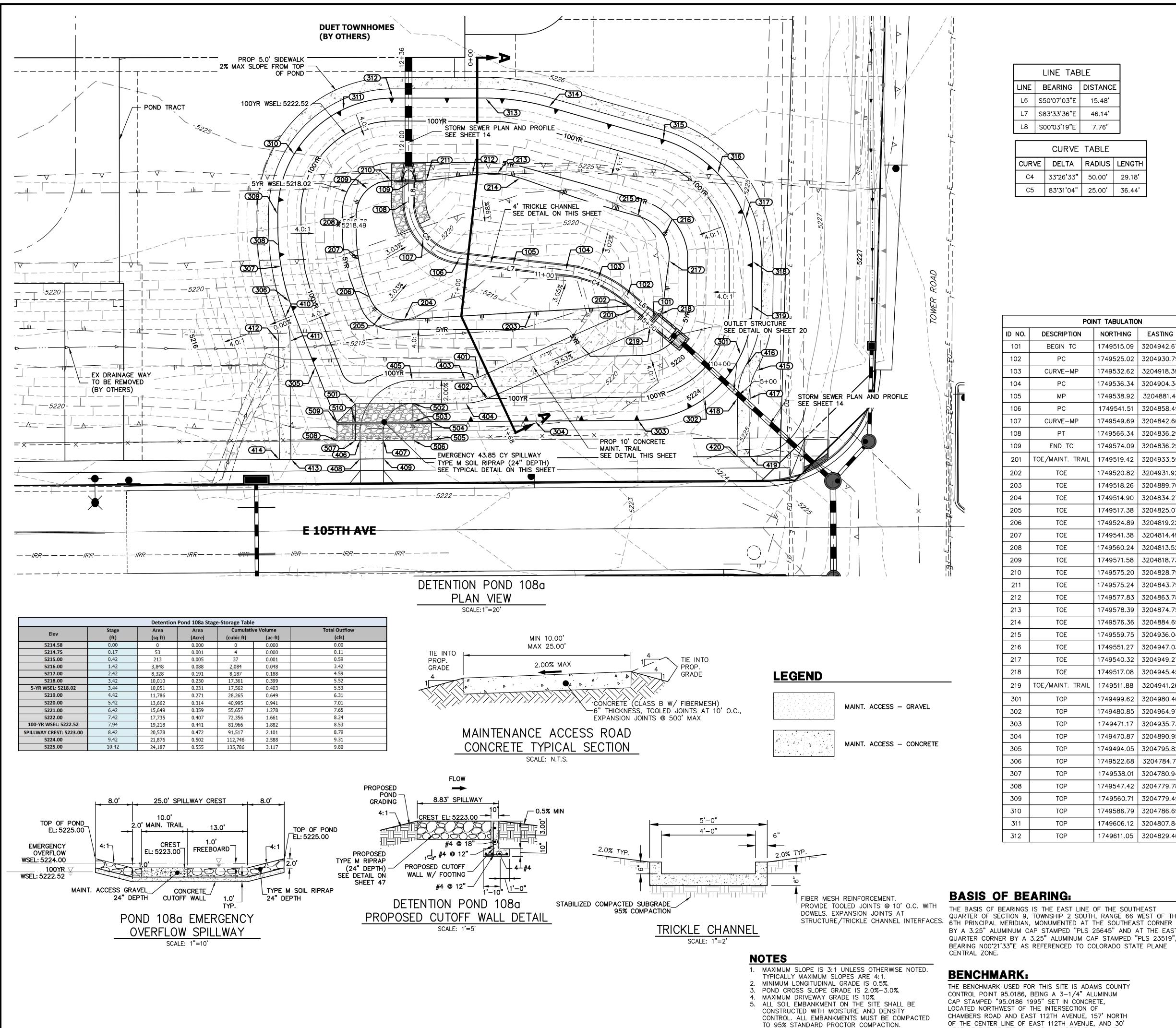
Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

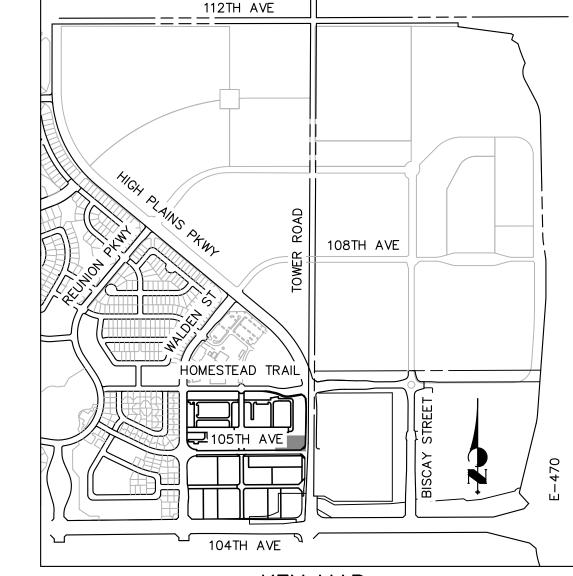
Stage - Storage	Stage	Area	Area	Volume	Volume	Total Outflow	
Description	[ft]	[ft²]	[acres]	[ft 3]	[ac-ft]	[cfs]	
			0.000				╄
5214.58	0.00	0		0	0.000	0.00	Fo
5214.75	0.17	53	0.001	4	0.000	0.11	sta
5215.00	0.42	213	0.005	37	0.001	0.59	ch
5216.00	1.42	3,848	0.088	2,084	0.048	3.42	fro Sh
5217.00	2.42	8,328	0.191	8,187	0.188	4.59	7
5218.00	3.42	10,010	0.230	17,361	0.399	5.52	Als
5-YR WSEL: 5218.02	3.44	10,051	0.231	17,562	0.403	5.53	ou
5219.00	4.42	11,786	0.271	28,265	0.649	6.31	ov
5220.00	5.42	13,662	0.314	40,995	0.941	7.01	wh
		15,649	0.359	55,657	1.278	7.65	H
5221.00	6.42		0.407	72,356		8.24	-
5222.00	7.42	17,735			1.661		-
100-YR WSEL: 5222.52	7.94	19,218	0.441	81,966	1.882	8.53	-
SPILLWAY CREST: 5223.00	8.42	20,578	0.472	91,517	2.101	8.79	4
5224.00	9.42	21,876	0.502	112,746	2.588	9.31	4
5225.00	10.42	24,187	0.555	135,786	3.117	9.80	4
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For best results, include the stages of all grade slope changes (e.g. ISV and Floor) from the S-A-V table on Sheet 'Basin'.

Also include the inverts of all outlets (e.g. vertical orifice, overflow grate, and spillway, where applicable).



CURVE TABLE					
CURVE	DELTA	RADIUS	LENGTH		
C4	33 ° 26'33"	50.00'	29.18'		
C5	83°31'04"	25.00'	36.44'		



KEY MAP SCALE: 1"=1000'

	POII	NT TABULATIO	N	
ID NO.	DESCRIPTION	NORTHING	EASTING	ELEVATION
101	BEGIN TC	1749515.09	3204942.67	5214.75
102	PC	1749525.02	3204930.79	5214.83
103	CURVE-MP	1749532.62	3204918.39	5214.90
104	PC	1749536.34	3204904.34	5214.97
105	MP	1749538.92	3204881.41	5215.09
106	PC	1749541.51	3204858.49	5215.20
107	CURVE-MP	1749549.69	3204842.66	5215.29
108	PT	1749566.34	3204836.29	5215.38
109	END TC	1749574.09	3204836.29	5215.42
201	TOE/MAINT. TRAIL	1749519.42	3204933.59	5215.30
202	TOE	1749520.82	3204931.92	5215.31
203	TOE	1749518.26	3204889.70	5216.05
204	TOE	1749514.90	3204834.27	5216.67
205	TOE	1749517.38	3204825.07	5216.76
206	TOE	1749524.89	3204819.22	5216.74
207	TOE	1749541.38	3204814.49	5216.60
208	TOE	1749560.24	3204813.52	5216.49
209	TOE	1749571.58	3204818.73	5216.36
210	TOE	1749575.20	3204828.79	5216.08
211	TOE	1749575.24	3204843.79	5216.07
212	TOE	1749577.83	3204863.78	5216.78
213	TOE	1749578.39	3204874.75	5216.95
214	TOE	1749576.36	3204884.69	5216.94
215	TOE	1749559.75	3204936.04	5216.77
216	TOE	1749551.27	3204947.03	5216.65
217	TOE	1749540.32	3204949.27	5216.22
218	TOE	1749517.08	3204945.45	5215.27
219	TOE/MAINT. TRAIL	1749511.88	3204941.26	5215.27
301	TOP	1749499.62	3204980.46	5225.00
302	TOP	1749480.85	3204964.97	5225.00
303	TOP	1749471.17	3204935.73	5225.00
304	TOP	1749470.87	3204890.95	5225.00
305	TOP	1749494.05	3204795.82	5225.00
306	TOP	1749522.68	3204784.71	5225.00
307	TOP	1749538.01	3204780.94	5225.00
308	TOP	1749547.42	3204779.78	5225.00
309	TOP	1749560.71	3204779.49	5225.00
310	TOP	1749586.79	3204786.69	5225.00
311	TOP	1749606.12	3204807.84	5225.00
312	TOP	1749611.05	3204829.46	5225.00

POINT TABULATION						
ID NO.	DESCRIPTION	NORTHING	EASTING	ELEVATION		
313	TOP	1749611.07	3204869.48	5225.00		
314	TOP	1749607.22	3204897.04	5225.00		
315	TOP	1749593.02	3204946.66	5225.00		
316	TOP	1749578.38	3204970.34	5225.00		
317	TOP	1749558.51	3204982.46	5225.00		
318	TOP	1749540.09	3204985.52	5225.00		
319	TOP	1749520.86	3204985.40	5225.00		
401	MAINT. TRAIL	1749489.95	3204866.82	5222.36		
402	MAINT. TRAIL	1749480.80	3204870.85	5222.48		
403	MAINT. TRAIL	1749488.67	3204861.07	5222.80		
404	MAINT. TRAIL	1749478.67	3204860.93	5223.00		
405	MAINT. TRAIL	1749488.52	3204838.04	5222.80		
406	MAINT. TRAIL /SPILLWAY CREST	1749462.36	3204815.22	5222.95		
407	SPILLWAY CREST/ MAINT. TRAIL	1749462.43	3204825.22	5222.96		
408	MAINT. TRAIL	1749454.36	3204815.27	5222.78		
409	MAINT. TRAIL	1749454.43	3204825.27	5222.86		
410	SW-PC	1749516.35	3204782.76	5225.00		
411	SW-PT	1749505.57	3204784.84	5224.71		
412	SW-PT	1749505.54	3204779.84	5224.70		
413	MATCH SW	1749454.16	3204785.18	5222.65		
414	MATCH SW	1749454.13	3204780.23	5222.64		
415	SW-PC	1749492.75	3204987.10	5226.10		
416	SW-PC	1749495.16	3204982.72	5226.00		
417	SW-PT	1749480.54	3204984.01	5225.70		
418	SW-PT	1749480.51	3204979.01	5225.50		
419	MATCH SW	1749455.49	3204984.18	5225.07		
420	MATCH SW	1749455.46	3204979.23	5225.00		
501	SPILLWAY CREST	1749478.35	3204813.11	5223.00		
502	SPILLWAY CREST /MAINT. TRAIL	1749478.52	3204838.11	5223.00		
503	SPILLWAY CREST	1749470.52	3204838.17	5223.00		
504	SPILLWAY/TOP	1749470.37	3204846.17	5225.00		
505	SPILLWAY	1749462.57	3204846.22	5223.22		
506	SPILLWAY CREST	1749462.52	3204838.22	5222.99		
507	SPILLWAY CREST	1749462.35	3204813.22	5222.94		
508	SPILLWAY	1749462.30	3204805.22	5224.21		
509	SPILLWAY/TOP	1749470.29	3204805.17	5225.00		
510	SPILLWAY CREST	1749470.35	3204813.17	5223.00		

THE BASIS OF BEARINGS IS THE EAST LINE OF THE SOUTHEAST QUARTER OF SECTION 9, TOWNSHIP 2 SOUTH, RANGE 66 WEST OF THE BY A 3.25" ALUMINUM CAP STAMPED "PLS 25645" AND AT THE EAST QUARTER CORNER BY A 3.25" ALUMINUM CAP STAMPED "PLS 23519",

WEST OF THE CENTER LINE OF CHAMBERS ROAD, WITH AN ELEVATION OF 5143.89 (NAVD 1988 USFT).

6. PROVIDE JOINTS AT TEN FEET ON CENTER ALONG

CONCRETE TRICKLE CHANNEL



Know what's below.

Call before you dig.

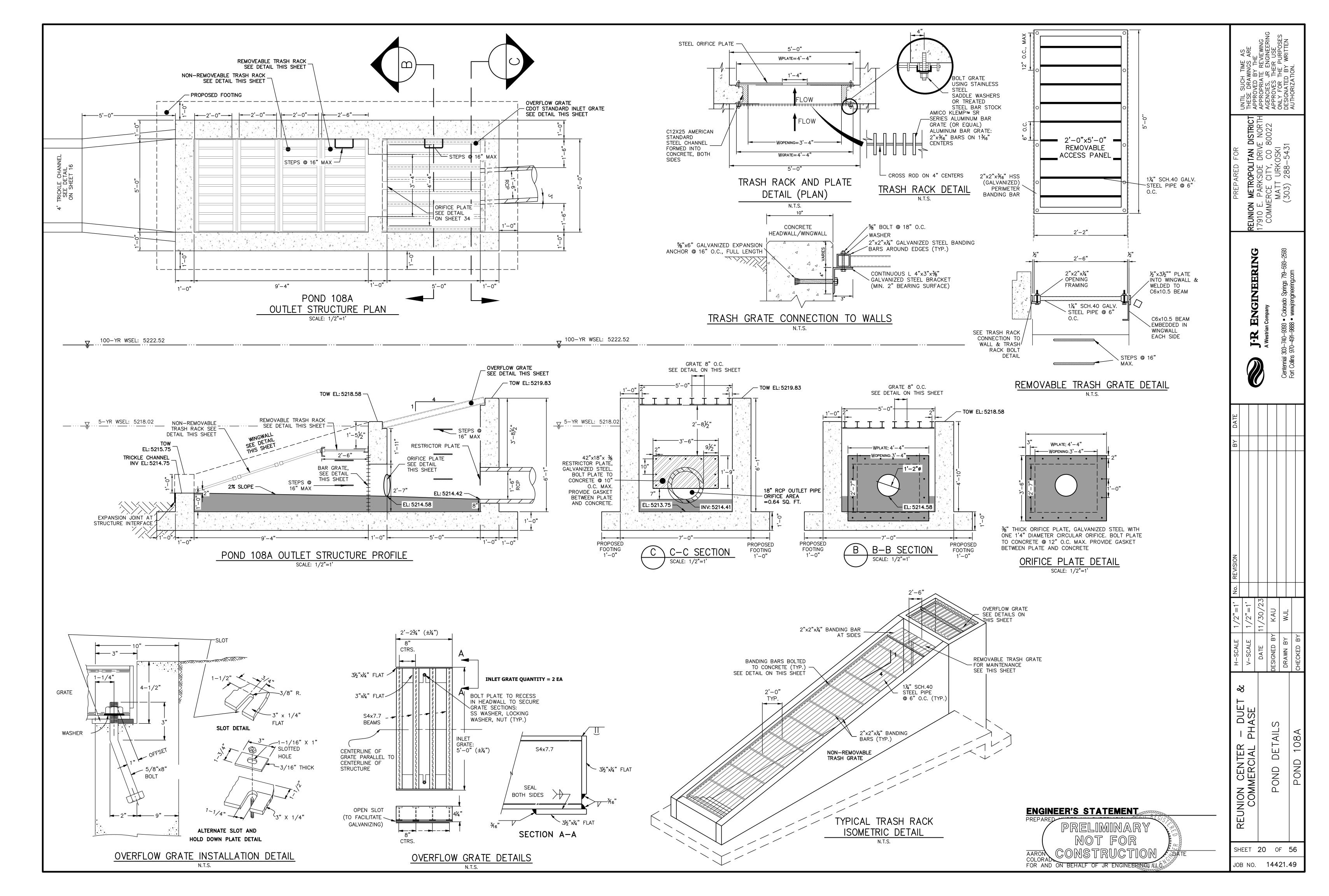
FOR AND ON BEHALF OF JR ENGINEERING!

ORIGINAL SCALE: 1" = 20'

SHEET 16 OF 56

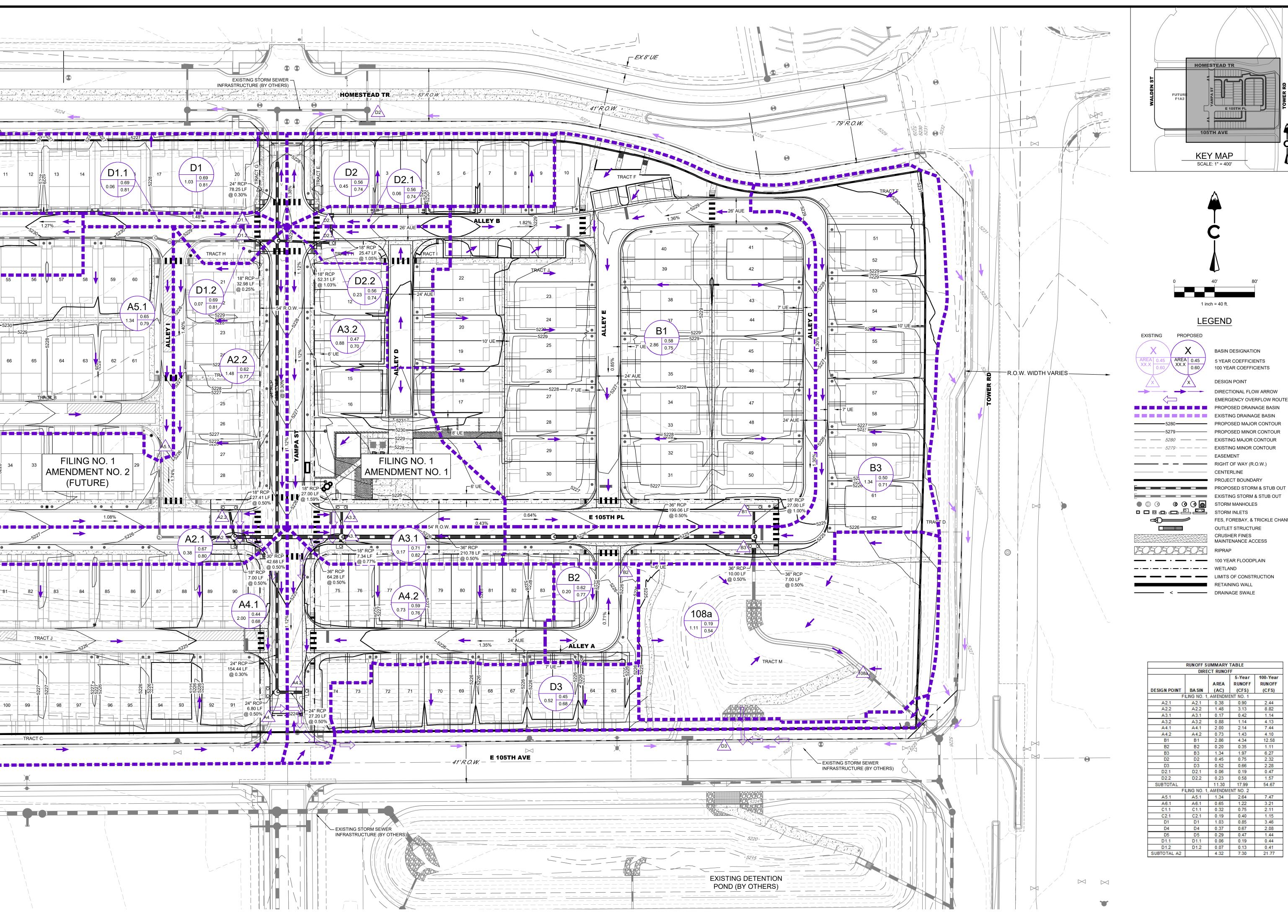
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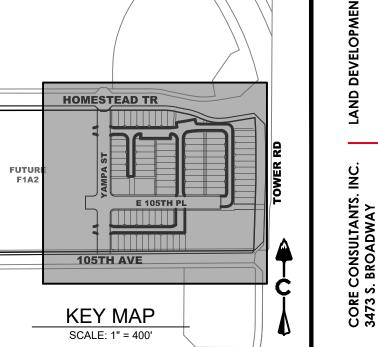
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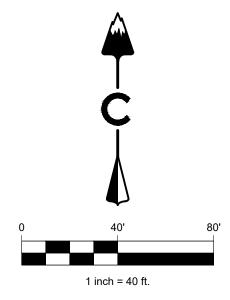


9\Drawings\Sheet Dwgs\Construction Plans\Phase 1\Duet and Commercia\Pond Details\Ponds 108a and 108b Outlet Structures.dwg, 20 Pond 108A Outlet-DT01, 12/

BACK POCKET DRAINAGE MAPS







RUNOFF SUMMARY TABLE 5-Year 100-Year AREA RUNOFF RUNOFF DESIGN POINT BASIN (AC) (CFS) (CFS) FILING NO. 1, AMENDMENT NO. 1
 A2.1
 0.38
 0.90
 2.44

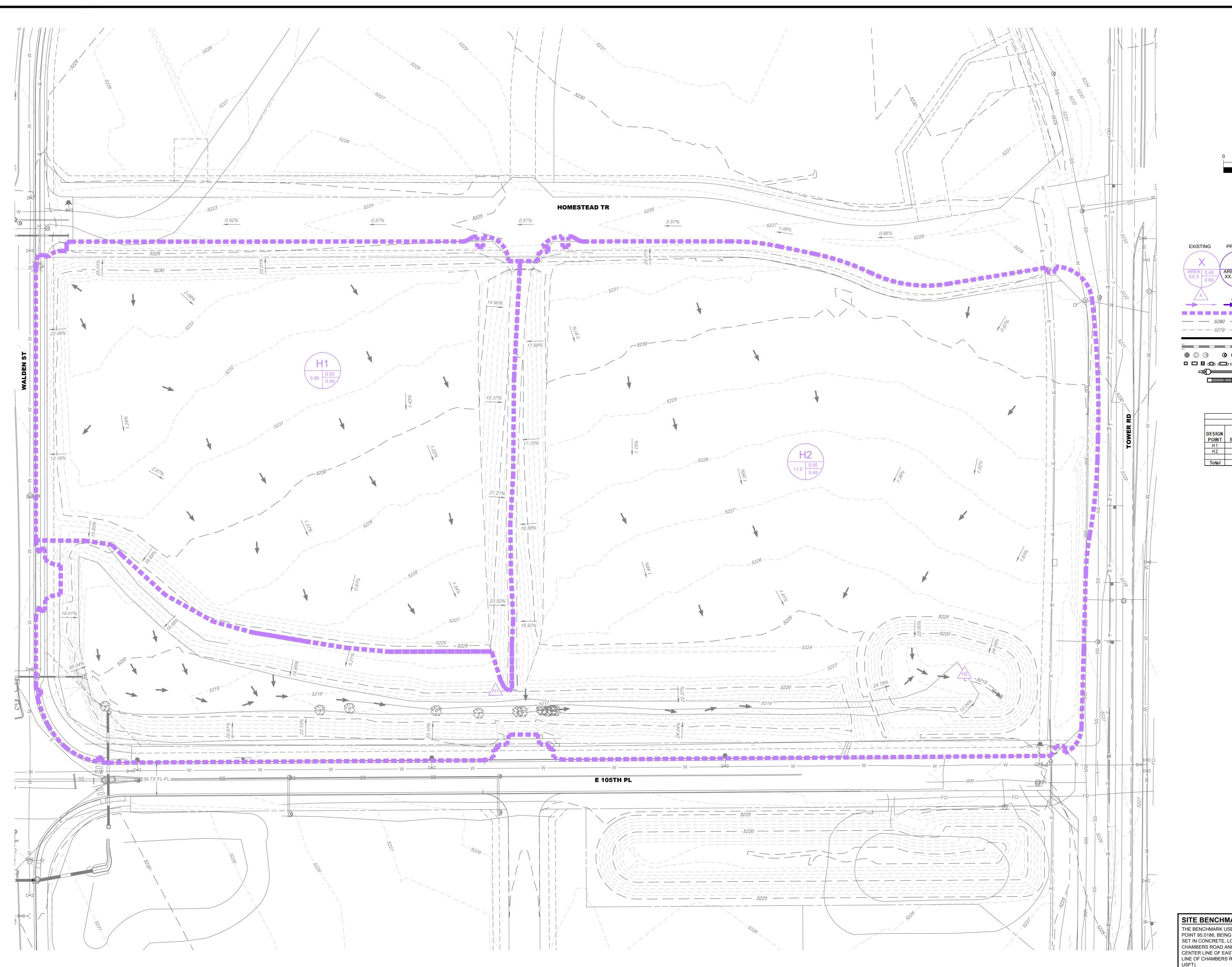
 A2.2
 1.48
 3.13
 8.82

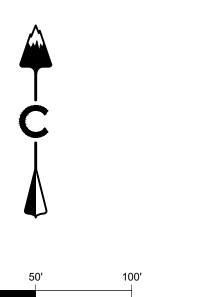
 A3.1
 0.17
 0.42
 1.14
 A3.2 A3.2 0.88 1.14 4.13 A4.1 A4.1 2.00 2.14 7.44 A4.2 0.73 1.43 B1 2.86 4.34 12.58 B2 0.20 0.35 1.11 D2.2 D2.2 0.23 0.58 1.57 SUBTOTAL 11.30 17.99 54.67 FILING NO. 1, AMENDMENT NO. 2 A5.1 A5.1 1.34 2.64 7.47

	OR HOM	
46	OK 110.	
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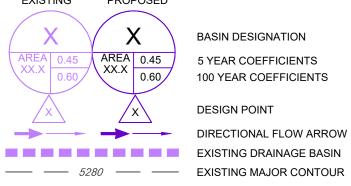
FILIN RCE C

DESIGNED BY: AC DRAWN BY: AC CHECKED BY: <u>JRS</u> JOB NO. 18-004 SHEET 1 OF









BASIN DESIGNATION AREA 0.45 5 YEAR COEFFICIENTS 100 YEAR COEFFICIENTS 100 YEAR COEFFICIENTS **DESIGN POINT**

STORM MANHOLES

STORM INLETS

 DIRECTIONAL FLOW ARROW — — — 5279- — — EXISTING MINOR CONTOUR PROJECT BOUNDARY EXISTING STORM & STUB OUT

FES, FOREBAY, & TRICKLE CHANNEL OUTLET STRUCTURE

		F SUMMA		
DESIGN POINT	BASIN	AREA (AC)	5-Year RUNOFF (CFS)	100-Yea RUNOF (CF S)
H1	H1	5.85	0.48	10.30
H2	H2	11.52	0.70	15.15
Total		17.37	1.18	25.45

SITE BENCHMARK:

THE BENCHMARK USED FOR THIS SITE IS ADAMS COUNTY CONTROL POINT 95.0186, BEING A 3-1/4" ALUMINUM CAP STAMPED "95.0186 1995" SET IN CONCRETE, LOCATED NORTHWEST OF THE INTERSECTION OF CHAMBERS ROAD AND EAST 112TH AVENUE, 157' NORTH OF THE CENTER LINE OF EAST 112TH AVENUE, AND 30' WEST OF THE CENTER LINE OF CHAMBERS ROAD, WITH AN ELEVATION OF 5143.89 (NAVD 1988)

JOB NO. 18-004 SHEET 1 OF 1

DESIGNED BY: ACJ

CHECKED BY: JRS

