

# PRELIMINARY DRAINAGE REPORT

# 6601 COLORADO BOULEVARD INDUSTRIAL AT CLAIRE AND ALYSSA INDUSTRIAL SUBDIVISION

Commerce City, Colorado

PREPARED FOR: 6601 COLORADO HOLDING, LLC 2551 N York St Denver, CO 80205 Attn: Karl Umland

PREPARED BY: Galloway & Company, Inc. 5500 Greenwood Plaza Blvd, Suite 200 Greenwood Village, CO 80111 Attn: Jenny Romano

PREPARED: October 24, 2022

REVISED: September 27, 2023

### **ENGINEER'S STATEMENT**

I affirm that this report and plan for the Final drainage design for 6601 Colorado Holding, LLC was prepared by me (or under my direct supervision) in accordance with the provisions of the Commerce City Storm Drainage Design and Technical Criteria Manual for the owners thereof. I understand that the City of Commerce City does not and will not assume liability for drainage facilities designed by others.

Jennifer Romano, PE #44401 For and on behalf of Galloway & Company, Inc. Date

### **DEVELOPER'S CERTIFICATION**

"6601 Colorado Holding, LLC hereby certifies that the drainage facilities for the 6601 Colorado Boulevard Industrial facility shall be constructed according to the design presented in this report. I understand that the City of Commerce City does not and will not assume liability for the drainage facilities designed and/or certified by my engineer and that the City of Commerce City reviews drainage plans pursuant to the Municipal Code; but cannot, on behalf of 6601 Colorado Holding, LLC, guarantee that final drainage design review will absolve 6601 Colorado Holding, LLC and/or their successors and/or assigns of future liability for improper design."

Authorized Signature 6601 Colorado Holding, LLC – Karl Umland Date

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# I. General Location and Description

### **Location**

The 6601 Colorado Holding site, is located on a parcel of land situated in the SW ¼ of Section 1, Township 3 south, Range 68 West of the 6<sup>th</sup> Principal Meridian, Commerce City, County of Adams, State of Colorado. The site is currently developed as a light vehicle storage yard, unused fields, a small collection of storage buildings, and two single family residences. The site is bound by Colorado Boulevard to the east, industrial private lots to the north and south, and the O'Brian canal to the west. See Appendix A for a Vicinity Map of the site.

# **Description of Property**

The site is currently developed as a storage yard with a few acres of unused field area and is zoned I-1 light industrial and AG agricultural. The project seeks to rezone the site as medium industrial (I-2). The area of disturbance is estimated to be approximately 11.36. acres. The west half of the site generally slopes to the northwest at 1-3% slopes while the east portion of the site slopes at less than 1% generally to the east.

According to the USDA NRCS Web Soil Survey for Adams County the site contains Terrace escarpments and Vona sandy loam, 0 to 1 percent, which are both classified as Hydrologic Soil Group A. Refer to Appendix A for soil survey information.

There are no known existing irrigation canals or irrigation ditches on the project site. There are no wetlands present on-site. O'Brian canal is located directly west of the site and will not be impacted by this development. Surrounding properties to the north and south of the site are zoned for industrial (I-1 and I-2). There's an existing Suncor pipeline easement along the south edge of the property as well as an easement for the O'Brian canal west of the site.

This report will present the proposed drainage design for this development, which includes regrading of the open yard of the site and a proposed warehouse building with associated paving on the east side of the site. On-site stormwater will be managed with a series of inlets connected to an infiltration pond. No existing connection to a public storm sewer exists or is proposed.

# Proposed Project Description

The project proposes to demolish all existing buildings on site as well as two existing water wells. The existing yard composing the majority of the site will be regraded to discourage ponding on site and route surface runoff to a proposed infiltration pond at the southwest corner of the site. A 30,000 SF light industrial building is proposed on the east side of the site. Paved parking and access drives surround the proposed building. Additional site improvements include installation of an approximately 263,260 SF reclaimed asphalt storage yard, utility services to the building, additional fencing and new access gates, site lights, and landscaping improvements. The development will be served by two access points along Colorado Boulevard.

# Drainage Studies Relevant to the Site

There are no known drainage studies relevant to the site or adjacent areas.

# II. Drainage Basins and Sub-Basins

### **Existing Basin Description**

The majority of the existing site, primarily the western section of the property, sheet flows west and outfalls to the existing O'Brian Canal. The remainder of the site is sloped at less than 1% generally sloping to the east. There are no existing detention or water quality facilities located on the project site

and there is no existing storm infrastructure in close proximity to the site. The proposed development will include stormwater infrastructure to collect and infiltrate water on site at a pond located in the southeast corner of the site. No offsite basins are accounted for in the proposed drainage design. No history of flooding is documented at the site as shown in the FEMA FIRM included in Appendix A of this report.

# Proposed Sub-Basin Descriptions

The proposed drainage plan for the site consists of nine drainage basins over the 11.55 acre site

As will be discussed later, the below proposed basin coverages are not reflected in the infiltration pond sizing. The pond has been sized to accommodate potential future use. In the existing and proposed condition, no off-site flows are anticipated to flow on site. Below is a breakdown of the site coverages as proposed:

Basin A-1 (0.69 acres) represents the proposed building roof area. Downspouts on the south side of the building route runoff to the concrete and asphalt paved area south of the building before runoff is collected and piped to the proposed infiltration pond.

Basin A-2 and A-3 (0.87 and 1.07 acres respectfully) are located on the eastern side of the site and consist of mostly paved areas surrounding the proposed building. They consist of asphalt and concrete pavement, sidewalks, and landscaping. Drainage from the basins is collected at a pair of inlets north and south of the proposed building. These inlets are routed to the proposed infiltration pond.

Basin A-4 through A-7 (2.90, 0.17, 1.87, and 3.65 acres respectfully) are located on the west portion of the site. The majority of this area is proposed as reclaimed asphalt storage/parking areas. Landscaping surrounds the yard. The individual basins are broken apart by drainage point. Runoff within basins A-4, A-5, and A-6 are routed by grass-lined swales and collected by inlets placed at low spots on the site. These inlets discharge to the proposed infiltration pond. Meanwhile, Basin A-7 sheet flows to the proposed infiltration pond.

Basin B-1 (0.13 acres) is located on the eastern most edge of the site. Due to proposed grading, this area is unable to be collected on site and is discharged to Colorado Boulevard.

Basing C-1 (0.19 acres) represents the landscaped edge of the existing canal that is infeasible to route to the proposed pond. Runoff on this sliver of land routes to the drainage ditch.

# **III. Design Criteria**

### **Regulations**

The proposed drainage design complies with the Mile High Flood District *Urban Storm Drainage Criteria Manual* and the Commerce City *Storm Drainage Design and Technical Criteria Manual*.

### **Hydrology**

The drainage calculations will be based on the *Storm Drainage Design and Technical Criteria Manual*. The design point rainfall values listed below will be utilized in the design calculations at a later stage in the project. These values were obtained from Chapter 5.2 of the *Storm Drainage Design and Technical Criteria Manual* (refer to Appendix A).

		Average F	Recurrence Interv	/al (years)	
Duration	2	5	10	50	100
60-min	0.97	1.37	1.55	2.24	2.58

The time of concentration for each basin is assumed to be 5 minutes, which is based on the minimum allowable standards per the *Urban Storm Drainage Criteria Manual, Chapter 6*.

The rational method will used to calculate peak flows as the tributary areas are less than 100 acres. The rational method has proven to be accurate for basins of this size and is based on the following formula:

Where:

Q = Peak Discharge (cfs)
C = Runoff Coefficient
I = Runoff Intensity (inches/hour)
A = Drainage Area (acres)

### **Hydraulics**

Sheet flow, swales, and inlets shall convey runoff through the site to the designated infiltration pond. The WQCV water surface elevation, EURV water surface elevation, and 100-year water surface elevation were calculated using the Mile High Flood District Detention Basin Design Workbook (refer to Appendix C).

# Water Quality Enhancement

The proposed infiltration pond will provide water quality for approximately 97.2% of the site, which meets the state MS4 permit requirement of 80% minimum. The remaining 0.32 acres (Basins B-1 and C-1) of the site will flow offsite untreated since it is infeasible to capture and treat runoff from these areas, as allowed by the MS4 permit. The proposed infiltration pond will be seeded and grown to established vegetation that will assist in the removal of soluble pollutants such as phosphorous and nitrogen through biological uptake. Sediment will be removed during the percolation process.

The site is required to disconnect impervious areas per section 14.3.1 of the City Storm Drainage Criteria Manual. 20% of the upstream impervious area must be disconnected via a combination of landscape buffers, swales, or permeable pavement. The project proposes to disconnect basin A-4 and A-6. These basins are characterized primarily by reclaimed asphalt yard area totaling 4.03 acres. Reclaimed asphalt is not counted as fully impervious. Instead, this area is modeled as 80% impervious which equates to 27.9% of the upstream impervious area of the total site. This fulfills the area requirements of section 14.3.1.

The area within these basins is disconnected via grass lined swales that convey water to inlets that discharge to the proposed infiltration pond on site. Calculations for these swales are provided in Appendix C. Specifically, swales 1, 6, and 7 (as identified on the drainage plan) have been analyzed. The entirety of the A-6 area was assumed to drain to swale 1. The flow in basin A-4 was split equally between swales 6 and 7. Swales 1 and 7 have slopes less than 2% in order to keep velocities below 1 ft/s. These two swales have underdrains that connect to the sump inlets at the end of each swale. In addition, the project proposes a series of riprap check dams within the swales to reduce swale velocities.

# **IV. Stormwater Management Facility Design**

# Stormwater Conveyance Facilities

Stormwater runoff will be conveyed through the site via sheet flow or vegetated swales, inlets, and pipes to the proposed infiltration pond.

# Stormwater Storage Facilities

A single infiltration pond will be provided at the southwest corner of the site. Infiltration was chosen because there is no existing storm infrastructure available on or adjacent to the site to outfall detained runoff nor can it be released into the O'Brian Canal. Percolation testing was performed in three pits on site and established a design infiltration rate of 50 in/hr. Nearby sites have utilized a similar approach for drainage conformance in Commerce City. As proposed, a majority of the site is proposed as a reclaimed asphalt paving yard suitable for storage or parking. Per coordination with Commerce City, the impervious value for reclaimed/recycled asphalt has been taken from the City of Fort Collins Criteria Manual, Chapter 5 Table RO-11. This table provides an impervious value of 80% for gravel areas. In Appendix B the composite percent impervious calculations show that this approach leads to an overall basin imperviousness of 63.1%. Therefore, the pond is sufficiently sized for the proposed development with additional capacity for further impervious development on the site.

A MHFD-Detention spreadsheet was utilized to calculate the 100-year water surface elevation for the pond. The 1-hour point rainfall data built into this spreadsheet was utilized. The Rain Garden – Bioretention BMP was used since this provides the most accurate approximation for an infiltration pond. The infiltration pond was sized for two times the required 100-year detention volume per Commerce City requirements. The percolation test performed by Ground indicates a design percolation rate of 50 in/hr. For the pond bottom area of 12,306 SF, this corresponds to an outflow rate of 14.24 cfs. An underdrain for the Rain Garden BMP was sized to match this infiltration rate. Because additional detention volume was provided a factor of safety was not applied to the release rates of the pond. The required design volume (2\*100-year detention volume) is 2.65 acre-feet. Based on the MHFD-Detention spreadsheet the provided storage volume in the 100-year storm event is 2.92 acre-feet.

# V. Conclusions

# **Compliance with Standards**

The proposed storm drainage design has been performed in accordance with applicable sections of the MHFD *Urban Storm Drainage Criteria Manual*, the Commerce City *Storm Drainage Design and Technical Criteria Manual*, and sound engineering principles. The proposed improvements will modify existing drainage patterns to limit runoff currently running to neighboring properties or the existing canal by diverting flows to the proposed infiltration pond. The design shows that the runoff from the proposed and existing site improvements will be safely conveyed and treated with no adverse effects to downstream systems. Detailed calculations provided in this report show the design will be adequate for the proposed development.

# **VI. References**

- 1. <u>Urban Storm Drainage Criteria Manual</u>, Mile High Flood District, August 2018 (with current revisions).
- 2. <u>Storm Drainage Design and Technical Criteria Manual</u>, City of Commerce City, May 2023.
- 3. Fort Collins Stormwater Criteria Manual, City of Fort Collins, December 2018.
- 4. Soil Map Adams County, Colorado as available through the Natural Resources Conservation Service National Cooperative Soil Survey web site via Web Soil Survey 2.0.

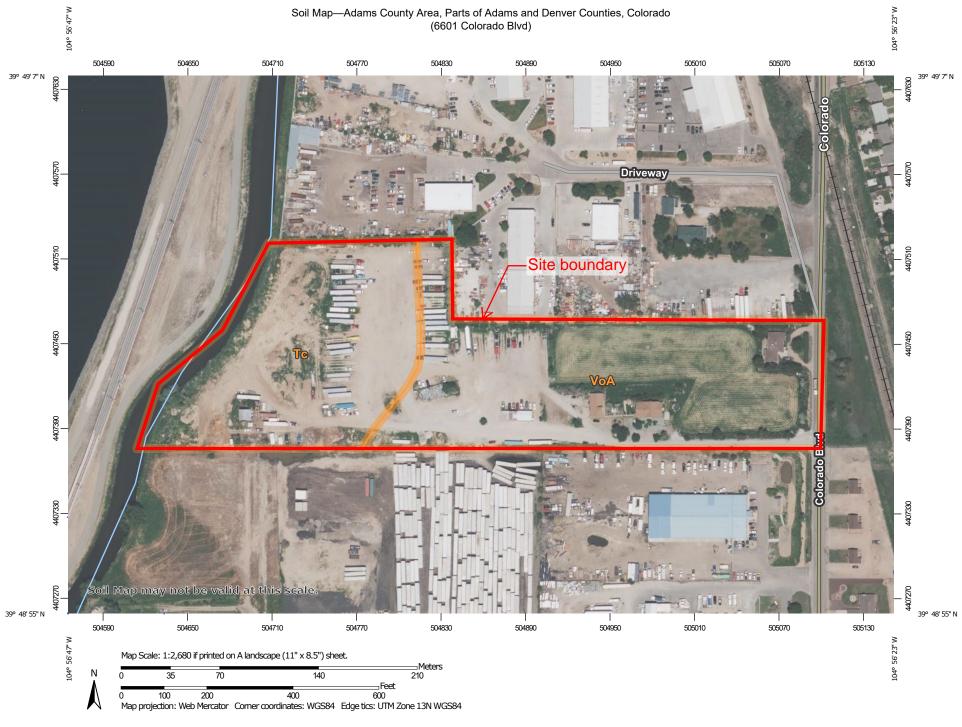
**APPENDIX A – Reference Material** 

Vicinity Map NRCS Soils Map FEMA FIRM





VICINITY MAP



USDA Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey

MAP L
Area of Interest (AOI)         Area of Interest (AOI)         Soils         Soil Map Unit Polygons         Soil Map Unit Polygons         Soil Map Unit Points         Soil Assolution         March Points         Mine or Quary         Soil Map Unit Points         Soinkole         Soinkhole         Soinkhole



# Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
Тс	Terrace escarpments	5.3	42.9%
VoA	Vona sandy loam, 0 to 1 percent slopes	7.1	57.1%
Totals for Area of Interest		12.4	100.0%



# National Flood Hazard Layer FIRMette



### Legend

regulatory purposes.

#### 104°56'49"W 39°49'14"N SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT Without Base Flood Elevation (BFE) Zone A. V. A9 With BFE or Depth Zone AE, AO, AH, VE, AR SPECIAL FLOOD HAZARD AREAS **Regulatory Floodway** LOMF570-08-0791P eff.8/31/28 FEET 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X Future Conditions 1% Annual Chance Flood Hazard Zone X Area with Reduced Flood Risk due to Zone A Levee. See Notes. Zone X OTHER AREAS OF FLOOD HAZARD Area with Flood Risk due to Levee Zone D NO SCREEN Area of Minimal Flood Hazard Zone X Effective LOMRs OTHER AREAS Area of Undetermined Flood Hazard Zone D - — – – Channel, Culvert, or Storm Sewer GENERAL STRUCTURES LIIII Levee, Dike, or Floodwall CITY OF COMMERCE CITY 20.2 Cross Sections with 1% Annual Chance 080006 17.5 Water Surface Elevation **Coastal Transect** T003S R067W S06 AREA OF MINIMAL FLOOD HAZARD Mase Flood Elevation Line (BFE) Limit of Study T03S R67W S6 Zone X T03S R68W S1 Jurisdiction Boundary EETS **Coastal Transect Baseline** T003S R068W S01 OTHER **Profile Baseline** 08001C0604F FEATURES Hydrographic Feature **Digital Data Available** No Digital Data Available MAP PANELS Unmapped The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location. This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 2/7/2023 at 2:27 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time. This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for 104°56'12"W 39°48'46"N Feet unmapped and unmodernized areas cannot be used for

1:6.000

2.000

Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020

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250

500

1,000

1.500

APPENDIX B – Hydrology Calculations

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#### **COMPOSITE % IMPERVIOUS CALCULATIONS**

Subdivision: Lot 1, CLAIRE AND ALYSSA INDUSTRIAL SUBDIVISION Location: CO, Commerce City 
 Project Name:
 6601 Colorado Blvd

 Project No.:
 6CH01

 Calculated By:
 MSJ

 Checked By:
 JRR

 Date:
 2/7/22

			Paved Roa	ds		Lawns			Roofs		Reclaime	ed Asphalt	Surfacing	Basins Total
Basin ID	Total Area (ac)	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	Weighted % Imp.
A-1	0.69	100	0.00	0.00	0	0.00	0.00	90	0.69	90.20	80	0.00	0.00	90.20
A-2	0.87	100	0.63	72.69	0	0.24	0.00	90	0.00	0.00	80	0.00	0.00	72.69
A-3	1.07	100	1.03	95.87	0	0.05	0.00	90	0.00	0.00	80	0.00	0.00	95.87
A-4	2.90	100	0.00	0.00	0	0.24	0.00	90	0.00	0.00	80	2.66	73.50	73.50
A-5	0.17	100	0.00	0.00	0	0.17	0.00	90	0.00	0.00	80	0.00	0.00	0.00
A-6	1.87	100	0.00	0.00	0	0.50	0.00	90	0.00	0.00	80	1.37	58.60	58.60
A-7	3.65	100	0.00	0.00	0	1.47	0.00	90	0.00	0.00	80	2.19	47.90	47.90
B-1	0.14	100	0.04	28.57	0	0.10	0.00	90	0.00	0.00	80	0.00	0.00	28.57
C-1	0.19	100	0.00	0.00	0	0.19	0.00	90	0.00	0.00	80	0.00	0.00	0.00
Total	11.55	100	1.70	14.71	0	2.96	0.00	90	0.69	5.40	80	6.22	43.10	63.21

otal Site As Designed

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#### **COMPOSITE % IMPERVIOUS CALCULATIONS**

Subdivision: Lot 1, CLAIRE AND ALYSSA INDUSTRIAL SUBDIVISION Location: CO, Commerce City 
 Project Name:
 6601 Colorado Blvd

 Project No.:
 6CH01

 Calculated By:
 MSJ

 Checked By:
 JRR

 Date:
 2/7/22

			Paved Roa	ds		Lawns			Roofs		Reclaime	ed Asphalt	Surfacing	Basins Total
Basin ID	Total Area (ac)	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	Weighted % Imp.
A-1	0.69	100	0.00	0.00	0	0.00	0.00	90	0.69	90.20	80	0.00	0.00	90.20
A-2	0.87	100	0.63	72.69	0	0.24	0.00	90	0.00	0.00	80	0.00	0.00	72.69
A-3	1.07	100	1.03	95.87	0	0.05	0.00	90	0.00	0.00	80	0.00	0.00	95.87
A-4	2.90	100	0.00	0.00	0	0.24	0.00	90	0.00	0.00	80	2.66	73.50	73.50
A-5	0.17	100	0.00	0.00	0	0.17	0.00	90	0.00	0.00	80	0.00	0.00	0.00
A-6	1.87	100	0.00	0.00	0	0.50	0.00	90	0.00	0.00	80	1.37	58.60	58.60
A-7	3.65	100	0.00	0.00	0	1.47	0.00	90	0.00	0.00	80	2.19	47.90	47.90
B-1	0.13	100	0.03	22.73	0	0.10	0.00	90	0.00	0.00	80	0.00	0.00	22.73
C-1	0.19	100	0.00	0.00	0	0.19	0.00	90	0.00	0.00	80	0.00	0.00	0.00
Total	11.55	100	1.69	14.64	0	2.96	0.00	90	0.69	5.40	80	6.22	43.10	63.14

Total Site As Designed

### STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Lot 1, CLAIRE AND ALYSSA INDUSTRIAL SUBDIVISION Location: CO, Commerce City Project Name: 6601 Colorado Blvd

Project No.: 6CH01

Calculated By: MSJ Checked By: JRR

Date: 2/7/22

		SUB-B/	ASIN			INITI/	AL/OVER	LAND		TR	AVEL TIN	1E			Tc CHECK		
		DAT	A				(T <sub>i</sub> )				(T <sub>t</sub> )			(U	RBANIZED BA	SINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	C <sub>100</sub>	C <sub>5</sub>	L	S	Ti	L	S	Cv	VEL.	T <sub>t</sub>	COMP. T <sub>c</sub>	TOTAL	Urbanized $T_c$	T <sub>c</sub>
ID	(AC)	Soils Group	(%)			(FT)	(%)	(MIN)	(FT)	(%)		(FPS)	(MIN)	(MIN)	LENGTH (FT)	(MIN)	(MIN)
A-1	0.69	А	90.2	0.81	0.75												5.0
A-2	0.87	А	72.7	0.68	0.57												5.0
A-3	1.07	A	95.9	0.86	0.82												5.0
A-4	2.90	A	73.5	0.68	0.58												5.0
A-5	0.17	A	0.0	0.11	0.00												5.0
A-6	1.87	A	58.6	0.57	0.44												5.0
A-7	3.65	A	47.9	0.48	0.34												5.0
B-1	0.14	A	28.6	0.33	0.17												5.0
C-1	0.19	A	0.0	0.11	0.00												5.0
Total	11.55	А	63.2	0.60	0.48												5.0
																	5.0

#### NOTES:

 $T_i = (0.395^{*}(1.1 - C_5)^{*}(L)^{0.5})/((S)^{0.33}), S in ft/ft$ 

T<sub>t</sub>=L/60V (Velocity From Fig. 501)

Velocity V=Cv\*S^0.5, S in ft/ft

Tc Check = 10+L/180

For Urbanized basins a minimum  $T_{\rm c}$  of 5.0 minutes is required.

For non-urbanized basins a minimum  $T_c$  of 10.0 minutes is required

#### STANDARD FORM SF-3

#### STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision: Lot 1, CLAIRE AND ALYSSA INDUSTRIAL SUBDIVISION

Project Name: 6601 Colorado Blvd

Project Name: 6001 Col Project No.: 6CH01 Calculated By: MSJ Checked By: JRR Date: 2/7/22

Location: CO, Commerce City Design Storm: 5-Year

				DIR	ECT RI	JNOFF			1	OTAL	RUNO	F	STR	EET	1	PIPE		TRA	AVEL -	ГІМЕ	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	l (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	l (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	REMARKS
	1	A-1	0.69	0.75	5.0	0.52	4.79	2.5													Building Roof area
	1	A-2	0.87	0.57	5.0	0.49	4.79	2.3													Parking lot area north of building
	1	A-3	1.07	0.82	5.0	0.88	4.79	4.2													Parking lot area south of building
	1	A-4	2.90	0.58	5.0	1.68	4.79	8.0													Gravel lot, swale and inlet at north prop edge
	1	A-5	0.17	0.00	5.0	0.00	4.79	0.0													Landscape area, swale and inlet at north prop edge
	1	A-6	1.87	0.44	5.0	0.82	4.79	3.9													Gravel lot, swale and inlet along north and west edge
	1	A-7	3.65	0.34	5.0	1.24	4.79	5.9													Gravel lot, sheet flow to infiltration pond
									5.0	5.63	4.79	27.0									Total runoff from on-site to infiltration pond
	2	B-1	0.14	0.17	5.0	0.02	4.79	0.1													East frontage of site sheet flowing east to Colo. Blvd
									5.0	0.02	4.79	0.1									Total runoff from on-site to Colorado Blvd
	3	C-1	0.19	0.00	5.0	0.00	4.79	0.0													Existing area to remain. All Lscape. Sheet flow to canal
									5.0	0.00	4.79	0.0									Total runoff from on-site to O'Brian Canal
																	<u> </u>			<u> </u>	

#### STANDARD FORM SF-3 STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Location: CO, Commerce City Design Storm: 100-Year	Subdivision:	Lot 1, CLAIRE AND ALYSSA INDUSTRIAL SUBDIVISION
Design Storm: 100-Year		
	Design Storm:	100-Year

Project Name:	6601 Colorado Blvd
Project No.:	6CH01
Calculated By:	MSJ
Checked By:	JRR
Date:	2/7/22

DIRECT RUNOFF TOTAL RUNOFF STREET PIPE TRAVEL TIME Design Flow (cfs) ipe Size (inches) Street Flow (cfs) /elocity (fps) Jesign Point Runoff Coeff. ength (ft) STREET REMARKS Slope (%) Slope (%) Area (Ac) **Basin ID** C\*A (Ac) C\*A (Ac) Tc (min) lc (min) Tt (min) (in/hr) (in/hr) Q (cfs) Q (cfs) 1 A-1 0.69 0.81 5.0 0.56 9.02 5.1 Building Roof area 0.87 0.68 A-2 5.0 0.59 9.02 5.3 Parking lot area north of building 1 1 1.07 0.86 0.92 A-3 5.0 9.02 8.3 Parking lot area south of building 5.0 1 A-4 2.90 0.68 1.97 9.02 17.8 Gravel lot, swale and inlet at north prop edge A-5 0.17 0.11 5.0 0.02 9.02 0.2 Landscape area, swale and inlet at north prop edge 1 9.02 1 1.87 0.57 1.07 Gravel lot, swale and inlet along north and west edge A-6 5.0 9.7 A-7 3.65 0.48 5.0 1.75 9.02 15.8 Gravel lot, sheet flow to infiltration pond 5.0 6.88 4.79 33.0 Total runoff from on-site to infiltration pond 2 B-1 0.14 0.33 5.0 0.05 9.02 0.5 East frontage of site sheet flowing east to Colo. Blvd 5.0 0.05 4.79 0.2 Total runoff from on-site to Colorado Blvd 3 C-1 0.19 0.11 5.0 0.02 9.02 0.2 Existing area to remain. All Lscape. Sheet flow to canal 5.0 0.02 4.79 0.1 Total runoff from on-site to O'Brian Canal

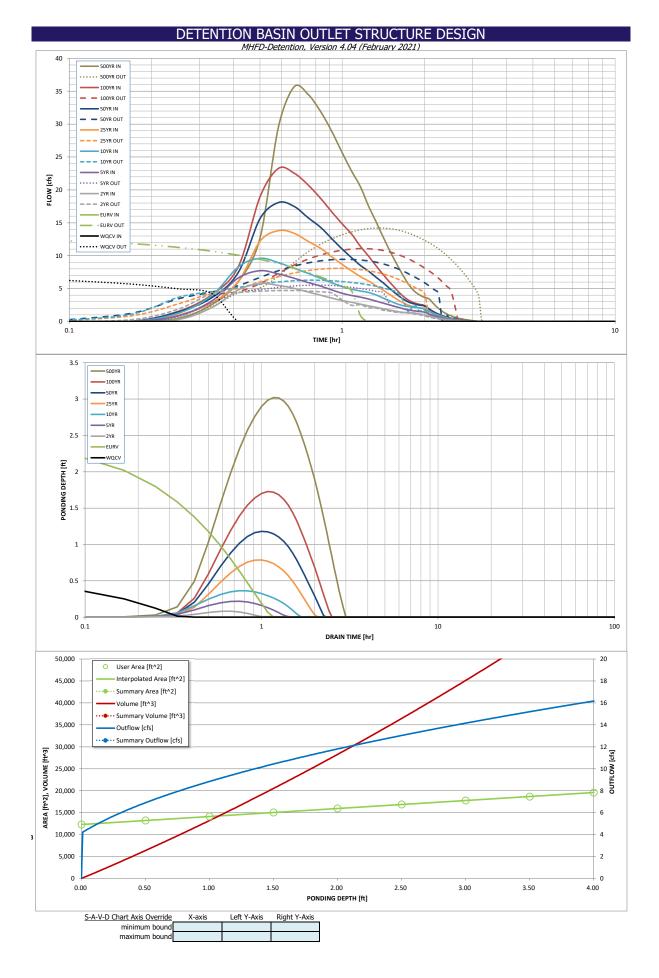
# **APPENDIX C – Hydraulic Calculations**

UD-Detention Spreadsheet Emergency Spillway Sizing UD-BMP Spreadsheets for Swales

# DETENTION BASIN OUTLET STRUCTURE DESIGN

	MHFD-Detention,	Version 4.04	(Februar	v 2021	)
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Basin ID: Site	
ZONE 2 ZONE 2 ZONE 1 ZONE 1 ZONE 1 ZONE 1 ZONE 1 ZONE 1	
Stage (ft) Volume (ac-ft) Outlet Type	
VOLUME EURV WOCV JOINT TO A CONTRACT TO A CONTRACT OF THE CONTRACT. THE CONTRACT OF THE CONTRACT OF THE CONTRACT OF THE CONTRACT OF THE CONTRACT. THE CONTRACT OF THE CONTRACT OF THE CONTRACT OF THE CONTRACT OF THE CONTRACT. THE CONTRACT O	
ZONE 1 AND 2 ORIFICE ZONE 2 (EURV) 2.59 0.687	
PERMANENT ORIFICES ZONE 3 (User) #VALUE! 2.521	
POOL     Example Zone Configuration (Retention Pond)     Total (all zones)     3.392	
User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP) Calculated Parameters for Underd	<u>ain</u>
Underdrain Orifice Invert Depth = $1.00$ ft (distance below the filtration media surface) Underdrain Orifice Area = $1.6$ ft <sup>2</sup>	
Underdrain Orifice Diameter = 17.25 inches Underdrain Orifice Centroid = 0.72 feet	
User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)  Calculated Parameters for Plate  NO Orifice Area are Day  NO Orifice Area area Area  NO Orifice Area area  NO Orifice Area area	
Invert of Lowest Orifice =ft (relative to basin bottom at Stage = 0 ft)WQ Orifice Area per Row = $N/A$ $ft^2$ Depth at top of Zone using Orifice Plate =ft (relative to basin bottom at Stage = 0 ft)Elliptical Half-Width = $N/A$ feet	
Orifice Plate: Orifice Vertical Spacing = inches Elliptical Slot Centroid = N/A feet	
Orifice Plate: Orifice Area per Row = $\frac{1}{10000000000000000000000000000000000$	
User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)	
Row 1 (optional) Row 2 (optional) Row 3 (optional) Row 4 (optional) Row 5 (optional) Row 6 (optional) Row 7 (optional) Row 8 (optional)	)
Stage of Orifice Centroid (ft)	
Orifice Area (sq. inches)	
	_
Row 9 (optional) Row 10 (optional) Row 11 (optional) Row 12 (optional) Row 13 (optional) Row 14 (optional) Row 15 (optional) Row 16 (optional)	<u>1)</u>
Stage of Orifice Centroid (ft)	
Orifice Area (sq. inches)	
User Input: Vertical Orifice (Circular or Rectangular) Calculated Parameters for Vertical	Orifico
	Jrince
Not Coloritoria Not Coloritoria Not Coloritoria	ft <sup>2</sup>
Not Selected Not S	
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Invert of Vertical Orifice       ft (relative to basin bottom at Stage = 0 ft)       Vertical Orifice Area =         Depth at top of Zone using Vertical Orifice       ft (relative to basin bottom at Stage = 0 ft)       Vertical Orifice Centroid =	feet
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Invert of Vertical Orifice =       ft (relative to basin bottom at Stage = 0 ft)       Vertical Orifice Area =         Depth at top of Zone using Vertical Orifice =       ft (relative to basin bottom at Stage = 0 ft)       Vertical Orifice Centroid =	feet
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Invert of Vertical Orifice =       ft (relative to basin bottom at Stage = 0 ft)       Vertical Orifice Area =         Depth at top of Zone using Vertical Orifice =       ft (relative to basin bottom at Stage = 0 ft)       Vertical Orifice Centroid =         Vertical Orifice Diameter =       inches	
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Invert of Vertical Orifice =	<u>v Weir</u> feet
Invert of Vertical Orifice =	<u>v Weir</u> feet
Invert of Vertical Orifice =	v Weir feet feet
Invert of Vertical Orifice =	v Weir feet feet ft <sup>2</sup>
Invert of Vertical Orifice =	<u>v Weir</u> feet feet ft <sup>2</sup> ft <sup>2</sup>
Invert of Vertical Orifice =       inches         Depth at top of Zone using Vertical Orifice =       inches         Vertical Orifice Diameter =       inches         User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe).       Calculated Parameters for Overflow         Overflow Weir Front Edge Height, Ho =       Not Selected       ft (relative to basin bottom at Stage = 0 ft)       Height of Grate Upper Edge, Ht =       Overflow Weir Stope Length =         Overflow Weir Front Edge Length =       feet       Overflow Weir Stope Length =       Intervention of the top of the	<u>v Weir</u> feet feet ft <sup>2</sup> ft <sup>2</sup>
Invert of Vertical Orifice =       inches         Depth at top of Zone using Vertical Orifice =       inches         Vertical Orifice Diameter =       inches         User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe).       Calculated Parameters for Overflow         Overflow Weir Front Edge Height, Ho =       Not Selected       Not Selected       Not Selected         Overflow Weir Front Edge Length =       feet       Overflow Weir Slope Length =       inches         Overflow Weir Grate Slope =       H:V       Grate Open Area / 100-yr Orifice Area =       inches         Horiz. Length of Weir Sides =       Mot Selected       feet       Overflow Grate Open Area w/ Debris =       inches         User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)       Not Selected       Not Selected	v Weir feet feet ft <sup>2</sup> ft <sup>2</sup>
Invert of Vertical Orifice =	v Weir feet feet ft <sup>2</sup> ft <sup>2</sup>
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Invert of Vertical Orifice =	v Weir feet feet ft <sup>2</sup> ft <sup>2</sup>
Invert of Vertical Orifice =	v Weir feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup>
Invert of Vertical Orifice =	v Weir feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup>
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Invert of Vertical Orifice =	v Weir feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup>
Invert of Vertical Orifice =	v Weir feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup>
Invert of Vertical Orifice =	v Weir feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup>
Invert of Vertical Orifice =       int (relative to basin bottom at Stage = 0 ft)       Vertical Orifice Area =         Depth at top of Zone using Vertical Orifice Diameter =       inches         User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe).       Calculated Parameters for Overflow Neir Slope Length =         Overflow Weir Front Edge Height, Ho =       Not Selected       Not Selected       Not Selected       Not Selected         Overflow Weir Grate Slope =       H:V       Grate Open Area / 100-yr Orifice Area =       inches         Overflow Weir Grate Slope =       H:V       Grate Open Area / 100-yr Orifice Area =       inches         User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)       Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)       Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate (Orcular Orifice, Restrictor Plate, or Rectangular Orifice)       Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate (Orcular Orifice Area =	v Weir feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> rt <sup>2</sup>
Invert of Vertical Orifice =	v Weir feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> feet radians
Invert of Vertical Orifice =	v Weir feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> feet radians gh AF). 500 Year
Invert of Vertical Orifice =       Invert of Vertical Orifice =       Invert of Vertical Orifice =       Invertical Orifice Area =         Depth at top of Zone using Vertical Orifice Diameter =       Invert of Vertical Orifice Diameter =       Invertical Orifice Diameter =       Invertical Orifice Centroid =         User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe).       Calculated Parameters for Overflow Neir Grate Upper Edge, H, =         Overflow Weir Front Edge Height, Ho       Invert of Vertical Orifice Slope =       Invertical Orifice Diameter =       Invertical Orifice Overflow Weir Grate Slope =         Horiz. Length Orier Slope       Invert of Vertical Orifice, Restrictor Plate, or Rectangular Orifice)       Calculated Parameters for Overflow Overflow Grate Open Area W/ Debris =         Overflow Grate Type =       Invert of Outlet Pipe       Not Selected       Not Selected         Debris Clogging % =       Invert of Outlet Pipe w/ How Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)       Calculated Parameters for Outlet Pipe w/ How Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)       Calculated Parameters for Outlet Pipe w/ How Restriction Plate Orifice Area =         User Input: Outlet Pipe w/ How Restriction Plate Orifice, Restrictor Plate, or Rectangular Orifice)       Calculated Parameters for Outlet Pipe w/ How Restriction Plate Orifice Area =         User Input: Inner of Outlet Pipe w/ How Restriction Plate Orifice Plate Not Selected       Not	v Weir feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> feet radians gh AF). 500 Year 3.35 2.445
Invert of Vertical Orifice =       inft       ft (relative to basin bottom at Stage = 0 ft)       Vertical Orifice Area =         Depth at top of Zone using Vertical Orifice Diameter =       inches         User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe).       Calculated Parameters for Overflow         Overflow Weir Front Edge Height, Ho =       Not Selected       Not Selected       Not Selected         Overflow Weir Front Edge Length =       Overflow Weir Grate Stope =       H+V       Grate Open Area w/loop or fice Area a =         Overflow Weir Grate Stope =       H+V       Grate Open Area w/loop or fice Area a =       Overflow Weir Stope Length =         Overflow Weir Grate Stope =       H+V       Grate Open Area w/loop or fice Area a =       Overflow Weir Stope Length =         Overflow Weir Grate Stope =       H+V       Grate Open Area w/loop or fice Area a =       Overflow Weir Stope Length =         Overflow Weir Front Edge Length =       Not Selected       Not Selected       Not Selected         Overflow Weir Grate Stope =       H+V       Grate Open Area w/loop or fice Area a =       Overflow Weir Stope =         Debris Clogging % =       Not Selected       Not Selected       Not Selected       Not Selected         Detric Unite Orifice Length =       Inclassin Area at Top orifice Area a =       Inclassin Area at Top orifice Area	<u>v Weir</u> feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> feet radians <u>500 Year</u> 3.35 2.445
Invert of Vertical Orifice       Invert of Vertical Orifice       Invert of Vertical Orifice area         Depth at top of Zone using Vertical Orifice Diameter =       Invert of Vertical Orifice Diameter =       Invert of Vertical Orifice Centrol =         User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe).       Calculated Parameters for Overflow Veir foront Edge Height, Ho =         Overflow Weir Front Edge Height, Ho =       Not Selected       Not Selected       Not Selected         Hvirz. Length of Weir Sizes =       Invert of Vertical Orifice Area =       Invert Ory Propring Area / 100-yr Orifice Area =       Invert Orifice Area =         Hvirz. Length of Weir Sizes =       Invert of Pite (Groular Orifice, Restrictor Plate, or Rectangular Orifice)       Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate (Oroular Orifice, Restrictor Plate, or Rectangular Orifice)       Calculated Parameters for Outlet Pipe w/ Flow Restriction         User Input: Outlet Pipe w/ Flow Restriction Plate (Oroular Orifice, Restrictor Plate, or Rectangular Orifice)       Calculated Parameters for Spillway Invert Stage =       Invert Stage = 0 ft)       Outlet Orifice Area =       Not Selected         User Input: Emergency Spillway (Rectangular or Trapezoidal)       Feet       Spillway Invert Stage =       Invert Stage = 0 ft)       Spillway Design Flow Depth =       Invert Spillway Invert Stage	v Weir feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> feet radians gh AF). 500 Year 3.35 2.445
Invert of Vertical Orifice =       inft       ft (relative to basin bottom at Stage = 0 ft)       Vertical Orifice Area =         Depth at top of Zone using Vertical Orifice Diameter =       inches         User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe).       Calculated Parameters for Overflow         Overflow Weir Front Edge Height, Ho =       Not Selected       Not Selected       Not Selected         Overflow Weir Front Edge Length =       Overflow Weir Grate Stope =       H+V       Grate Open Area w/loop or fice Area a         Overflow Weir Front Edge Length =       Overflow Weir Grate Stope =       H+V       Grate Open Area w/loop or fice Area a         Overflow Weir Front Edge Length =       Overflow Weir Grate Stope Area w/loop or fice Area a       Overflow Weir Stope Length =       Image: Calculated Parameters for Overflow Grate Open Area w/loop or fice Area a         Overflow Weir Front Edge Length =       Not Selected       Not Selected       Not Selected       Not Selected         Overflow Weir Front Edge Height, Ho =       Edet Area       Overflow Grate Open Area w/loop or fice Area a       Image: Calculated Parameters for Overflow Grate Stope       Image: Calculated Parameters for Overflow Height Area at Iloop, or fice Area a         Overflow Weir Front Edge Height, Ho =       Image: Calculate Area       Image: Calculate Area       Image: Calculate Area         User Input: Outlet Pipe	<u>v Weir</u> feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> feet radians <u>500 Year</u> 3.35 2.445
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Invert of Vertical Orifice a       th (relative to basin bottom at Stage = 0 ft)       Vertical Orifice Centroid =         Depth at top of Zone using Vertical Orifice Diameter =       inches         User Input: Overflow Weir (Dropbox with Flat or Stoped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe).       Calculated Parameters for Overflow         Overflow Weir Front Edge Height, Ho =       Not Selected       Not Selected       Not Selected         Overflow Weir Front Edge Height, Ho =       Not Selected       Not Selected       Not Selected         Overflow Weir Front Edge Leight =       Feet       Overflow Grate Open Area (1/00 Proffice Area =       Image: Control of Control open Area (1/00 Proffice Area =       Image: Controp	v Weir feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> feet radians gh AF). 500 Year 3.35 2.445 2.445 2.445 11.0 0.98 35.7 14.2
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Invert of Vertical Orifice       intervent         Depth at top of Zone using Vertical Orifice       intervent         Vertical Orifice Control =       intervent         Vertical Orifice Control =       intervent         User Input: Overflow Weir Font Edge Height, Ho       Not Selected         Not Selected       Not Selected         Overflow Weir Font Edge Height, Ho       Not Selected         Overflow Weir Font Edge Length       fet         Overflow Grate Open Area v/ Debris =       intches         Debris Clogging % =       gs         User Input: Outlet Pipe W. How Restricton Plate, Greater Pipe =       gs         Overflow Grate Open Area v/ Debris =       intches         Itser Input: Emergency Splikway (Rectangular or Trapezoidal)       Calculated Parameters for Spallway Edge Length         Fet	v Weir feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> feet radians gh AF). 500 Year 3.35 2.445 2.445 2.445 11.0 0.98 35.7 14.2 1.3 a Filtration Media N/A N/A
Invert of Vertical Orfice =       in       if (relative to basin bottom at Stage = 0 ft)       Vertical Orfice Area =       in         Depth at top of Zone using Vertical Orfice Dameter =       inches       inches       inches         User Input: Overflow Weir Cont Edge Height, Ho       Not Selected       Not Sel	v Weir feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> feet radians gh AF). 500 Year 3.35 2.445 2.445 11.0 0.98 35.7 14.2 1.3 a filtration Media N/A N/A 3
Invert of Vertical Orfice =       in the set of	<u>v Weir</u> feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> feet radians <u>gh AF).</u> <u>500 Year</u> 3.35 2.445 11.0 0.98 35.7 14.2 1.3 a filtration Media N/A N/A N/A 3 3
Invert of Vertical Orfice =       in       if (relative to basin bottom at Stage = 0 ft)       Vertical Orfice Area =       in         Depth at top of Zone using Vertical Orfice Dameter =       inches       inches       inches         User Input: Overflow Weir Cont Edge Height, Ho       Not Selected       Not Sel	v Weir feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> feet radians gh AF). 500 Year 3.35 2.445 2.445 11.0 0.98 35.7 14.2 1.3 a filtration Media N/A N/A 3



# DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

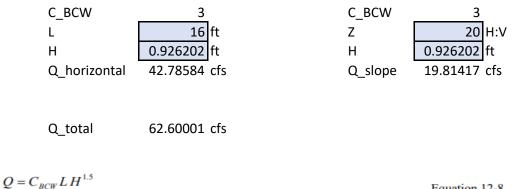
Inflow Hydrographs

	The user can o	verride the calcu	ulated inflow hy	drographs from	this workbook	with inflow hydr	ographs develop	oed in a separate	program.	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.48
	0:15:00	0.00	0.00	0.29	0.84	1.25	0.99	1.44	1.52	2.59
	0:20:00	0.00	0.00	2.12	3.13	3.97	2.84	3.63	4.09	6.05
	0:25:00	0.00	0.00	4.80	6.62	8.31	6.11	7.47	8.34	12.66
	0:30:00	0.00	0.00	5.77	7.71	9.59	12.19	15.63	18.93	29.50
	0:35:00	0.00	0.00	5.49	7.24	8.94	13.80	18.07	23.26	35.66
	0:40:00	0.00	0.00	5.05	6.57	8.09	13.42	17.51	22.55	34.53
	0:45:00	0.00	0.00	4.48	5.92	7.32	12.18	15.78	20.76	31.91
	0:50:00 0:55:00	0.00	0.00	3.99 3.55	5.38	6.56	11.12 9.83	14.32 12.58	18.72 16.65	28.88 25.66
	1:00:00	0.00	0.00		4.79 4.28	5.88 5.30	9.83		10.05	23.86
	1:05:00	0.00	0.00	3.18 2.93	3.94	4.91	7.69	11.01 9.69	13.28	22.88
	1:10:00	0.00	0.00	2.63	3.70	4.64	6.82	8.53	11.41	17.51
	1:15:00	0.00	0.00	2.38	3.41	4.40	6.13	7.63	9.93	15.11
	1:20:00	0.00	0.00	2.15	3.09	4.03	5.41	6.71	8.43	12.74
	1:25:00	0.00	0.00	1.93	2.78	3.54	4.75	5.85	7.09	10.64
	1:30:00	0.00	0.00	1.72	2.49	3.09	4.05	4.95	5.90	8.77
	1:35:00	0.00	0.00	1.53	2.23	2.71	3.41	4.14	4.83	7.10
	1:40:00	0.00	0.00	1.39	1.94	2.43	2.87	3.45	3.90	5.66
	1:45:00	0.00	0.00	1.32	1.75	2.27	2.47	2.96	3.24	4.66
	1:50:00	0.00	0.00	1.29	1.62	2.16	2.25	2.67	2.85	4.06
	1:55:00 2:00:00	0.00	0.00	1.15	1.53	2.06 1.89	2.10	2.49	2.61 2.44	3.68
	2:05:00	0.00	0.00	0.82	1.42	1.89	1.59	1.88	1.91	3.41 2.66
	2:10:00	0.00	0.00	0.64	0.88	1.18	1.23	1.46	1.45	2.00
	2:15:00	0.00	0.00	0.50	0.68	0.91	0.95	1.10	1.10	1.51
	2:20:00	0.00	0.00	0.38	0.53	0.70	0.73	0.86	0.84	1.15
	2:25:00	0.00	0.00	0.29	0.40	0.53	0.56	0.66	0.64	0.88
	2:30:00	0.00	0.00	0.22	0.30	0.40	0.42	0.49	0.48	0.66
	2:35:00	0.00	0.00	0.17	0.22	0.30	0.31	0.37	0.36	0.49
	2:40:00	0.00	0.00	0.12	0.16	0.23	0.23	0.28	0.28	0.38
	2:45:00	0.00	0.00	0.09	0.12	0.16	0.17	0.20	0.20	0.28
	2:50:00	0.00	0.00	0.06	0.08	0.11	0.12	0.14	0.14	0.19
	2:55:00 3:00:00	0.00	0.00	0.04	0.05	0.07	0.08	0.09	0.09	0.12
	3:05:00	0.00	0.00	0.02	0.03	0.04	0.05	0.05	0.05	0.07
	3:10:00	0.00	0.00	0.00	0.00	0.02	0.02	0.02	0.02	0.03
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00 4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00 4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00 4:55:00	0.00 0.00	0.00	0.00	0.00	0.00 0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00 5:15:00	0.00 0.00	0.00	0.00	0.00	0.00 0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00 5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

e user should graphically compare the summary S-A-V-D table to the full S-A- Stage Stage Area Area			Total				
Stage - Storage Description	[ft]	[ft <sup>2</sup> ]	[acres]	[ft <sup>3</sup> ]	[ac-ft]	Outflow [cfs]	
							For best results, inc
							stages of all grade s
							changes (e.g. ISV a from the S-A-V table
							Sheet 'Basin'.
				-			Also include the inve outlets (e.g. vertical
							overflow grate, and
							where applicable).
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# DETENTION BASIN OUTLET STRUCTURE DESIGN

#### Emergency spillway sizing



Where:

Equation 12-8

Q = discharge (cfs)

 $C_{BCW}$  = broad-crested weir coefficient (This ranges from 2.6 to 3.0. A value of 3.0 is often used in practice.) See Hydraulic Engineering Circular No. 22 for additional information.

L = broad-crested weir length (ft)

H = head above weir crest (ft)

Sloping Broad-Crested Weir: Figure 12-20 shows an example of a sloping broad-crested weir. The equation to calculate the flow over the sloping portion of the weir is as follows:

$$Q = \left(\frac{2}{5}\right) C_{BCW} Z H^{2.5}$$

Equation 12-9

Where:

Q = discharge (cfs)

 $C_{BCW}$  = broad-crested weir coefficient (This ranges from 2.6 to 3.0. A value of 3.0 is often used in practice.) See Hydraulic Engineering Circular No. 22 for additional information.

Z = side slope (horizontal: vertical)

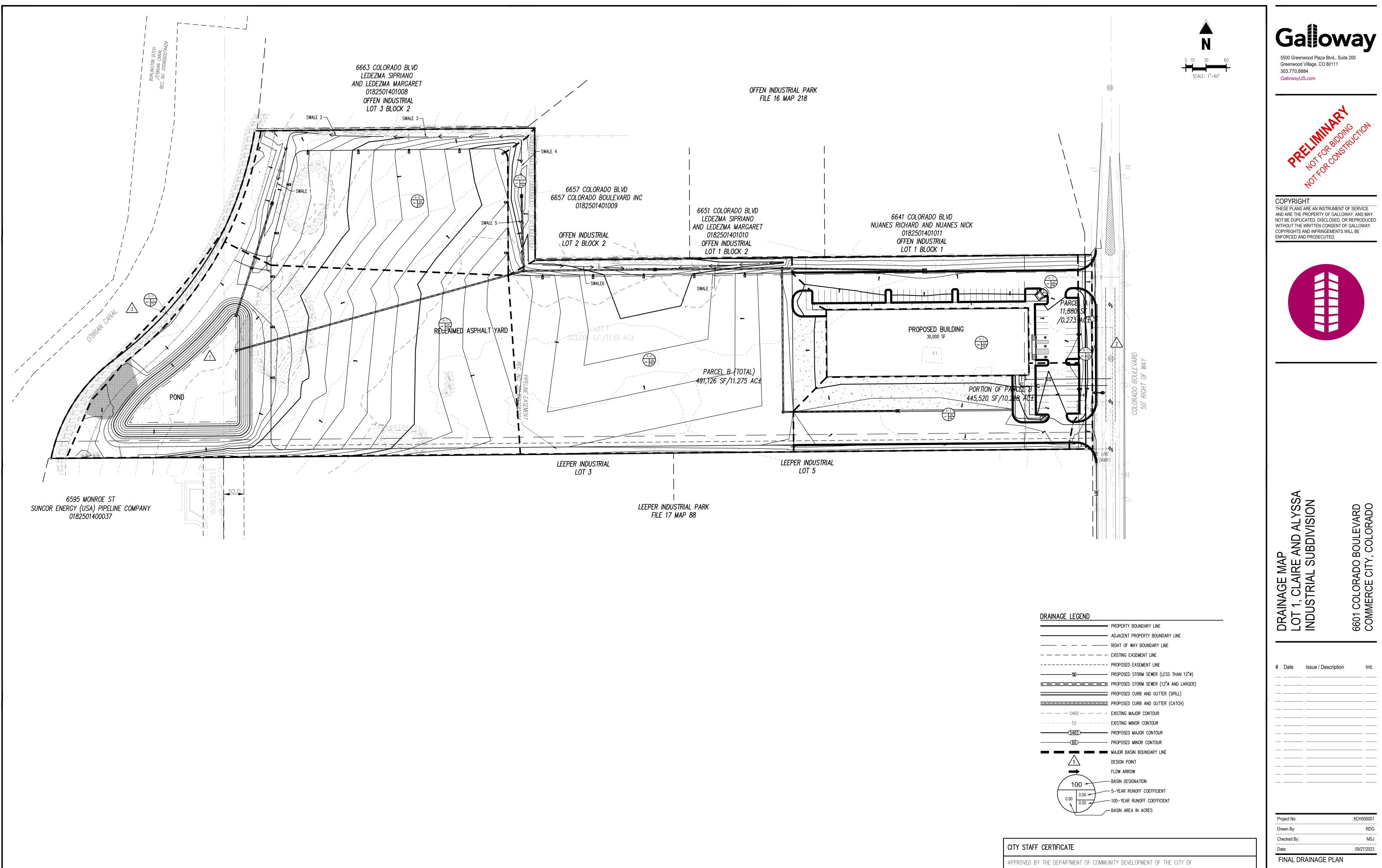
H = head above weir crest (ft)

	Design Procedure Form: Gras UD-BMP (Version 3.07, Mar					
Designer:	MSJ					
Company:	Galloway					
Date:	September 27, 2023					
Project:	6601 Colorado Boulevard					
Location:	Commerce City, CO - SWALE 1					
1. Design Dis	scharge for 2-Year Return Period	$Q_2 = 3.90$ cfs				
2. Hydraulic I	Residence Time					
A) : Lengt	h of Grass Swale	$L_{\rm S} = 257.0$ ft				
B) Calcula	ated Residence Time (based on design velocity below)	T <sub>HR</sub> =4.4 minutes				
3. Longitudin	al Slope (vertical distance per unit horizontal)					
A) Availab	ble Slope (based on site constraints)	$S_{avail} = 0.020$ ft / ft				
B) Design	Slope	$S_{D} = 0.008$ ft / ft				
4. Swale Geo	ometry					
A) Channe	el Side Slopes (Z = 4 min., horiz. distance per unit vertical)	Z = 4.00 ft / ft				
	Width of Swale (enter 0 for triangular section)	$W_{\rm B} = $ 0.00 ft				
5. Vegetation	1	Choose One				
A) Type o	f Planting (seed vs. sod, affects vegetal retardance factor)	◯ Grass From Seed				
6. Design Ve	locity (0.857 ft / s maximum for desirable 5-minute residence time)	$V_2 = 0.98$ ft / s				
7. Design Flo	ow Depth (1 foot maximum)	$D_2 = 1.00$ ft				
A) Flow A	rea	$A_2 = 4.0$ sq ft				
B) Top W	idth of Swale	$W_T = 8.0$ ft				
C) Froude	Number (0.50 maximum)	F = 0.24				
D) Hydrau		R <sub>H</sub> = 0.49				
	y-Hydraulic Radius Product for Vegetal Retardance	VR = 0.47				
	ng's n (based on SCS vegetal retardance curve D for sodded grass) ative Height of Grade Control Structures Required	$n = 0.084$ $H_{\rm D} = 3.10$ ft				
8. Underdrair (Is an und	n derdrain necessary?)	Choose One       REQUIRED IF THE         Image: State of the state of				
9. Soil Prepa (Describes	ration soil amendment)					
10. Irrigation		Choose One Temporary  Permanent				
Notes:						

	Design Procedure Form: Grass Swale (GS)						
Designer:	UD-BMP (Version 3.07, March	1 2018) Sheet 1 of 1					
Company:	Galloway						
Date:	May 26, 2023						
Project:	6601 Colorado Boulevard						
Location:	Location: Commerce City, CO - SWALE 6						
1. Design Dis	scharge for 2-Year Return Period	$Q_2 = 4.00$ cfs					
2. Hydraulic F	2. Hydraulic Residence Time						
A) : Lengt	h of Grass Swale	L <sub>S</sub> = <u>165.0</u> ft					
B) Calcula	ated Residence Time (based on design velocity below)	T <sub>HR</sub> = <u>3.0</u> minutes					
3. Longitudin	al Slope (vertical distance per unit horizontal)						
A) Availab	ole Slope (based on site constraints)	S <sub>avail</sub> = 0.020 ft / ft					
B) Design	Slope	$S_{D} = 0.020$ ft / ft					
4. Swale Geo	ometry						
A) Channe	el Side Slopes (Z = 4 min., horiz. distance per unit vertical)	Z = 10.30 ft / ft					
B) Bottom	Width of Swale (enter 0 for triangular section)	W <sub>B</sub> = 0.00 ft					
5. Vegetation	1	Choose One					
A) Type of	f Planting (seed vs. sod, affects vegetal retardance factor)	Grass From Seed Grass From Sod					
6. Design Ve	locity (0.55 ft / s maximum for desirable 5-minute residence time)	$V_2 = 0.92$ ft / s					
7. Design Flo	w Depth (1 foot maximum)	$D_2 = 0.65$ ft					
A) Flow A	rea	A <sub>2</sub> =sq ft					
B) Top Wi	idth of Swale	W <sub>T</sub> = 13.4 ft					
C) Froude	Number (0.50 maximum)	F = 0.28					
D) Hydrau							
E) Velocit	y-Hydraulic Radius Product for Vegetal Retardance	VR =					
F) Mannin	g's n (based on SCS vegetal retardance curve D for sodded grass)	n =					
G) Cumula	ative Height of Grade Control Structures Required	$H_D = 0.00$ ft					
8. Underdrair (Is an und	n derdrain necessary?)	Choose One					
9. Soil Prepa	ration soil amendment)						
(Describe s							
10. Irrigation		Choose One Temporary  Permanent					
Notes:							

	Design Procedure Form: Gras					
Designer:	UD-BMP (Version 3.07, Marc MSJ	h 2018) Sheet 1 of				
Company:	Galloway					
Date:	September 27, 2023					
Project:	6601 Colorado Boulevard					
Location:	Commerce City, CO - SWALE 7					
1. Design Di	scharge for 2-Year Return Period	$Q_2 = 4.00$ cfs				
2. Hydraulic	Residence Time					
A) : Lengt	th of Grass Swale	L <sub>S</sub> = 187.5 ft				
B) Calcula	ated Residence Time (based on design velocity below)	T <sub>HR</sub> = <u>3.2</u> minutes				
3. Longitudin	nal Slope (vertical distance per unit horizontal)					
A) Availal	ble Slope (based on site constraints)	$S_{avail} = 0.020$ ft / ft				
B) Desigr		$S_D = 0.010$ ft / ft				
4. Swale Ge	ometry					
A) Chann	el Side Slopes (Z = 4 min., horiz. distance per unit vertical)	Z = 5.00 ft / ft				
B) Bottom	n Width of Swale (enter 0 for triangular section)	$W_B = 0.00$ ft				
5. Vegetatior	n	Choose One				
-	of Planting (seed vs. sod, affects vegetal retardance factor)	Grass From Seed Grass From Sod				
А) туре о						
6. Design Ve	elocity (0.625 ft / s maximum for desirable 5-minute residence time)	$V_2 = 0.99$ ft / s				
7. Design Flo	ow Depth (1 foot maximum)	$D_2 = 0.90$ ft				
A) Flow A	Area	$A_2 = 4.1$ sq ft				
B) Top W	/idth of Swale	$W_T = 9.0$ ft				
	Number (0.50 maximum)	F = 0.26				
D) Hydrau	ulic Radius	$R_{H} = 0.44$				
E) Velocit	ty-Hydraulic Radius Product for Vegetal Retardance	VR = 0.44				
F) Mannir	ng's n (based on SCS vegetal retardance curve D for sodded grass)	n = 0.088				
G) Cumul	lative Height of Grade Control Structures Required	$H_D = 1.90$ ft				
8. Underdrai		Choose One     AN UNDERDRAIN IS     REQUIRED IF THE     DESIGN SLOPE < 2.0%				
(is an un	derdrain necessary?)	DESIGN SLOPE < 2.0%				
9. Soil Prepa	aration					
	soil amendment)					
10. Irrigation		Choose One Temporary  Permanent				
<b>U</b>						
Notes:		1				

APPENDIX D – Drainage Map





DEPARTMENT OF COMMUNITY DEVELOPMENT SIGNATURE

COMMERCE CITY, THIS \_\_\_\_\_ DAY OF \_\_\_\_\_, \_\_\_ A.D.

DR1