

# PRELIMINARY DRAINAGE REPORT

# 6601 COLORADO BOULEVARD INDUSTRIAL AT CLAIRE AND ALYSSA INDUSTRIAL SUBDIVISION

Commerce City, Colorado

PREPARED FOR: 6601 COLORADO HOLDING, LLC 2551 N York St Denver, CO 80205 Attn: Karl Umland

PREPARED BY:

Galloway & Company, Inc. 5500 Greenwood Plaza Blvd, Suite 200 Greenwood Village, CO 80111 Attn: Jenny Romano

PREPARED: October 24, 2022

**REVISED:** 

**September 27, 2023** 

#### **ENGINEER'S STATEMENT**

I affirm that this report and plan for the Final drainage des prepared by me (or under my direct supervision) in accord Storm Drainage Design and Technical Criteria Manual for of Commerce City does not and will not assume liability fo	lance with the provisions of the Commerce City the owners thereof. I understand that the City
Jennifer Romano, PE #44401	 Date
For and on behalf of Galloway & Company, Inc.	
DEVELOPER'S CERTIFICATION	
"6601 Colorado Holding, LLC hereby certifies that the drai Industrial facility shall be constructed according to the des the City of Commerce City does not and will not assume li- certified by my engineer and that the City of Commerce C Municipal Code; but cannot, on behalf of 6601 Colorado H design review will absolve 6601 Colorado Holding, LLC ar liability for improper design."	ign presented in this report. I understand that iability for the drainage facilities designed and/o ity reviews drainage plans pursuant to the Holding, LLC, guarantee that final drainage
Authorized Signature	 Date
6601 Colorado Holding, LLC – Karl Umland	

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- A. Reference Materials
- B. Hydrology CalculationsC. Hydraulic CalculationsD. Drainage Map

## I. General Location and Description

### Location

The 6601 Colorado Holding site, is located on a parcel of land situated in the SW ¼ of Section 1, Township 3 south, Range 68 West of the 6<sup>th</sup> Principal Meridian, Commerce City, County of Adams, State of Colorado. The site is currently developed as a light vehicle storage yard, unused fields, a small collection of storage buildings, and two single family residences. The site is bound by Colorado Boulevard to the east, industrial private lots to the north and south, and the O'Brian canal to the west. See Appendix A for a Vicinity Map of the site.

### **Description of Property**

The site is currently developed as a storage yard with a few acres of unused field area and is zoned I-1 light industrial and AG agricultural. The project seeks to rezone the site as medium industrial (I-2). The area of disturbance is estimated to be approximately 11.36. acres. The west half of the site generally slopes to the northwest at 1-3% slopes while the east portion of the site slopes at less than 1% generally to the east.

According to the USDA NRCS Web Soil Survey for Adams County the site contains Terrace escarpments and Vona sandy loam, 0 to 1 percent, which are both classified as Hydrologic Soil Group A. Refer to Appendix A for soil survey information.

There are no known existing irrigation canals or irrigation ditches on the project site. There are no wetlands present on-site. O'Brian canal is located directly west of the site and will not be impacted by this development. Surrounding properties to the north and south of the site are zoned for industrial (I-1 and I-2). There's an existing Suncor pipeline easement along the south edge of the property as well as an easement for the O'Brian canal west of the site.

This report will present the proposed drainage design for this development, which includes regrading of the open yard of the site and a proposed warehouse building with associated paving on the east side of the site. On-site stormwater will be managed with a series of inlets connected to an infiltration pond. No existing connection to a public storm sewer exists or is proposed.

# **Proposed Project Description**

The project proposes to demolish all existing buildings on site as well as two existing water wells. The existing yard composing the majority of the site will be regraded to discourage ponding on site and route surface runoff to a proposed infiltration pond at the southwest corner of the site. A 30,000 SF light industrial building is proposed on the east side of the site. Paved parking and access drives surround the proposed building. Additional site improvements include installation of an approximately 263,260 SF reclaimed asphalt storage yard, utility services to the building, additional fencing and new access gates, site lights, and landscaping improvements. The development will be served by two access points along Colorado Boulevard.

# Drainage Studies Relevant to the Site

There are no known drainage studies relevant to the site or adjacent areas.

# II. Drainage Basins and Sub-Basins

# **Existing Basin Description**

The majority of the existing site, primarily the western section of the property, sheet flows west and outfalls to the existing O'Brian Canal. The remainder of the site is sloped at less than 1% generally sloping to the east. There are no existing detention or water quality facilities located on the project site

and there is no existing storm infrastructure in close proximity to the site. The proposed development will include stormwater infrastructure to collect and infiltrate water on site at a pond located in the southeast corner of the site. No offsite basins are accounted for in the proposed drainage design. No history of flooding is documented at the site as shown in the FEMA FIRM included in Appendix A of this report.

### **Proposed Sub-Basin Descriptions**

The proposed drainage plan for the site consists of nine drainage basins over the 11.55 acre site

As will be discussed later, the below proposed basin coverages are not reflected in the infiltration pond sizing. The pond has been sized to accommodate potential future use. In the existing and proposed condition, no off-site flows are anticipated to flow on site. Below is a breakdown of the site coverages as proposed:

Basin A-1 (0.69 acres) represents the proposed building roof area. Downspouts on the south side of the building route runoff to the concrete and asphalt paved area south of the building before runoff is collected and piped to the proposed infiltration pond.

Basin A-2 and A-3 (0.87 and 1.07 acres respectfully) are located on the eastern side of the site and consist of mostly paved areas surrounding the proposed building. They consist of asphalt and concrete pavement, sidewalks, and landscaping. Drainage from the basins is collected at a pair of inlets north and south of the proposed building. These inlets are routed to the proposed infiltration pond.

Basin A-4 through A-7 (2.90, 0.17, 1.87, and 3.65 acres respectfully) are located on the west portion of the site. The majority of this area is proposed as reclaimed asphalt storage/parking areas. Landscaping surrounds the yard. The individual basins are broken apart by drainage point. Runoff within basins A-4, A-5, and A-6 are routed by grass-lined swales and collected by inlets placed at low spots on the site. These inlets discharge to the proposed infiltration pond. Meanwhile, Basin A-7 sheet flows to the proposed infiltration pond.

Basin B-1 (0.13 acres) is located on the eastern most edge of the site. Due to proposed grading, this area is unable to be collected on site and is discharged to Colorado Boulevard.

Basing C-1 (0.19 acres) represents the landscaped edge of the existing canal that is infeasible to route to the proposed pond. Runoff on this sliver of land routes to the drainage ditch.

# III. Design Criteria

# Regulations

The proposed drainage design complies with the Mile High Flood District *Urban Storm Drainage Criteria Manual* and the Commerce City *Storm Drainage Design and Technical Criteria Manual*.

# **Hydrology**

The drainage calculations will be based on the *Storm Drainage Design and Technical Criteria Manual*. The design point rainfall values listed below will be utilized in the design calculations at a later stage in the project. These values were obtained from Chapter 5.2 of the *Storm Drainage Design and Technical Criteria Manual* (refer to Appendix A).

		Average Recurrence Interval (years)											
Duration	2	5	10	50	100								
60-min	0.97	1.37	1.55	2.24	2.58								

The time of concentration for each basin is assumed to be 5 minutes, which is based on the minimum allowable standards per the *Urban Storm Drainage Criteria Manual, Chapter 6*.

The rational method will used to calculate peak flows as the tributary areas are less than 100 acres. The rational method has proven to be accurate for basins of this size and is based on the following formula:

Q = CIA

Where:

Q = Peak Discharge (cfs)

C = Runoff Coefficient

I = Runoff Intensity (inches/hour)

A = Drainage Area (acres)

### Hydraulics

Sheet flow, swales, and inlets shall convey runoff through the site to the designated infiltration pond. The WQCV water surface elevation, EURV water surface elevation, and 100-year water surface elevation were calculated using the Mile High Flood District Detention Basin Design Workbook (refer to Appendix C).

## Water Quality Enhancement

The proposed infiltration pond will provide water quality for approximately 97.2% of the site, which meets the state MS4 permit requirement of 80% minimum. The remaining 0.32 acres (Basins B-1 and C-1) of the site will flow offsite untreated since it is infeasible to capture and treat runoff from these areas, as allowed by the MS4 permit. The proposed infiltration pond will be seeded and grown to established vegetation that will assist in the removal of soluble pollutants such as phosphorous and nitrogen through biological uptake. Sediment will be removed during the percolation process.

The site is required to disconnect impervious areas per section 14.3.1 of the City Storm Drainage Criteria Manual. 20% of the upstream impervious area must be disconnected via a combination of landscape buffers, swales, or permeable pavement. The project proposes to disconnect basin A-4 and A-6. These basins are characterized primarily by reclaimed asphalt yard area totaling 4.03 acres. Reclaimed asphalt is not counted as fully impervious. Instead, this area is modeled as 80% impervious which equates to 27.9% of the upstream impervious area of the total site. This fulfills the area requirements of section 14.3.1.

The area within these basins is disconnected via grass lined swales that convey water to inlets that discharge to the proposed infiltration pond on site. Calculations for these swales are provided in Appendix C. Specifically, swales 1, 6, and 7 (as identified on the drainage plan) have been analyzed. The entirety of the A-6 area was assumed to drain to swale 1. The flow in basin A-4 was split equally between swales 6 and 7. Swales 1 and 7 have slopes less than 2% in order to keep velocities below 1 ft/s. These two swales have underdrains that connect to the sump inlets at the end of each swale. In addition, the project proposes a series of riprap check dams within the swales to reduce swale velocities.

# IV. Stormwater Management Facility Design

### **Stormwater Conveyance Facilities**

Stormwater runoff will be conveyed through the site via sheet flow or vegetated swales, inlets, and pipes to the proposed infiltration pond.

## **Stormwater Storage Facilities**

A single infiltration pond will be provided at the southwest corner of the site. Infiltration was chosen because there is no existing storm infrastructure available on or adjacent to the site to outfall detained runoff nor can it be released into the O'Brian Canal. Percolation testing was performed in three pits on site and established a design infiltration rate of 50 in/hr. Nearby sites have utilized a similar approach for drainage conformance in Commerce City. As proposed, a majority of the site is proposed as a reclaimed asphalt paving yard suitable for storage or parking. Per coordination with Commerce City, the impervious value for reclaimed/recycled asphalt has been taken from the City of Fort Collins Criteria Manual, Chapter 5 Table RO-11. This table provides an impervious value of 80% for gravel areas. In Appendix B the composite percent impervious calculations show that this approach leads to an overall basin imperviousness of 63.1%. Therefore, the pond is sufficiently sized for the proposed development with additional capacity for further impervious development on the site.

A MHFD-Detention spreadsheet was utilized to calculate the 100-year water surface elevation for the pond. The 1-hour point rainfall data built into this spreadsheet was utilized. The Rain Garden – Bioretention BMP was used since this provides the most accurate approximation for an infiltration pond. The infiltration pond was sized for two times the required 100-year detention volume per Commerce City requirements. The percolation test performed by Ground indicates a design percolation rate of 50 in/hr. For the pond bottom area of 12,306 SF, this corresponds to an outflow rate of 14.24 cfs. An underdrain for the Rain Garden BMP was sized to match this infiltration rate. Because additional detention volume was provided a factor of safety was not applied to the release rates of the pond. The required design volume (2\*100-year detention volume) is 2.65 acre-feet. Based on the MHFD-Detention spreadsheet the provided storage volume in the 100-year storm event is 2.92 acre-feet.

#### V. Conclusions

# Compliance with Standards

The proposed storm drainage design has been performed in accordance with applicable sections of the MHFD *Urban Storm Drainage Criteria Manual*, the Commerce City *Storm Drainage Design and Technical Criteria Manual*, and sound engineering principles. The proposed improvements will modify existing drainage patterns to limit runoff currently running to neighboring properties or the existing canal by diverting flows to the proposed infiltration pond. The design shows that the runoff from the proposed and existing site improvements will be safely conveyed and treated with no adverse effects to downstream systems. Detailed calculations provided in this report show the design will be adequate for the proposed development.

#### VI. References

- 1. <u>Urban Storm Drainage Criteria Manual</u>, Mile High Flood District, August 2018 (with current revisions).
- 2. Storm Drainage Design and Technical Criteria Manual, City of Commerce City, May 2023.
- 3. Fort Collins Stormwater Criteria Manual, City of Fort Collins, December 2018.
- 4. Soil Map Adams County, Colorado as available through the Natural Resources Conservation Service National Cooperative Soil Survey web site via Web Soil Survey 2.0.

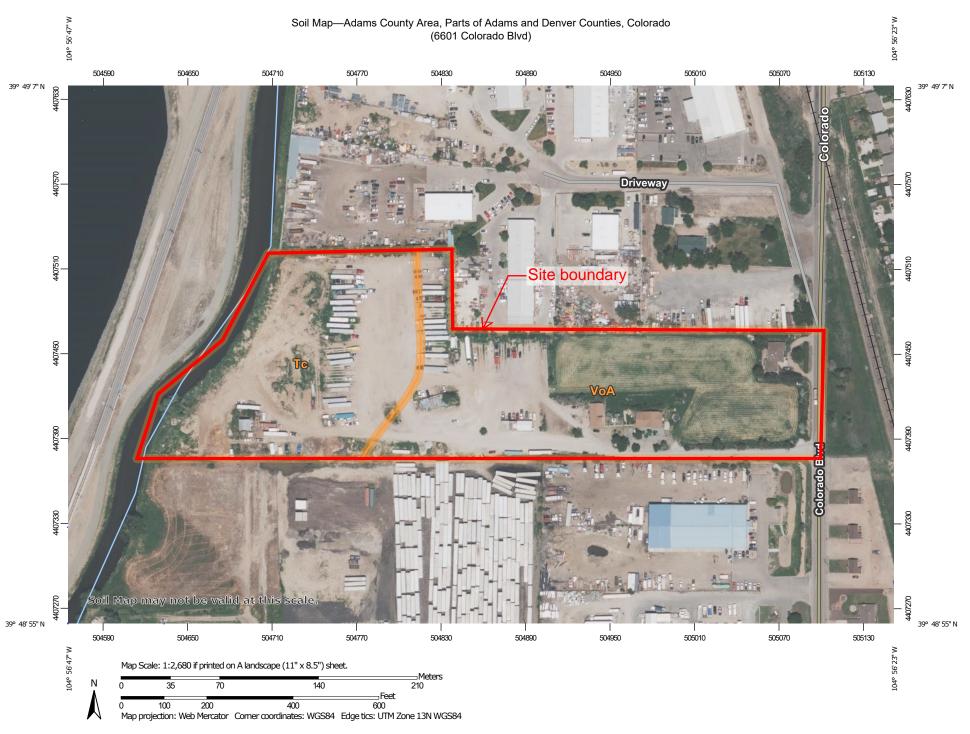
# **APPENDIX A – Reference Material**

Vicinity Map
NRCS Soils Map
FEMA FIRM





# VICINITY MAP



#### MAP LEGEND

#### Area of Interest (AOI)

Area of Interest (AOI)

#### Soils

Soil Map Unit Polygons



Soil Map Unit Lines



Soil Map Unit Points

#### **Special Point Features**

Blowout



Borrow Pit



Clay Spot



Closed Depression



Gravel Pit



**Gravelly Spot** 



Landfill



Lava Flow

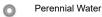
Marsh or swamp



Mine or Quarry



Miscellaneous Water



Rock Outcrop



Saline Spot



Sandy Spot



Severely Eroded Spot



Sinkhole



Slide or Slip



Sodic Spot

#### 8

Spoil Area



Stony Spot



Very Stony Spot



Wet Spot Other



Special Line Features

#### Water Features



Streams and Canals

#### Transportation



Rails



Interstate Highways



**US Routes** 



Major Roads

#### $\sim$

Local Roads

#### Background



Aerial Photography

#### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:20.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Adams County Area, Parts of Adams and Denver Counties, Colorado

Survey Area Data: Version 18, Aug 31, 2021

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jun 9, 2021—Jun 12, 2021

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

# **Map Unit Legend**

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
Тс	Terrace escarpments	5.3	42.9%
VoA	Vona sandy loam, 0 to 1 percent slopes	7.1	57.1%
Totals for Area of Interest		12.4	100.0%

# National Flood Hazard Layer FIRMette

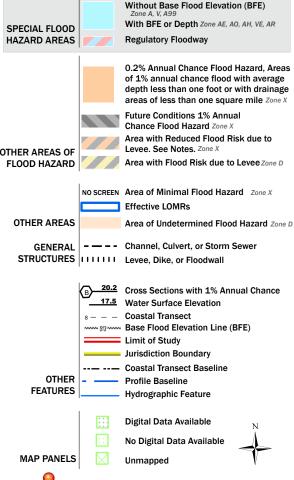


Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020



#### Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT



This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The pin displayed on the map is an approximate point selected by the user and does not represent

an authoritative property location.

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 2/7/2023 at 2:27 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

# **APPENDIX B – Hydrology Calculations**

#### **COMPOSITE % IMPERVIOUS CALCULATIONS**

Subdivision: Lot 1, CLAIRE AND ALYSSA INDUSTRIAL SUBDIVISION

Location: CO, Commerce City

 
 Project Name:
 6601 Colorado Blvd

 Project No.:
 6CH01

 Calculated By:
 MSJ
 Checked By: JRR
Date: 2/7/22

			Paved Roa	ds		Lawns			Roofs		Reclaime	ed Asphalt :	Surfacing	Basins Total
Basin ID	Total Area (ac)	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	Weighted % Imp.
A-1	0.69	100	0.00	0.00	0	0.00	0.00	90	0.69	90.20	80	0.00	0.00	90.20
A-2	0.87	100	0.63	72.69	0	0.24	0.00	90	0.00	0.00	80	0.00	0.00	72.69
A-3	1.07	100	1.03	95.87	0	0.05	0.00	90	0.00	0.00	80	0.00	0.00	95.87
A-4	2.90	100	0.00	0.00	0	0.24	0.00	90	0.00	0.00	80	2.66	73.50	73.50
A-5	0.17	100	0.00	0.00	0	0.17	0.00	90	0.00	0.00	80	0.00	0.00	0.00
A-6	1.87	100	0.00	0.00	0	0.50	0.00	90	0.00	0.00	80	1.37	58.60	58.60
A-7	3.65	100	0.00	0.00	0	1.47	0.00	90	0.00	0.00	80	2.19	47.90	47.90
B-1	0.14	100	0.04	28.57	0	0.10	0.00	90	0.00	0.00	80	0.00	0.00	28.57
C-1	0.19	100	0.00	0.00	0	0.19	0.00	90	0.00	0.00	80	0.00	0.00	0.00
Total	11.55	100	1.70	14.71	0	2.96	0.00	90	0.69	5.40	80	6.22	43.10	63.21

Total Site As Designed

Galloway & Company, Inc. Page 1 of 1

#### **COMPOSITE % IMPERVIOUS CALCULATIONS**

Subdivision: Lot 1, CLAIRE AND ALYSSA INDUSTRIAL SUBDIVISION

Location: CO, Commerce City

 Project Name:
 6601 Colorado Blvd

 Project No.:
 6CH01

 Calculated By:
 MSJ

Checked By: JRR
Date: 2/7/22

			Paved Roa	ds		Lawns			Roofs		Reclaime	ed Asphalt :	Surfacing	Basins Total
Basin ID	Total Area (ac)	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	Weighted % Imp.
A-1	0.69	100	0.00	0.00	0	0.00	0.00	90	0.69	90.20	80	0.00	0.00	90.20
A-2	0.87	100	0.63	72.69	0	0.24	0.00	90	0.00	0.00	80	0.00	0.00	72.69
A-3	1.07	100	1.03	95.87	0	0.05	0.00	90	0.00	0.00	80	0.00	0.00	95.87
A-4	2.90	100	0.00	0.00	0	0.24	0.00	90	0.00	0.00	80	2.66	73.50	73.50
A-5	0.17	100	0.00	0.00	0	0.17	0.00	90	0.00	0.00	80	0.00	0.00	0.00
A-6	1.87	100	0.00	0.00	0	0.50	0.00	90	0.00	0.00	80	1.37	58.60	58.60
A-7	3.65	100	0.00	0.00	0	1.47	0.00	90	0.00	0.00	80	2.19	47.90	47.90
B-1	0.13	100	0.03	22.73	0	0.10	0.00	90	0.00	0.00	80	0.00	0.00	22.73
C-1	0.19	100	0.00	0.00	0	0.19	0.00	90	0.00	0.00	80	0.00	0.00	0.00
Total	11.55	100	1.69	14.64	0	2.96	0.00	90	0.69	5.40	80	6.22	43.10	63.14

Total Site As Designed

Galloway & Company, Inc. Page 1 of 1

#### STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Lot 1, CLAIRE AND ALYSSA INDUSTRIAL SUBDIVISION Location: CO, Commerce City

Project Name: 6601 Colorado Blvd

Project No.: 6CH01
Calculated By: MSJ

Checked By: JRR

Date: 2/7/22

		SUB-BA	ASIN			INITI	AL/OVER	LAND		TR	AVEL TIN	ΛE			Tc CHECK		
		DAT	Ά				(T <sub>i</sub> )		(T <sub>t</sub> ) (URBANIZED BASINS)								FINAL
BASIN	D.A.	Hydrologic	Impervious	C <sub>100</sub>	C <sub>5</sub>	L	S	T <sub>i</sub>	L	L S Cv VEL. T, (					TOTAL	Urbanized T <sub>c</sub>	T <sub>c</sub>
ID	(AC)	Soils Group	(%)			(FT)	(%)	(MIN)	(FT)	(%)		(FPS)	(MIN)	(MIN)	LENGTH (FT)	(MIN)	(MIN)
A-1	0.69	Α	90.2	0.81	0.75												5.0
A-2	0.87	Α	72.7	0.68	0.57												5.0
A-3	1.07	Α	95.9	0.86	0.82												5.0
A-4	2.90	Α	73.5	0.68	0.58												5.0
A-5	0.17	Α	0.0	0.11	0.00												5.0
A-6	1.87	Α	58.6	0.57	0.44												5.0
A-7	3.65	Α	47.9	0.48	0.34												5.0
B-1	0.14	Α	28.6	0.33	0.17												5.0
C-1	0.19	Α	0.0	0.11	0.00												5.0
Total	11.55	Α	63.2	0.60	0.48												5.0
																	5.0

#### NOTES:

 $T_i = (0.395*(1.1 - C_5)*(L)^0.5)/((S)^0.33)$ , S in ft/ft

T<sub>t</sub>=L/60V (Velocity From Fig. 501) Velocity V=Cv\*S^0.5, S in ft/ft

Tc Check = 10+L/180

For Urbanized basins a minimum  $T_{\text{c}}$  of 5.0 minutes is required.

For non-urbanized basins a minimum T<sub>c</sub> of 10.0 minutes is required

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#### STANDARD FORM SF-3

#### STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision: Lot 1, CLAIRE AND ALYSSA INDUSTRIAL SUBDIVISION	
Location: CO, Commerce City	
Design Storm: 5-Year	

 Project Name:
 6601 Colorado Blvd

 Project No.:
 6CH01

 Calculated By:
 MSJ

 Checked By:
 JRR

 Date:
 2/7/22

				DIR	ECT R	JNOFF			1	OTAL	RUNOF	F	STF	REET		PIPE		TRA	VEL 1	IME	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	l (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	l (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	REMARKS
	1	A-1	0.69	0.75	5.0	0.52	4.79	2.5													Building Roof area
	1	A-2	0.87	0.57	5.0	0.49	4.79	2.3													Parking lot area north of building
	1	A-3	1.07	0.82	5.0	0.88	4.79	4.2													Parking lot area south of building
	1	A-4	2.90	0.58	5.0	1.68	4.79	8.0													Gravel lot, swale and inlet at north prop edge
	1	A-5	0.17	0.00	5.0	0.00	4.79	0.0													Landscape area, swale and inlet at north prop edge
	1	A-6	1.87	0.44	5.0	0.82	4.79	3.9													Gravel lot, swale and inlet along north and west edge
	1	A-7	3.65	0.34	5.0	1.24	4.79	5.9													Gravel lot, sheet flow to infiltration pond
									5.0	5.63	4.79	27.0									Total runoff from on-site to infiltration pond
	2	B-1	0.14	0.17	5.0	0.02	4.79	0.1													East frontage of site sheet flowing east to Colo. Blvd
									5.0	0.02	4.79	0.1									Total runoff from on-site to Colorado Blvd
	3	C-1	0.19	0.00	5.0	0.00	4.79	0.0													Existing area to remain. All Lscape. Sheet flow to canal
									5.0	0.00	4.79	0.0									Total runoff from on-site to O'Brian Canal

Galloway & Company, Inc. Page 1 of 1

## STANDARD FORM SF-3 STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Subdivision: Lot 1, CLAIRE AND ALYSSA INDUSTRIAL SUBDIVISION	
Location: CO, Commerce City	
Design Storm: 100-Year	

 Project Name:
 6601 Colorado Blvd

 Project No.:
 6CH01

 Calculated By:
 MSJ

 Checked By:
 JRR

 Date:
 2/7/22

				DIRE	CT RUN	IOFF				TOTAL	RUNOF	F	STR	REET		PIPE		TRA	VEL 1	IME	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	l (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	l (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	REMARKS
	1	A-1	0.69	0.81	5.0	0.56	9.02	5.1													Building Roof area
	1	A-2	0.87	0.68	5.0	0.59	9.02	5.3													Parking lot area north of building
	1	A-3	1.07	0.86	5.0	0.92	9.02	8.3													Parking lot area south of building
	1	A-4	2.90	0.68	5.0	1.97	9.02	17.8													Gravel lot, swale and inlet at north prop edge
	1	A-5	0.17	0.11	5.0	0.02	9.02	0.2													Landscape area, swale and inlet at north prop edge
	1	A-6	1.87	0.57	5.0	1.07	9.02	9.7													Gravel lot, swale and inlet along north and west edge
	1	A-7	3.65	0.48	5.0	1.75	9.02	15.8													Gravel lot, sheet flow to infiltration pond
									5.0	6.88	4.79	33.0									Total runoff from on-site to infiltration pond
	2	B-1	0.14	0.33	5.0	0.05	9.02	0.5													East frontage of site sheet flowing east to Colo. Blvd
									5.0	0.05	4.79	0.2									Total runoff from on-site to Colorado Blvd
	3	C-1	0.19	0.11	5.0	0.02	9.02	0.2													Existing area to remain. All Lscape. Sheet flow to canal
									5.0	0.02	4.79	0.1									Total runoff from on-site to O'Brian Canal

Galloway & Company, Inc. Page 1 of 1

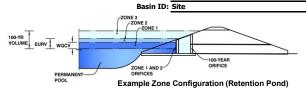
# **APPENDIX C – Hydraulic Calculations**

UD-Detention Spreadsheet
Emergency Spillway Sizing
UD-BMP Spreadsheets for Swales

#### DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)

Project: 6601 Colorado Boulevard



	Estimated	Estimated	
	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	0.63	0.185	Filtration Media
Zone 2 (EURV)	2.59	0.687	
Zone 3 (User)	#VALUE!	2.521	
``	Total (all zones)	3.392	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface) 1.00 Underdrain Orifice Diameter = 17.25 inches

	Calculated Parameters for Underda					
Underdrain Orifice Area =	1.6	ft <sup>2</sup>				
Underdrain Orifice Centroid =	0.72	feet				

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft) Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft) Orifice Plate: Orifice Vertical Spacing = inches Orifice Plate: Orifice Area per Row = inches

e

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (optional)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

<u>User Input: Vertical Orifice (Circular or Rectangular)</u>

	Not Selected	Not Selected		
Invert of Vertical Orifice =			ft (relative to basin bottom at Stage = 0 ft)	Vert
Depth at top of Zone using Vertical Orifice =			ft (relative to basin bottom at Stage = 0 ft)	Vertical
Vertical Orifice Diameter =			inches	

	Calculated Parame	ters for Vertical Orifi	ice
	Not Selected	Not Selected	
Vertical Orifice Area =		f	t <sup>2</sup>
rtical Orifice Centroid =		f	eet

Calculated Parameters for Overflow Weir

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe)

	Not Selected	Not Selected		Not Selected	Not Selected	
Overflow Weir Front Edge Height, Ho =			ft (relative to basin bottom at Stage = 0 ft) Height of Grate Upper Edge, $H_t$ =			feet
Overflow Weir Front Edge Length =			feet Overflow Weir Slope Length =			feet
Overflow Weir Grate Slope =			H:V Grate Open Area / 100-yr Orifice Area =			
Horiz. Length of Weir Sides =			feet Overflow Grate Open Area w/o Debris =			ft <sup>2</sup>
Overflow Grate Type =			Overflow Grate Open Area w/ Debris =			ft <sup>2</sup>
Debris Clogging % =			%			-

<u>User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)</u>

Outlet Pipe w/ Flow Restriction Plate	(Circular Orifice, I	Restrictor Plate, or	Rectangular Orifice)	Calculated Parameters	for Outlet Pipe w/	Flow Restriction Pl	ate
	Not Selected	Not Selected			Not Selected	Not Selected	l
Depth to Invert of Outlet Pipe =			ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =			ft <sup>2</sup>
Circular Orifice Diameter =			inches	Outlet Orifice Centroid =			feet
•			Half-Central Angle o	f Restrictor Plate on Pipe =	N/A	N/A	radians

User Input: Emer

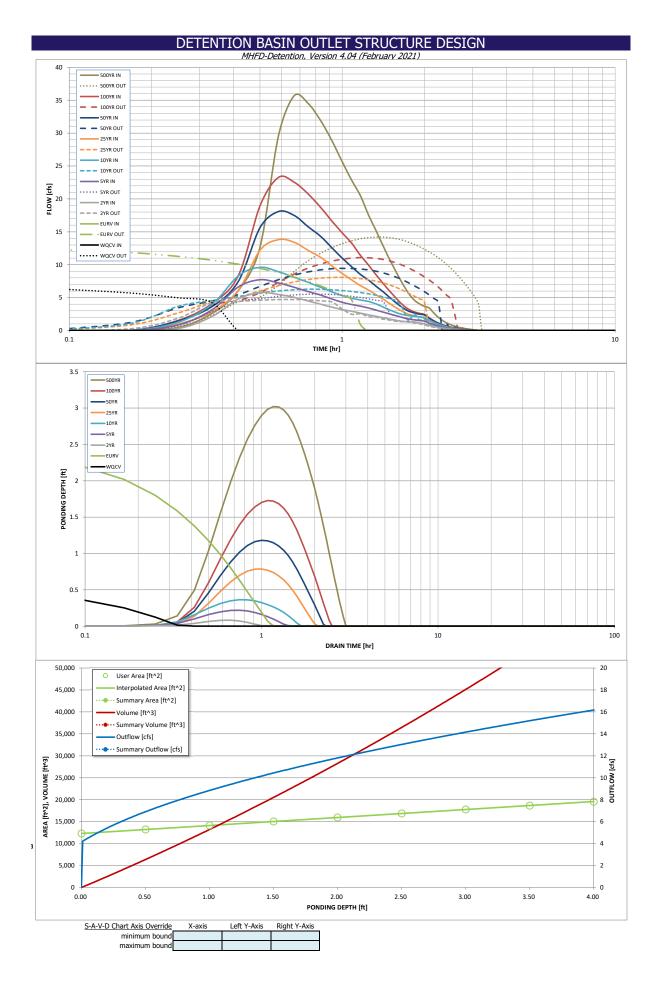
put: Emergency Spillway (Rectangular or Trapezoidal)										
Spillway Invert Stage=		ft (relative to basin bottom at Stage = 0 ft)								
Spillway Crest Length =		feet								
Spillway End Slopes =		H:V								
Freeboard above Max Water Surface =		feet								

	Calculated Parame	ters for Spillway
Spillway Design Flow Depth=		feet
Stage at Top of Freeboard =		feet
Basin Area at Top of Freeboard =		acres

Basin Volume at Top of Freeboard =

Routed Hydrograph Results	The user can over	The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).								
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year	
One-Hour Rainfall Depth (in) =	N/A	N/A	0.84	1.12	1.37	1.75	2.08	2.43	3.35	
CUHP Runoff Volume (acre-ft) =	0.185	0.871	0.437	0.599	0.754	1.016	1.285	1.606	2.445	
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.437	0.599	0.754	1.016	1.285	1.606	2.445	
CUHP Predevelopment Peak Q (cfs) =		N/A	0.0	0.0	0.1	0.2	2.0	4.5	11.0	
OPTIONAL Override Predevelopment Peak Q (cfs) =		N/A								
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.00	0.00	0.01	0.02	0.18	0.40	0.98	
Peak Inflow Q (cfs) =		N/A	5.8	7.7	9.6	13.8	18.1	23.3	35.7	
Peak Outflow Q (cfs) =	7.1	13.0	4.7	5.5	6.3	8.1	9.4	11.1	14.2	
Ratio Peak Outflow to Predevelopment Q =		N/A	N/A	145.3	73.8	38.5	4.6	2.5	1.3	
Structure Controlling Flow =	Filtration Media	Filtration Media	Filtration Media	Filtration Media	Filtration Media	Filtration Media	Filtration Media	Filtration Media	Filtration Media	
Max Velocity through Grate 1 (fps) =		N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	
Time to Drain 97% of Inflow Volume (hours) =	0	1	1	1	2	2	2	2	3	
Time to Drain 99% of Inflow Volume (hours) =	0	1	1	1	2	2	2	3	3	
Maximum Ponding Depth (ft) =		2.59	0.08	0.22	0.36	0.79	1.18	1.73	3.02	
Area at Maximum Ponding Depth (acres) =	0.31	0.39	0.29	0.29	0.30	0.32	0.33	0.35	0.41	
Maximum Volume Stored (acre-ft) =	0.186	0.872	0.023	0.060	0.104	0.233	0.362	0.548	1.040	

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## DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]		10 Year [cfs]		50 Year [cfs]		500 Year [cfs]
	0:00:00									
5.00 min	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:15:00	0.00	0.00	0.00	0.00	0.00 1.25	0.00	0.00 1.44	0.00 1.52	0.48 2.59
	0:20:00	0.00	0.00	2.12	3.13	3.97	2.84	3.63	4.09	6.05
	0:25:00	0.00	0.00	4.80	6.62	8.31	6.11	7.47	8.34	12.66
	0:30:00	0.00	0.00	5.77	7.71	9.59	12.19	15.63	18.93	29.50
	0:35:00	0.00	0.00	5.49	7.24	8.94	13.80	18.07	23.26	35.66
	0:40:00	0.00	0.00	5.05	6.57	8.09	13.42	17.51	22.55	34.53
	0:45:00	0.00	0.00	4.48	5.92	7.32	12.18	15.78	20.76	31.91
	0:50:00	0.00	0.00	3.99	5.38	6.56	11.12	14.32	18.72	28.88
	0:55:00	0.00	0.00	3.55	4.79	5.88	9.83	12.58	16.65	25.66
	1:00:00	0.00	0.00	3.18 2.93	4.28 3.94	5.30 4.91	8.67 7.69	11.01 9.69	14.84 13.28	22.86 20.48
	1:10:00	0.00	0.00	2.63	3.70	4.64	6.82	8.53	11.41	17.51
	1:15:00	0.00	0.00	2.38	3.41	4.40	6.13	7.63	9.93	15.11
	1:20:00	0.00	0.00	2.15	3.09	4.03	5.41	6.71	8.43	12.74
	1:25:00	0.00	0.00	1.93	2.78	3.54	4.75	5.85	7.09	10.64
	1:30:00	0.00	0.00	1.72	2.49	3.09	4.05	4.95	5.90	8.77
	1:35:00	0.00	0.00	1.53	2.23	2.71	3.41	4.14	4.83	7.10
	1:40:00	0.00	0.00	1.39	1.94	2.43	2.87	3.45	3.90	5.66
	1:45:00	0.00	0.00	1.32	1.75	2.27	2.47	2.96	3.24	4.66
	1:50:00 1:55:00	0.00	0.00	1.29	1.62	2.16	2.25	2.67	2.85	4.06
	2:00:00	0.00	0.00	1.15 1.03	1.53 1.42	2.06 1.89	2.10	2.49	2.61	3.68 3.41
	2:05:00	0.00	0.00	0.82	1.13	1.51	1.59	1.88	1.91	2.66
	2:10:00	0.00	0.00	0.64	0.88	1.18	1.23	1.46	1.45	2.00
	2:15:00	0.00	0.00	0.50	0.68	0.91	0.95	1.12	1.10	1.51
	2:20:00	0.00	0.00	0.38	0.53	0.70	0.73	0.86	0.84	1.15
	2:25:00	0.00	0.00	0.29	0.40	0.53	0.56	0.66	0.64	0.88
	2:30:00	0.00	0.00	0.22	0.30	0.40	0.42	0.49	0.48	0.66
	2:35:00	0.00	0.00	0.17	0.22	0.30	0.31	0.37	0.36	0.49
	2:40:00 2:45:00	0.00	0.00	0.12	0.16 0.12	0.23 0.16	0.23 0.17	0.28 0.20	0.28 0.20	0.38
	2:50:00	0.00	0.00	0.09	0.12	0.16	0.17	0.20	0.20	0.28
	2:55:00	0.00	0.00	0.04	0.05	0.07	0.08	0.09	0.09	0.12
	3:00:00	0.00	0.00	0.02	0.03	0.04	0.05	0.05	0.05	0.07
	3:05:00	0.00	0.00	0.01	0.01	0.02	0.02	0.02	0.02	0.03
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00 3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00 4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00 4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00 4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00 5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00 5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00 6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ı	0.00.00	0.00	0.00	0.00	0.00	0.00	0.00	5.00	0.00	5.50

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## DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)

Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.

The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage Description	Stage [ft]	Area [ft ²]	Area [acres]	Volume [ft <sup>3</sup> ]	Volume [ac-ft]	Total Outflow [cfs]	
							For best results, include the
							stages of all grade slope
							changes (e.g. ISV and Floor) from the S-A-V table on
							Sheet 'Basin'.
							Also include the inverts of al outlets (e.g. vertical orifice,
							overflow grate, and spillway
							where applicable).
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MHFD-Detention\_v4 04.xlsm, Outlet Structure

#### Emergency spillway sizing

Q\_total 62.60001 cfs

$$Q = C_{BCW}LH^{1.5}$$
 Equation 12-8

Where:

Q = discharge (cfs)

 $C_{BCW}$  = broad-crested weir coefficient (This ranges from 2.6 to 3.0. A value of 3.0 is often used in practice.) See Hydraulic Engineering Circular No. 22 for additional information.

L =broad-crested weir length (ft)

H = head above weir crest (ft)

<u>Sloping Broad-Crested Weir:</u> Figure 12-20 shows an example of a sloping broad-crested weir. The equation to calculate the flow over the sloping portion of the weir is as follows:

$$Q = \left(\frac{2}{5}\right) C_{BCW} Z H^{2.5}$$
 Equation 12-9

Where:

Q = discharge (cfs)

 $C_{BCW}$  = broad-crested weir coefficient (This ranges from 2.6 to 3.0. A value of 3.0 is often used in practice.) See Hydraulic Engineering Circular No. 22 for additional information.

Z = side slope (horizontal: vertical)

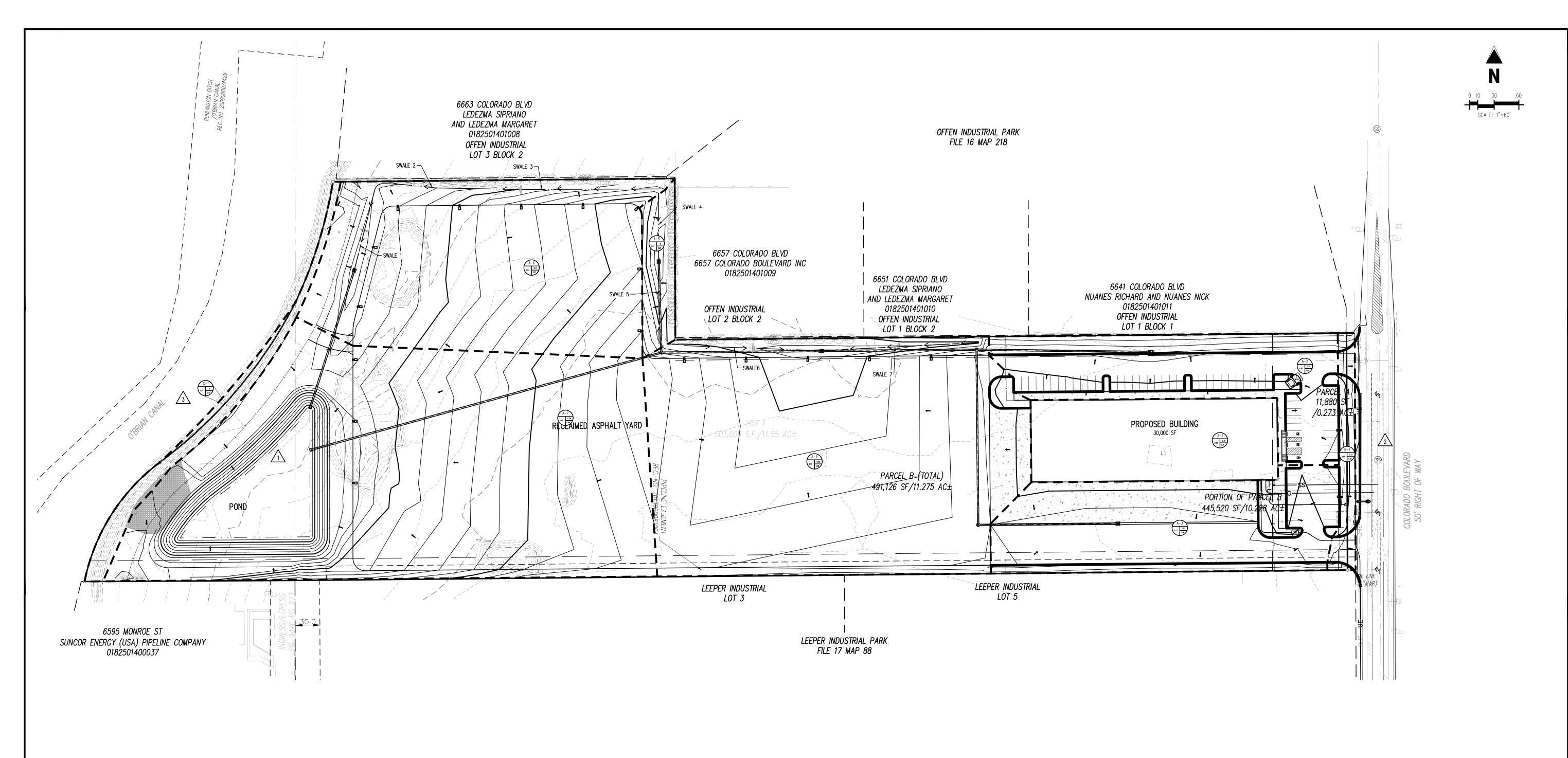
H = head above weir crest (ft)

	Design Procedure Form: Grass	
Docimor	UD-BMP (Version 3.07, March 2	(1018) Sheet 1 of 1
Designer: Company:	Galloway	
Date:	September 27, 2023	
Project:	6601 Colorado Boulevard	
Location:	Commerce City, CO - SWALE 1	<del></del>
1. Design Dis	charge for 2-Year Return Period	Q <sub>2</sub> = 3.90 cfs
2. Hydraulic R	Residence Time	
A) : Length	n of Grass Swale	L <sub>S</sub> = 257.0 ft
B) Calcula	ted Residence Time (based on design velocity below)	T <sub>HR</sub> = 4.4 minutes
3. Longitudina	al Slope (vertical distance per unit horizontal)	
A) Availab	le Slope (based on site constraints)	S <sub>avail</sub> = 0.020 ft / ft
B) Design		$S_D = 0.008$ ft / ft
4. Swale Geo	metry	
A) Channe	el Side Slopes (Z = 4 min., horiz. distance per unit vertical)	$Z = \underbrace{4.00}_{ft / ft}$
B) Bottom	Width of Swale (enter 0 for triangular section)	W <sub>B</sub> = 0.00 ft
5. Vegetation		Choose One
A) Type of	Planting (seed vs. sod, affects vegetal retardance factor)	☐ Grass From Seed
6. Design Vel	ocity (0.857 ft / s maximum for desirable 5-minute residence time)	$V_2 = 0.98$ ft / s
7. Design Flo	w Depth (1 foot maximum)	$D_2 = 1.00$ ft
A) Flow Ar	rea	$A_2 = 4.0$ sq ft
B) Top Wi	dth of Swale	$W_T = 8.0$ ft
C) Froude I	Number (0.50 maximum)	F = 0.24
D) Hydrau	lic Radius	R <sub>H</sub> = 0.49
E) Velocity	y-Hydraulic Radius Product for Vegetal Retardance	VR = 0.47
F) Mannin	g's n (based on SCS vegetal retardance curve D for sodded grass)	n = 0.084
G) Cumula	ative Height of Grade Control Structures Required	$H_D = \boxed{3.10}$ ft
8. Underdrain (Is an und	n derdrain necessary?)	Choose One  PYES NO  AN UNDERDRAIN IS  REQUIRED IF THE  DESIGN SLOPE < 2.0%
9. Soil Prepar (Describe s	ration soil amendment)	
10. Irrigation		Choose One Permanent
Notes:		

	Design Procedure Form: Grass	Swale (GS)	
Designer:	UD-BMP (Version 3.07, March 2	2018) She	eet 1 of 1
Company: Date:	May 26, 2023		
Project:	6601 Colorado Boulevard		
Location:	Commerce City, CO - SWALE 6		
1. Design Dis	scharge for 2-Year Return Period	Q <sub>2</sub> = 4.00 cfs	
2. Hydraulic F	Residence Time		
A) : Lengt	h of Grass Swale	L <sub>S</sub> = 165.0 ft	
B) Calcula	ated Residence Time (based on design velocity below)	T <sub>HR</sub> = 3.0 minutes	
3. Longitudina	al Slope (vertical distance per unit horizontal)		
A) Availab	ole Slope (based on site constraints)	$S_{avail} = 0.020$ ft / ft	
B) Design	Slope	$S_D = 0.020$ ft / ft	
4. Swale Geo	ometry		
A) Channe	el Side Slopes (Z = 4 min., horiz. distance per unit vertical)	Z = 10.30 ft / ft	
B) Bottom	Width of Swale (enter 0 for triangular section)	W <sub>B</sub> = 0.00 ft	
5. Vegetation		Choose One	
A) Type of	f Planting (seed vs. sod, affects vegetal retardance factor)	Grass From Seed Grass From Sod	
6. Design Ve	locity (0.55 ft / s maximum for desirable 5-minute residence time)	V <sub>2</sub> = 0.92 ft / s	
7. Design Flo	w Depth (1 foot maximum)	D <sub>2</sub> = 0.65 ft	
A) Flow A	rea	$A_2 = 4.4$ sq ft	
B) Top Wi	idth of Swale	W <sub>T</sub> = 13.4 ft	
C) Froude	Number (0.50 maximum)	F = 0.28	
D) Hydrau	ılic Radius	R <sub>H</sub> = 0.32	
E) Velocit	y-Hydraulic Radius Product for Vegetal Retardance	VR = 0.30	
	g's n (based on SCS vegetal retardance curve D for sodded grass)	n = 0.107	
•	ative Height of Grade Control Structures Required	$H_D = \begin{bmatrix} 0.00 & \text{ft} \end{bmatrix}$	
G) Cumul	auve meight of Grade Control Structures Required	110 - 0.00 11	
8. Underdrair (Is an und	n derdrain necessary?)	Choose One  YES NO	
9. Soil Prepa (Describe	ration soil amendment)		
,	,		
10. Irrigation		Choose One Permanent	
Notes:		ı	

	Design Procedure Form: Grass	Swale (GS)
Danismas	UD-BMP (Version 3.07, March 2	2018) Sheet 1 of 1
Designer:	MSJ Galloway	
Company: Date:	September 27, 2023	
Project:	6601 Colorado Boulevard	
Location:	Commerce City, CO - SWALE 7	
	-	
1. Design Dis	scharge for 2-Year Return Period	Q <sub>2</sub> = 4.00 cfs
2. Hydraulic F	Residence Time	
A) : Lengtl	h of Grass Swale	L <sub>S</sub> = 187.5 ft
B) Calcula	ated Residence Time (based on design velocity below)	T <sub>HR</sub> = 3.2 minutes
3. Longitudina	al Slope (vertical distance per unit horizontal)	
A) Availab	ole Slope (based on site constraints)	$S_{avail} = 0.020$ ft / ft
B) Design	Slope	$S_D = 0.010$ ft / ft
4. Swale Geo	ometry	
A) Channe	el Side Slopes (Z = 4 min., horiz. distance per unit vertical)	Z = 5.00   ft / ft
B) Bottom	Width of Swale (enter 0 for triangular section)	$W_B = 0.00$ ft
5. Vegetation		Choose One
A) Type of	f Planting (seed vs. sod, affects vegetal retardance factor)	Grass From Seed Grass From Sod
6. Design Vel	locity (0.625 ft / s maximum for desirable 5-minute residence time)	$V_2 =                                   $
7. Design Flo	w Depth (1 foot maximum)	$D_2 =                                   $
A) Flow A	rea	$A_2 = 4.1$ sq ft
B) Top Wi	dth of Swale	$W_T = 9.0$ ft
C) Froude	Number (0.50 maximum)	F = 0.26
D) Hydrau	lic Radius	R <sub>H</sub> = 0.44
E) Velocity	y-Hydraulic Radius Product for Vegetal Retardance	VR = 0.44
F) Mannin	g's n (based on SCS vegetal retardance curve D for sodded grass)	n = 0.088
G) Cumula	ative Height of Grade Control Structures Required	$H_D = \boxed{1.90}$ ft
8. Underdrair (Is an und	n derdrain necessary?)	Choose One  O YES NO  AN UNDERDRAIN IS REQUIRED IF THE DESIGN SLOPE < 2.0%
9. Soil Prepa (Describe s	ration soil amendment)	
10. Irrigation		Choose One Permanent
Notes:		

# APPENDIX D - Drainage Map



# DRAINAGE LEGEND PROPERTY BOUNDARY LINE ADJACENT PROPERTY BOUNDARY LINE ----- RIGHT OF WAY BOUNDARY LINE - - - - - - - - EXISTING EASEMENT LINE ---- PROPOSED EASEMENT LINE PROPOSED STORM SEWER (LESS THAN 12"ø) PROPOSED STORM SEWER (12" Ø AND LARGER) PROPOSED CURB AND GUTTER (SPILL) PROPOSED CURB AND GUTTER (CATCH) - — - 5460 — - Existing major contour ----- EXISTING MINOR CONTOUR PROPOSED MAJOR CONTOUR MAJOR BASIN BOUNDARY LINE DESIGN POINT FLOW ARROW ---- BASIN DESIGNATION 100 5-YEAR RUNOFF COEFFICIENT 0.00 100-YEAR RUNOFF COEFFICIENT

CITY STAFF CERTIFICATE	
APPROVED BY THE DEPARTMENT OF COMMUNITY DEVELOPMENT OF THE CITY OF	
COMMERCE CITY, THIS DAY OF,	A.D.
DEPARTMENT OF COMMUNITY DEVELOPMENT SIGNATURE	

BASIN AREA IN ACRES

# Galloway

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RAINAGE MAP OT 1, CLAIRE AND ALYSSA NDUSTRIAL SUBDIVISION

# Date Issue / Description

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Project No:	6CH000001
Drawn By:	RDG
Checked By:	MSJ
Date:	09/27/2023

FINAL DRAINAGE PLAN

DR1